SOURCES OF WATER AND NITROGEN TO THE WIDEFIELD AQUIFER,
SOUTHWESTERN EL PASO COUNTY, COLORADO

By Patrick Edelmann and Doug Cain

U.S. GEOLOGICAL SURVEY

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COLORADO SPRINGS DEPARTMENT OF PUBLIC UTILITIES and the

LOWER FOUNTAIN WATER-QUALITY MANAGEMENT ASSOCIATION



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# METRIC CONVERSION FACTORS

Inch-pound units used in this report may be converted to International System of Units (SI) by using the following conversion factors:

| Multiply inch-pound unit | Ву       | To obtain SI unit      |
|--------------------------|----------|------------------------|
| acre                     | 4,047    | square meter           |
| acre-foot                | 1,233    | cubic meter            |
| acre-foot per year       | 1,233    | cubic meter per annum  |
| cubic foot per second    | 0.02832  | cubic meter per second |
| cubic foot per day       | 0.02832  | cubic meter per day    |
| foot                     | 0.3048   | meter                  |
| foot per day             | 0.3048   | meter per day          |
| foot per mile            | 0.3048   | meter per mile         |
| inch                     | 25.40    | millimeter             |
| gallon per minute        | 0.06308  | liter per second       |
| gallon per day           | 0.003785 | cubic meter per day    |
| mile                     | 1.609    | kilometer              |
| mile per year            | 1.609    | kilometer per annum    |
| pound (avoirdupois)      | 453.6    | gram                   |
| pound per acre           | 1.120    | kilogram per hectare   |
| square foot              | 0.09294  | square meter           |
| square foot per day      | 0.09294  | square meter per day   |
| square mile              | 2.590    | square kilometer       |
| ton                      | 0.9072   | megagram               |

Water-quality terms and abbreviations used in this report:

milligram per liter (mg/L) milligram per liter as nitrogen (mg/L as N) microsiemen per centimeter at 25° Celsius ( $\mu$ s/cm) °Celsius (°C).



Fountain Creek downstream from the Colorado Springs Sewage  $$\operatorname{\textbf{Treatment}}$$  Plant effluent.

# SOURCES OF WATER AND NITROGEN TO THE WIDEFIELD AQUIFER, SOUTHWESTERN EL PASO COUNTY, COLORADO

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# ABSTRACT

The Widefield aquifer, located south of Colorado Springs, Colorado, is a shallow, very permeable part of the Fountain Creek alluvial aquifer, which is underlain by Pierre Shale. During the past 20 to 30 years, available data suggest that nitrate concentrations have increased from 0.5 to 3.0 milligrams per liter as nitrogen in the Widefield aquifer to concentrations that often approach and occasionally exceed the drinking-water standard of 10 milligrams per liter as nitrogen. Because of the large nitrate concentrations detected in the Widefield aquifer, distribution and sources of nitrogen to the aquifer were evaluated during 1981 and 1982.

During the summer of 1982, the concentration of nitrite plus nitrate in water collected from wells completed in the Widefield aquifer ranged from 3.2 to 15 milligrams per liter as nitrogen with a mean concentration of 6.9 milligrams per liter. In general, the concentrations of nitrite plus nitrate are greatest near the north end of the Widefield aquifer probably as a result of streamflow losses from Fountain Creek. These large concentrations appear to be diluted by tributary inflows or recharge from land surface in other parts of the aquifer.

A water budget for the Widefield aquifer indicates that the major source of inflow is recharge from Fountain Creek, north of the Widefield aquifer. During 1982, an estimated 8,000 acre-feet, or 65 percent of the 12,200 acre-feet of water that recharged the aquifer, was from streamflow losses from Fountain Creek. Other inflows to the aquifer, in order of decreasing contribution, are: (1) Infiltration and percolation of precipitation and irrigation return flow; (2) underflow from tributary alluvium; (3) underflow from Fountain Creek alluvium north of the Widefield aquifer; (4) infiltration from artificial recharge ponds on the Pinello Ranch; and (5) infiltration from septic systems and sewage lagoons.

A large percentage of flow in Fountain Creek is from the Colorado Springs Sewage Treatment Plant. During 1982, an estimated 38 percent of the flow and 85 percent of the nitrogen in Fountain Creek, in the reach that provides recharge to the Widefield aquifer, was from the Colorado Springs Sewage Treatment Plant. An estimated 130 tons of the total 162 tons of nitrogen available to recharge the aquifer during 1982 was from Fountain Creek. These data indicate that flow from the Colorado Springs Sewage Treatment Plant is the primary source of nitrogen entering the aquifer. Nitrogen also enters the aquifer as a result of seepage from Canal No. 4, which traverses the eastern part of the alluvial aquifer, artificial recharge ponds, and irrigation at the Pinello Ranch. These sources resulted in an additional 20 tons of nitrogen available to the aquifer during 1982. Nitrogen applied to the land through irrigation and fertilization probably was consumed by various crops in the area. Most of the nitrogen leaves the aquifer as a result of ground-water pumpage, and, to a lesser extent, by ground-water flow to Fountain Creek, ground-water outflow to the south, and possibly through denitrification processes.

#### 1.0 INTRODUCTION

The Widefield aquifer is located in the alluvium of Fountain Creek near Security, Colorado, about 5 miles south of Colorado Springs (fig. 1.0-1). The aquifer consists of alluvial-fill in a former channel of Fountain Creek. Approximately 30,000 people, currently (1983) living in the communities of Security, Stratmoor Hills, and Widefield, depend on the Widefield aquifer as their primary water supply. The aquifer is also used as a supplemental water supply for the city of Colorado Springs. Therefore, both the quantity and quality of ground water from the Widefield aquifer are important.

During 1981, analyses of water samples collected by the U.S. Geological Survey from wells tapping the Widefield aquifer indicated the ground water contained concentrations of nitrite plus nitrate between 5 and 10 mg/L as N (milligrams per liter as nitrogen). Because concentrations of nitrate in excess of 10 mg/L as N may cause methemoglobinemia in infants under three months of age, the U.S. Environmental Protection Agency (1976, p. 81) established a standard for nitrate in drinking water of 10 mg/L as N. As a result of the concentrations of nitrate found in 1981, the U.S. Geological Survey, in cooperation with the Colorado Springs Department of Public Utilities and the Lower Fountain Water Quality Management Association, expanded the study during 1982 and 1983 in an effort to determine: (1) Distribution and sources of nitrogen in the Widefield aquifer; and (2) quantity of water and nitrogen contributed to the aquifer by each source.

To meet these objectives, a 10-square-mile area (fig. 1.0-1), extending southward from Nevada Street in Colorado Springs to just south of Widefield was selected and intensively studied during 1982 and 1983. Within this reach, surface and ground water hydraulically connected to the Widefield aquifer were evaluated.

The scope of this investigation included: (1) Evaluating all existing hydrologic, geologic, and water-quality data for the study; (2) measuring flow and analyzing water samples collected from surface waters in the study area; (3) collecting and analyzing water samples from wells, tapping either the Widefield aquifer, Fountain Creek alluvium, or tributary alluvium to the Widefield aquifer; (4) evaluating hydraulic characteristics of the alluvial aquifer, using results from aquifer tests; (5) analyzing water samples collected from lagoons, ponds, and reservoirs overlying alluvium within the study area; and (6) installing and monitoring a nonrecording rain gage at Pinello Ranch (fig. 1.0-1). Much of the surface- and ground-water data used in this investigation was presented by Jenkins (1961, 1964), Bingham and Klein (1973), Livingston and others (1975), Klein and Bingham (1975), Livingston and others (1976a and 1976b), and Emmons (1977).

The authors wish to thank the many people who helped to make this study successful, including Gene Y. Michael, Gary Bostrom, Dennis T. Cafaro, Monte S. Fryt, William J. McCullough, and Max Grimes, with the Colorado Springs Department of Public Utilities; Robert T. Schrader, Bobby G. Padgett, and Richard L. Gilham with the Security Water and Sanitation District; Donald C. Lohrmeyer, Ronald Woolsey, and Chris Moffler with Widefield Homes Incorporated; Edmond W. Hakes and Elmer J. Wahlborg with the Stratmoor Hills Water and Sanitation District; F. Stuart Loosley with the Cherokee Water District; and Mary Barber with the U.S. Army.

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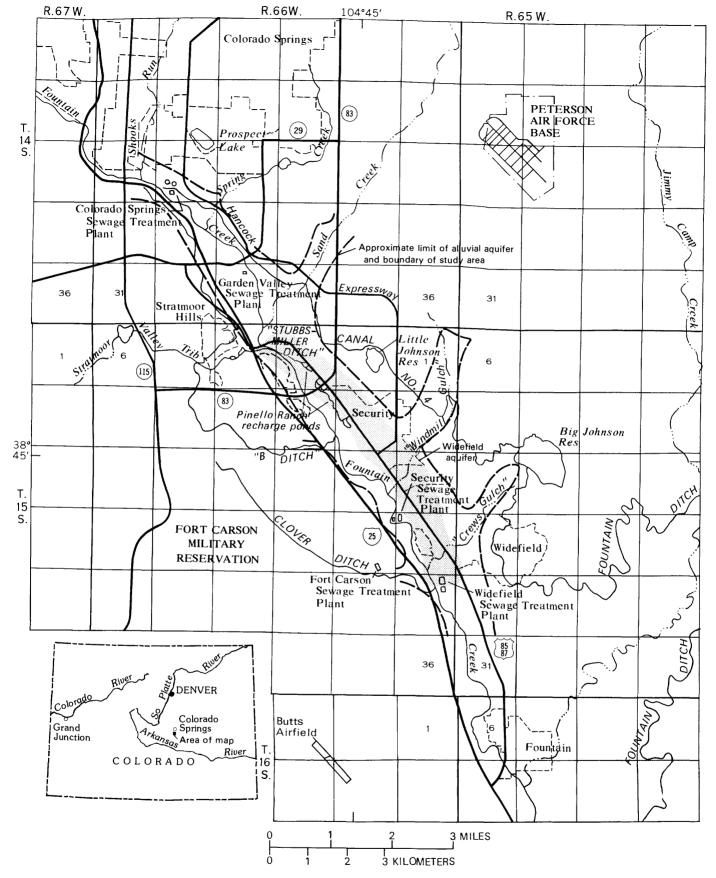


Figure 1.0-1.--Location of study area.

# 1.0 INTRODUCTION--Continued 1.1 Physical and Geologic Setting

The 10-square-mile study area lies in the valley of Fountain Creek and has mixed land uses. Most of the area adjacent to the flood plain of Fountain Creek is urbanized, except to the southwest, where the study area borders on Fort Carson Military Reservation. The flood plain generally is used for agriculture, although some light industry and commercial buildings are present. Most of the area east of Canal No. 4 and south of Sand Creek is undeveloped land, but some residential development is occurring.

Total relief in the area is about 400 feet, and the gradient of Fountain Creek is about 30 feet per mile. The valley floor is underlain by alluvium deposited on top of the Cretaceous Pierre Shale, which is the bedrock throughout the area. The alluvium consists of sand and gravel, with minor amounts of silt and clay (Jenkins, 1964, p. 15). The sand and gravel range in size from fine sand to cobbles; thickness of the alluvium ranges from 0 to 100 feet (fig. 1.1-1). The greatest thickness is in the Widefield-Security area (Livingston and others, 1976b, pl. 1), where the alluvium is deposited in a former channel of Fountain Creek, which is deeply eroded into shale bedrock. As indicated by figure 1.1-1, the 3.5-square-mile area, locally known as the Widefield aquifer, contains coarse sands; this area has the largest transmissive properties in the alluvial aquifer, with reported well yields as large as 3,120 gallons per minute. Eolian sand overlies older alluvial deposits and the Pierre Shale east of the Widefield aquifer (Scott and Wobus, 1973).



Venetucci Ranch--one of the three agricultural areas still remaining in the area.

# 1.0 INTRODUCTION--Continued

A temperate climate generally is prevalent in the area, characterized by about 85 percent sunny days, an annual relative humidity of about 54 percent, large daily range in temperature, and fairly mild winters with little snow. The area is semiarid with a mean annual precipitation of about 15.5 inches. However, large variations in annual precipitation do occur.

Between 1949 and 1982, annual precipitation at the Colorado Springs weather station located at Peterson Air Force Base ranged from 8.59 inches in 1964 to 25.43 inches in 1965 (fig. 1.2-1). The mean annual precipitation for this period was 15.48 inches. The cumulative departure from the mean precipitation from 1949 to 1982, illustrating temporal trends in precipitation, also is shown in figure 1.2-1. Cumulative decreases in precipitation occurred during the periods 1949-56, 1959-64, and 1972-75. Cumulative increases in precipitation occurred during the periods 1956-59 and 1975-82. Variations in precipitation affect the overall hydrologic system. For example, during a wet year, such as 1982, the streams had more flow and ground-water withdrawals decreased as a result of less agricultural and lawn-irrigation demands.

Areal variations in precipitation also occur (fig. 1.2-2) as a result of localized summer thunderstorms. For example, during 1982, 21.9 inches of precipitation were recorded at Colorado Springs weather station, which is located at Peterson Air Force Base; about 28 inches of precipitation were measured at the Pinello Ranch rain gage; and 24.3 inches of precipitation were recorded at Fort Carson's Butts Airfield weather station. Because Pinello Ranch lies in the study area, the monthly precipitation measured there is used in calculations for this report.

Semiarid conditions result in high evapotranspiration, which generally exceeds precipitation. Potential evapotranspiration is evapotranspiration that occurs when adequate moisture is always available. Potential evapotranspiration was estimated to be 32.7 inches in 1982 using the modified Blaney-Criddle equation (U.S. Soil Conservation Service, 1967, p. 7). The modified Blaney-Criddle equation uses mean monthly air temperature, monthly percentage of daytime hours of the year, and an empirical monthly consumptive-use crop coefficient, which varies by crop. Because the study area primarily is urbanized, the monthly crop coefficients for turf grass, as estimated by CH2M Hill (1982, p. 3) for the Colorado Springs area, were used. Actual evapotranspiration was estimated to be 21.9 inches in 1982. Monthly actual evapotranspiration was approximated by multiplying the monthly potential evapotranspiration by 0.67. This factor was used for the Colorado Springs area by CH2M Hill (1982, p. 4) and was derived from a relationship between lawn quality and relative evapotranspiration, developed by Danielson and others (1981, p. 32). Relative evapotranspiration is defined as the ratio of actual evapotranspiration to potential evapotranspiration. Monthly potential and actual evapotranspiration for 1982 are shown in figure 1.2-2. Annual evaporation from natural water bodies in the area, such as lakes, ponds, and reservoirs, was about 60 inches (Hansen and others, 1978, p. 33).

#### 2.0 SURFACE WATER

Surface water in the study area is hydraulically connected to the alluvial aquifer (Livingston and others, 1976a) and is an important source of recharge that affects the quality of water in the Widefield aquifer. During 1982, flow and water-chemistry data were obtained at 23 surface-water sites (fig. 2.0-1 and table 2.0-1). Four sites were on Fountain Creek; stream gages are operated at two of these sites (1 and 19). At site 1, the contributing drainage area of Fountain Creek (394 square miles) is mostly foothills or mountains north and west of Colorado Springs. The flow at site 1 is affected by diversions, ground-water pumpage, storage reservoirs, and small upstream municipal-sewage effluents.

As Fountain Creek crosses the study area, it receives additional sewage effluent from the city of Colorado Springs (site 3), Garden Valley (site 11), Security (site 18), Fort Carson Sewage Treatment Plant via Clover Ditch Drain (site 21), and Widefield (site 22)(fig. 2.0-1).

Several tributaries enter Fountain Creek in the study area. Shooks Run and Spring Creek (sites 2 and 9) drain the Colorado Springs urban area. Sand Creek (sites 12 and 13), an ephemeral stream, drains a 62-square-mile, partially urbanized area to the east of Colorado Springs. Sand Creek receives flows from a sand-and-gravel operation downstream from Canal No. 4 and may receive some seepage from an abandoned landfill located about a mile upstream from the mouth (Schneider and Turk, 1983). A small tributary, called Stratmoor Valley tributary in this report (site 14), drains Stratmoor Hills and areas to the west. B Ditch (site 16) drains part of the Fort Carson cantonment area and may receive seepage from an abandoned landfill used between 1946 and 1956 for disposal of mixed sanitary wastes, construction wastes, and sludges (M.E. Halla, Fort Carson Environmental Program Director, written commun., 1981). A small tributary locally known as "Windmill Gulch" (site 17) drains a relatively undeveloped area east of Security. Another small tributary from the east, locally known as "Crews Gulch" (site 20), provides drainage for much of Widefield and receives outflow from a small recreation lake owned by Fountain Valley School in the south end of Section 18, Township 15 South, Range 65 West. Water is pumped into the lake from two wells in the Widefield aquifer. Crews Gulch also may receive seepage from Big Johnson Reservoir.

Two major canals divert water from Fountain Creek for use in, or transportation through, the study area. Canal No. 4, also known as the Fountain Mutual Ditch, diverts water from Fountain Creek just downstream from the outfall of the Colorado Springs Sewage Treatment Plant. The flow of Canal No. 4 is recorded daily at the headgate (site 4). Canal No. 4 parallels Fountain Creek, and its water is used for minor amounts of irrigation between the headgate and Big Johnson Reservoir. Several intermediate data-collection sites (5, 6, and 7) were established on the canal during 1982 (fig. 2.0-1 and table 2.0-1). Another canal, locally known as the "Stubbs-Miller Ditch" (site 15), diverts water from Fountain Creek for artificial recharge and irrigation on the Pinello Ranch.

# 2.0 SURFACE WATER--Continued

#### 2.1 Fountain Creek

Flow in Fountain Creek is perennial in the study area. Records from stream gages at site 1, Fountain Creek at Colorado Springs, and site 19, Fountain Creek at Security (fig. 2.1-1), indicate that mean flows generally are low and fairly stable during the winter months, and quite variable during the irrigation season. These flow variations are caused by the amount of winter snowpack, and by the number and severity of summer thunderstorms.

Mean monthly flows at the gage at Security (site 19) are greater than at the upstream gage at Colorado Springs (site 1), because inflows between the gages are greater than diversions. Between 1976 and 1982, the mean flow of Fountain Creek at Security (site 19) was 33 ft<sup>3</sup>/s (cubic feet per second) greater than the mean flow of Fountain Creek at Colorado Springs (site 1). During 1982, the mean flow of Fountain Creek at Security was 110 ft<sup>3</sup>/s, and the mean flow of Fountain Creek at Colorado Springs was 54 ft<sup>3</sup>/s. The 56-ft<sup>3</sup>/s increase in flow in 1982 between site 1 and site 19 was the largest increase during the 1976-82 period. Fountain Creek flows in 1982 were among the highest for the period of record (fig. 2.1-2). Livingston and others (1976a) showed that Fountain Creek is hydraulically connected to the alluvial aquifer. In the reach just downstream from the confluence with Spring Creek to just downstream from the headgate of the Stubbs-Miller Ditch, the creek generally loses water to the ground-water system; from that point downstream to Security (site 19), it generally gains water from the ground-water system. This interconnection directly ties water-quality conditions in Fountain Creek to water-quality conditions in the alluvial aquifer.

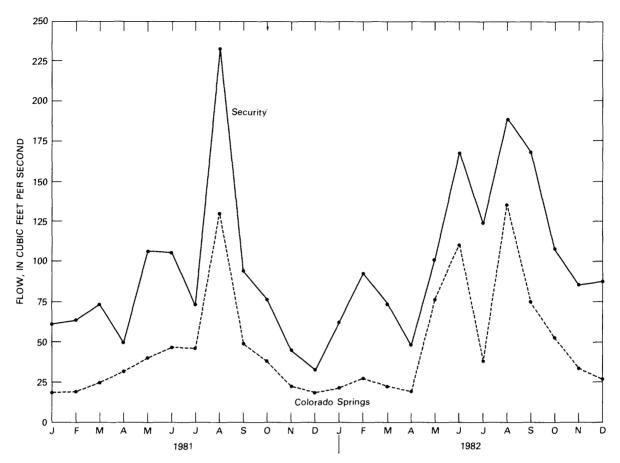


Figure 2.1-1.--Mean monthly flow at two sites on Fountain Creek during 1981 and 1982.

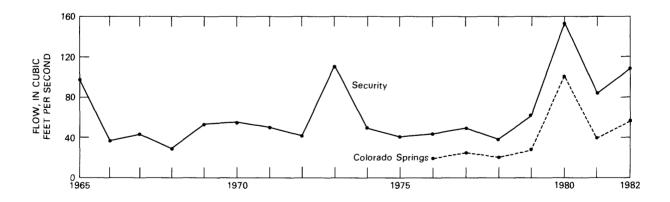


Figure 2.1-2.--Mean annual flow at two sites on Fountain Creek.

# 2.0 SURFACE WATER--Continued 2.2 Inflows and Diversions

 Water enters Fountain Creek from seven small tributaries and five sewage-treatment plants and is diverted by two major canals in the study area (fig. 2.0-1). These inflows and diversions affect both the quantity and quality of water in Fountain Creek and the quality of water in the Widefield aquifer.

Flow was measured quarterly during baseflow periods at six of the tributaries and continuously at B Ditch Drain near Security (site 16) during 1982 (table 2.0-1, fig. 2.2-1). Because the flow of B Ditch Drain was measured continuously, brief periods of heavy runoff that occurred during 11 days, that were not measured at the quarterly sites, are not included in the calculations of its mean. The mean flows shown in figure 2.2-1 provide a good representation of the flow on most days. As shown in figure 2.2-1, none of the tributaries contributed large quantities of flow to Fountain Creek.

Sewage-treatment plants contribute much more flow to Fountain Creek than tributaries (fig. 2.2-1). The largest amount of flow is contributed by the Colorado Springs Sewage Treatment Plant (site 3), near the upstream end of the study area (fig. 2.0-1). Increasingly smaller amounts are contributed by Fort Carson Sewage Treatment Plant, which flows into Clover Ditch Drain, and by the Security (site 18), Widefield (site 22), and Garden Valley (site 11) Sewage Treatment Plants. Flow from the Colorado Springs Sewage Treatment Plant varies somewhat from month to month (fig. 2.2-2), with flow slightly higher in the summer. Similar trends occur for other sewage-treatment plants in the area. Between 1965 and 1982, mean annual flow from the Colorado Springs Sewage Treatment Plant more than doubled, from about 18 ft<sup>3</sup>/s (cubic feet per second) to greater than 40 ft<sup>3</sup>/s (fig. 2.2-3). Long-term flow data from the other sewage-treatment plants are not available.

The amount and quality of flow in Canal No. 4 and Stubbs-Miller Ditch are important because both diversions provide water that recharges the Widefield aquifer. Canal No. 4 diverted a mean flow of 14.8 ft<sup>3</sup>/s and the Stubbs-Miller Ditch diverted a mean flow of 1.56 ft<sup>3</sup>/s from Fountain Creek during 1982 (fig. 2.2-1). The 1982 diversions were lower than the mean flows, probably because of the large amount of precipitation during the summer months (figs. 1.2-2 and 2.2-3). Mean monthly flows for both diversions during 1982 are shown in figure 2.2-2.

## 2.0 SURFACE WATER--Continued

# 2.3 Quantification of Sources of Water in Fountain Creek and Canal No. 4

Upstream from the study area, water in Fountain Creek originates from a variety of natural and man-affected sources. In this report, water in Fountain Creek at Colorado Springs (site 1 in fig. 2.3-1) plus the small flow of Shooks Run (site 2 in fig. 2.3-1) is considered as one upstream source of water. About one-fourth mile downstream from Shooks Run, the flow from the Colorado Springs Sewage Treatment Plant (site 3 in fig. 2.3-1) enters Fountain Creek. During 1982, the mean flow of the treatment plant was 40.1 ft<sup>3</sup>/s (cubic feet per second), compared to 54.4 ft<sup>3</sup>/s in Fountain Creek at Colorado Springs. The combined mean flow of 94.5 ft<sup>3</sup>/s in Fountain Creek just downstream from the treatment plant comprised 42 percent of the flow from the Colorado Springs Sewage Treatment Plant (fig. 2.3-1). Between 1977 and 1982, this percentage varied between 26 and 62 percent.

The percentage of annual flow contributed by the sewage-treatment plant does not clearly explain the plant's effect on flows in Fountain Creek, because short periods of heavy runoff in Fountain Creek greatly contribute to its annual flow, while flow from the sewage-treatment plant is relatively constant. Duration curves shown in figure 2.3-2 show the amount of time that specified percentages of flow contributed by the Colorado Springs Sewage Treatment Plant were equaled or exceeded. During 1982, 42 percent or more of Fountain Creek flow was contributed by the Colorado Springs Sewage Treatment Plant 67 percent of the time. Because of relatively high flow in Fountain Creek during 1982 (fig. 2.1-2), the duration curve for 1982 is shifted downward in relation to the 1977-82 curve (also shown in fig. 2.3-2).

About one-eighth mile downstream from the Colorado Springs Sewage Treatment Plant outfall, Canal No. 4 diverts water from Fountain Creek on the same bank. Because of the short distance, complete mixing of the flow from the plant and Fountain Creek does not occur. As a result, Canal No. 4 generally receives a higher percentage of flow from the Colorado Springs Sewage Treatment Plant than if complete mixing occurs. An estimate of the lack of mixing was made using ammonia as a tracer. The ratio of observed ammonia concentrations based on total mixing and expected ammonia concentrations at the headgate of Canal No. 4 was found to be directly proportional to the mean daily flow in Fountain Creek at Colorado Springs (fig. 2.3-3). The line shown in figure 2.3-3, which was developed by using the method of least-squares (correlation coefficient = 0.81), defines a mixing ratio with the equation:

MIXING RATIO = 0.0067Q + 1.01,

where Q = mean daily flow of Fountain Creek at Colorado Springs.

To estimate the actual percentage of flow in Canal No. 4 contributed by the Colorado Springs Sewage Treatment Plant, the mixing ratio is multiplied by the percentage of flow from the treatment plant effluent at the Canal No. 4 diversion point, assuming complete mixing.

The mixing ratio was tested in 1982 by using it to calculate expected ammonia concentrations in Fountain Creek below Janitell Road (site 10 in fig. 2.3-1) and comparing these to observed ammonia concentrations (fig. 2.3-4). Agreement between observed and expected ammonia concentrations was very good.

Using the mixing ratio and a mass balance, sources of flow in Fountain Creek and Canal No. 4 were calculated on a daily basis during 1982. Calculations were based on the mean daily flows at Fountain Creek at Colorado Springs, Colorado Springs Sewage Treatment Plant outfall, and Canal No. 4 headgate, and mean 1982 flows at Shooks Run and Spring Creek (fig. 2.2-1). Sources of flow are shown as annual mean percentages in figure 2.3-1, and as duration curves in figure 2.3-2. Sources of flow in Fountain Creek below Janitell Road (site 10 in fig. 2.3-1) are important because this is the upstream end of the losing reach of Fountain Creek that recharges the Widefield aquifer. Sources of flow throughout this reach will be similar because inflows are small (fig. 2.3-1).

During 1982, an estimated 38 percent of the flow of Fountain Creek in the reach that provides recharge to the Widefield aquifer and an estimated 57 percent of the flow in Canal No. 4 were contributed by the Colorado Springs Sewage Treatment Plant. During this same period, flow from this plant comprised more than one-half the flow in the losing reach of Fountain Creek about 50 percent of the time, and in Canal No. 4 about 60 percent of the time.

#### 3.0 GROUND WATER

The Widefield aquifer is a shallow, highly permeable alluvial aquifer in which the saturated thickness varies with time and location but averages 30 to 35 feet. A significant part of the approximately 18,000 acre-feet of water in storage is withdrawn by wells each year. Thirty-three of the 50 municipal wells and 8 irrigation wells in the area are currently in use (fig. 3.0-1).

Amount and type of water use has changed significantly in the last 40 years (fig. 3.0-2). Between 1942 and 1950, a mean of 1,160 acre-feet of water was withdrawn from the aquifer, primarily for irrigation purposes (Livingston and others, 1976b, p. 51). Development of the ground-water system for municipal and industrial use began in 1951; pumpage for these uses began increasing in 1954, as population in the area increased because of expansion of Fort Carson. Since 1960, population has increased at a mean rate of about 1,000 people per year. As the area has become increasingly urbanized, ground water primarily has been used for municipal purposes. During the past 10 years, annual mean pumpage has been about 7,100 acre-feet; only about 9 percent, or 640 acre-feet, has been for irrigation use. During 1982, only about 7 percent, or 400 acre-feet of the total 5,400 acre-feet withdrawn, was for irrigation use; about 1,100 acre-feet were exported to Colorado Springs. Decreases in total pumpage and in the amount used for irrigation that occurred during 1982 were the result of the large and relatively constant amount of precipitation that occurred during the summer of 1982 (fig. 1.2-2).

Ground water in the Widefield aquifer flows naturally to the southeast (fig. 3.0-1). However, during periods of intense pumpage, localized depressions in the water table may occur, resulting in some temporary northward movement. The mean rate of water movement through the Widefield aquifer is dependent on hydraulic conductivity, hydraulic gradient, and effective porosity. In the Widefield aquifer, hydraulic conductivity, which is a measure of the volume rate of flow through a unit cross-sectional area, ranges from 670 to 1,140 feet per day (Wilson, 1965, p. 75-78; R.A. Hogan, W.W. Wheeler and Associates, written commun., 1983). Based on available U.S. Geological Survey data, a mean hydraulic conductivity for the Widefield aquifer is 830 feet per day. Hydraulic gradient in an alluvial aquifer is the slope or change in altitude of the water table over some specified distance in a given direction; it is about 0.006 for the area. Effective porosity is the interconnected pore space; for the purposes of this report, effective porosity is assumed to approximate specific yield. Specific yield is the ratio of the volume of water that a water-saturated material will yield by gravity to its own volume. Jenkins (1964, p. 23) noted that specific yield varied from 20 to 30 percent in the alluvial aquifer; he selected a value of 25 percent for all computations using specific yield.

As hydraulic properties of the aquifer change, the rate of movement of water through the aquifer changes. The mean rate of movement of water through the Widefield aquifer is about 20 feet per day, or 1.4 miles per year, assuming a gradient of 0.006, a hydraulic conductivity of 830 feet per day, and an effective porosity of 25 percent. Actual rate of movement of water through the Widefield aquifer varies with time and location, and may range from 13 to 34 feet per day (0.9 to 2.4 miles per year).

Water moves into the Widefield aquifer from: (1) Fountain Creek; (2) underflow from Fountain Creek alluvium north of the Widefield aquifer; (3) underflow from tributary alluvium; and (4) deep percolation from precipitation, irrigation, ponds, and lagoons overlying the aquifer. Water moves out of the Widefield aquifer to: (1) Fountain Creek; (2) Fountain Creek alluvium south of the Widefield aquifer; and (3) various locations, by pumpage of wells completed in the Widefield aquifer.

3.1 Inflows to the Widefield Aquifer
3.1.1 Recharge from Fountain Creek

Fountain Creek traverses the alluvial aquifer throughout the study area, and crosses the north end of the Widefield aquifer between sites 1 and 2 (fig. 3.1.1-1). Livingston and others (1976a, p. 64 and 1976b, p. 57-60) determined that Fountain Creek recharged the aquifer in a 3-mile reach of Fountain Creek, extending downstream from the confluence with Spring Creek (site 1, fig. 3.1.1-1) to downstream from the headgate of the Stubbs-Miller Ditch (site 2, fig. 3.1.1-1). The cross section of the alluvial aquifer shown in figure 3.1.1-1 depicts the thickness of alluvium underlying Fountain Creek north of the Widefield aquifer, and typifies the relationship between a losing stream and the underlying aquifer.

Between 1973 and 1977, the quantity of water interchanged between Fountain Creek and the aquifer was determined by 14 gain-loss investigations. A gain-loss investigation is an accounting of all surface water entering or leaving specified reaches of a stream; the investigation ideally is conducted during periods of relatively stable streamflow conditions. Differences in flow that cannot be accounted for by tributary inflow or by diversions are attributed to an interchange between ground and surface water. During many of the 14 gain-loss investigations, significant diurnal variations in flow occurred in a 3-mile reach between sites 1 and 2, and in a 4.2-mile reach between sites 2 and 3 (fig. 3.1.1-1), as a result of fluctuations in flow from the Colorado Springs Sewage Treatment Plant. Because of these fluctuations, it was necessary to adjust the original data (U.S. Geological Survey, 1974, p. 389-393; and 1978, p. 378-382), using estimates of time of travel, time of instantaneous flow measurements, and continuous flow records at the Security gaging station (site 3, fig. 3.1.1-1). During 4 of the 14 gain-loss investigations, poor flow records at the Security gage, coupled with inappropriate timing of flow measurements in the 3-mile reach between sites 1 and 2, prevented an accurate adjustment of the data. Adjusted gain-loss data for the 3-mile reach, based on the 10 remaining gain-loss runs, are summarized in table 3.1.1-1. A mean loss of 11 ft<sup>3</sup>/s (cubic feet per second), or about 8,000 acre-ft/yr (acre-feet per year), occurred between sites 1 and 2.

Table 3.1.1-1.--Summary of gain-loss investigations for losing reach of Fountain Creek in the study area

| Date               | Gain-loss <sup>1</sup><br>(cubic feet<br>per second) | Date               | Gain-loss <sup>1</sup><br>(cubic feet<br>per second) |
|--------------------|--|--------------------|--|
| July 26, 1973      | 3.0  | June 29, 1976      | -21.2  |
| September 6, 1973  | -16.4  | November 9, 1976   | -15.4  |
| October 31, 1973   |  | May 9, 1977        | 1.1  |
| September 26, 1974 | -14.8  | July 18, 1977      | <del>-</del> 7.7                                     |
| August 26, 1975    |  | September 27, 1977 | -3.6   |

<sup>1</sup>Positive number indicates amount of water gained by the stream. Negative number indicates amount of water lost to ground water.

At any given time, the actual amount of interchange between the stream and the aquifer in this 3-mile reach may vary significantly from an average  $11-ft^3/s$  loss. The actual amount of water lost to the aquifer is dependent on the hydraulic-head difference between the aquifer and the stream, and the hydraulic properties of the aquifer (Livingston and others, 1976a, p. 64). Emmons (1977, p. 38) noted that no significant long-term water-level changes occurred in the aquifer, although withdrawals from the aquifer had increased. He also stated that the stream-aquifer system was apparently in equilibrium. Since 1963, withdrawals have become more stable (fig. 3.0-1), and no changes in the hydrologic system that would have affected the stream-aquifer relationship in this reach have occurred. Because of this stability, the mean loss of  $11 \text{ ft}^3/s$ , based on adjusted gain-loss data for 1973 to 1977, should be a reasonable estimate of the stream-aquifer relationship; this mean is used to compute the amount of recharge from Fountain Creek in this report.

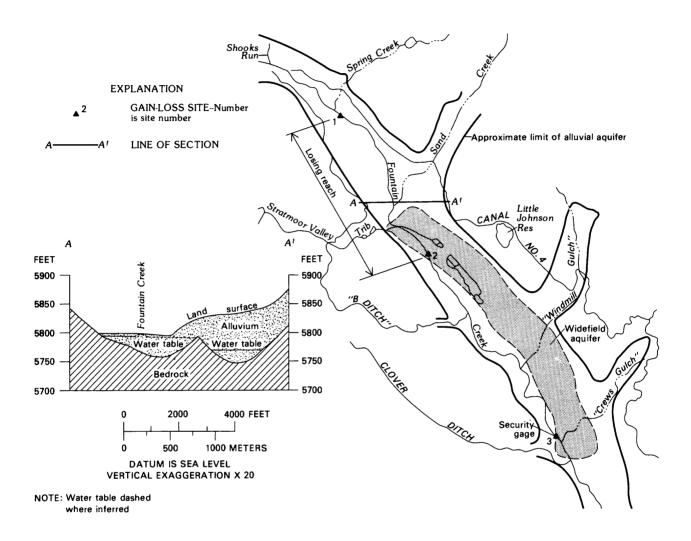


Figure 3.1.1-1.--Cross section of Fountain Creek alluvium showing altitude of the water table in the losing reach of Fountain Creek in the study area.

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3.1 Inflows to Widefield Aguifer -- Continued

3.1.2 Underflow from Fountain Creek Alluvium and Tributary Alluvium

The Widefield aquifer receives ground-water inflow from Fountain Creek alluvium, north of the aquifer, and from tributary alluvium, east and west of the aquifer. Ground-water inflow or underflow may be approximated by using a modified form of Darcy's law, expressed as:

$$Q = KIA$$

where Q = quantity of water passing through a cross section, in cubic feet per day;

K = hydraulic conductivity, in feet per day;

I = hydraulic gradient (dimensionless); and

A = cross-sectional area (width times saturated thickness), in feet squared.

Underflow from Fountain Creek alluvium enters the Widefield aquifer in the vicinity of the confluence of Sand Creek and Fountain Creek. In this area, ground water consists of surface-water losses from Fountain Creek, seepage from Canal No. 4, underflow from Sand Creek alluvium, and water originating in Fountain Creek alluvium north of Highway 29. For the purposes of this report, it was desirable to evaluate each inflow independently; the cross section selected for approximating underflow from Fountain Creek alluvium, exclusive of underflow from Sand Creek and water lost from Fountain Creek and Canal No. 4, is located north of Highway 29 (cross section A-A', fig. 3.1.2-1). Underflow at this point from Fountain Creek alluvium is about 84,000 ft<sup>3</sup>/d (cubic feet per day), or 700 acre-ft/yr (acre-feet per year) (table 3.1.2-1).

Water enters the Widefield aquifer from the east as underflow from Sand Creek alluvium, Windmill Gulch alluvium, and Crews Gulch alluvium, and from saturated eolian deposits that are recharged by leakage from Canal No. 4. Underflows from tributary alluvium east of the Widefield aquifer are shown in figure 3.1.2-1 and table 3.1.2-1. Because only one well is completed in the Crews Gulch alluvium, underflow could not be calculated directly, so it was estimated from its similarity to Windmill Gulch. Calculation of Crews Gulch underflow assumed: (1) Width equals 1,500 feet (fig. 3.1.2-1); (2) mean saturated thickness equals 10 feet; (3) hydraulic gradient equals the land-surface gradient of 0.014 (hydraulic gradient on the Windmill Gulch area equals land-surface gradient); and (4) hydraulic conductivity is the same as hydraulic conductivity in the Windmill Gulch area, approximately 50 feet per day. These assumptions result in an estimated underflow of 90 acre-ft/yr from Crews Gulch. Most of the underflow to the Widefield aquifer from the east is from saturated eolian deposits, with an estimated underflow of 720 acre-ft/yr. Two gain-loss investigations that were conducted on Canal No. 4 during 1982 indicate that Canal No. 4 loses water to underlying material. The cumulative flow gains and losses along Canal No. 4 on September 29, 1982, are shown in figure 3.1.2-2. Assuming a 2-ft<sup>3</sup>/s (cubic feet per second) loss of canal water on the 223 days the canal flowed during 1982, 880 acre-feet of water was lost from the canal to eolian deposits in the reach between Sand Creek and Windmill Gulch, indicating that canal seepage was the probable source of most recharge to ground water in eolian deposits.

A small amount of water enters the Widefield aquifer from the west as underflow from Stratmoor Valley tributary alluvium, B Ditch alluvium, and Clover Ditch alluvium (fig. 3.1.2-1, table 3.1.2-1). The remaining area west of the aquifer is Pierre Shale, which is considered to be impermeable. Underflow from Stratmoor Valley tributary is estimated to be about 5 acre-ft/yr, assuming a saturated area of 10,000 square feet, and hydraulic properties the same as B Ditch.

3.1 Inflows to the Widefield Aguifer -- Continued

3.1.3 Recharge from Land Surface

Recharge from land surface to the Widefield aquifer occurs through infiltration and percolation of precipitation and irrigation water, artificial recharge at the Pinello Ranch, and seepage from sewage lagoons and septic tanks.

Precipitation and lawn- and agricultural-irrigation water percolate downward and recharge the aquifer. The amount of recharge is dependent on: (1) Amount of precipitation and irrigation, (2) soil-moisture storage capacity, and (3) amount of evapotranspiration. Estimates of recharge were made separately for residential and agricultural areas and are shown in tables 3.1.3-1 and 3.1.3-2.

The amount of deep percolation from precipitation and lawn and agricultural irrigation that occurred monthly during 1982 was estimated from the following equation:

$$R = Rt - Re + I - Ir - Ru$$

where R = Recharge or deep percolation, in inches;

Rt = total precipitation measured at Pinello Ranch, in inches;

Re = effective precipitation, that is, the part of precipitation that remains in the soil profile and is available for consumptive use, in inches (U.S. Soil Conservation Service, 1967, p. 27);

I = irrigation, in inches;

Ru = runoff, in inches.

Each component in the equation is quantified in tables 3.1.3-1 and 3.1.3-2.

During 1982, an estimated 1,000 acre-feet of the approximately 2,000 acre-feet of precipitation and irrigation water applied to the 435 acres of lawns that overlie the aquifer percolated beneath the root zone and recharged the aquifer.

In addition to lawns overlying the aquifer, three agricultural areas exist, totaling approximately 286 acres. Alfalfa was grown on about 127 acres; corn was grown on most of the remaining 159 acres. The resulting amount of recharge to the aquifer from agricultural areas was estimated to be 1,200 acre-feet of the estimated 1,900 acre-feet of precipitation and irrigation water that was applied to the agricultural areas during 1982.

Pinello Ranch artificial-recharge ponds are a source of recharge to the aquifer. The Pinello Ranch is located at the north end of the Widefield aquifer. Water in the ponds is diverted from Fountain Creek via Stubbs-Miller Ditch. During 1982, the amount of recharge to the aquifer from the recharge ponds was estimated by using inflow records, observed changes in storage, and monthly evaporation. Monthly evaporation was estimated from an estimated annual evaporation of 60 inches (Hansen and others, 1978, p. 33), multiplied by ratios of monthly to total evaporation measured during 1982 at Pueblo Reservoir, which is about 5 miles west of Pueblo, Colo., and about 35 miles south of the study area (National Oceanic and Atmospheric Administration, 1982, p. 21). During 1982, an estimated 180 acre-feet of water from Pinello Ranch recharge ponds percolated to the water table.

Two sewage-treatment plants operate sewage lagoons that overlie the aquifer and are potential sources of recharge. Sewage lagoons at the Security Sewage Treatment Plant have clay liners that were reported to be intact (Richard Gilham, Security Wastewater Division, oral commun., 1982). Influent and effluent records are not accurate enough to estimate recharge to the aquifer from leakage through clay liners; however, the influent and effluent records suggest that, if leakage does occur, it is likely to be small. Sewage lagoons at the Widefield Sewage Treatment Plant are not lined; leakage is likely to occur. Insufficient data exist to accurately estimate the amount of water percolating to the water table. However, the amount may be greater than the 180 acre-feet that was estimated to recharge the aquifer from Pinello Ranch recharge ponds, because of greater surface area and volume of the Widefield lagoons.

Approximately 10 septic systems, servicing an estimated 20 people, exist in the area. Assuming a per capita flow of 40 gallons per day (Porter, 1980, p. 618), approximately 1 acre-ft/yr (acre-feet per year) of water from septic systems is available for recharge.

3.2 Outflows from the Widefield Aquifer
3.2.1 Discharge to Fountain Creek

Fountain Creek crosses the Widefield aquifer only at its western and eastern ends (fig. 3.2.1-1). Jenkins (1964) indicated that a buried shale "ridge" separated Fountain Creek from the Widefield aquifer in the area where Fountain Creek parallels the aquifer. However, Livingston and others (1976a, p. 64; and 1976b, p. 57-60) indicated that the shale barrier was not as significant as previously thought. The cross sections in figure 3.2.1-1 illustrate that Fountain Creek and the thin alluvial deposits underlying Fountain Creek are hydraulically connected to the Widefield aquifer throughout most of the area. Overall, the 4.2-mile reach extending from the Stubbs-Miller Ditch to the Security gage is generally a gaining reach; that is, the stream gains water from the aquifer. However, at times, the stream may lose water to the aquifer, as indicated by cross section B-B' (fig. 3.2.1-1). Because the altitude of the stream and aquifer appears to be similar, small changes in the altitude of the stream or water table could alter the direction and amount of movement of water between the stream and aquifer.

The amount of water interchanged between Fountain Creek and the Widefield aquifer was determined by means of 14 gain-loss investigations performed between 1973 and 1977. Because of significant diurnal variations in flow that occurred during the gain-loss investigations, it was necessary to adjust the original data (U.S. Geological Survey, 1974, p. 389-393; and 1978, p. 378-382) using estimates of time of travel, time of instantaneous-flow measurements, and flow records at the Security gage (site 3, fig. 3.2.1-1). During 3 of the 14 gain-loss investigations, accurate adjustments could not be made, either because of the time of flow measurements in the 4.2-mile reach between sites 2 and 3, or because of the inadequate record at the Security gage. Adjusted gain-loss data for the 4.2-mile reach, based on the remaining 11 gain-loss runs, are summarized in table 3.2.1-1. A mean gain of 3.2 ft<sup>3</sup>/s (cubic feet per second) occurred between sites 2 and 3. This mean gain is equivalent to a 2,300-acre-ft/yr (acre-feet per year) loss of water from the Widefield aquifer to Fountain Creek.

At any given time, the actual amount of interchange between Fountain Creek and the Widefield aquifer in this 4.2-mile reach may vary significantly from the mean 3.2-ft<sup>3</sup>/s gain, primarily as a result of hydraulic-head difference between the aquifer and the stream. Because no long-term changes in the hydrologic system have occurred, the mean gain of 3.2 ft<sup>3</sup>/s to Fountain Creek should be a reasonable estimate of the stream-aquifer relationship in this reach. However, because of the high water table that occurred during 1982, the amount of water that the stream gained from the aquifer was likely to have been greater than the mean 3.2 ft<sup>3</sup>/s.

Table 3.2.1-1.--Summary of gain-loss investigations for the gaining reach of Fountain Creek in the study area

| Date                                  | Gain-loss <sup>1</sup><br>(cubic feet<br>per second) | Date               | Gain-loss <sup>1</sup><br>(cubic feet<br>per second) |
|---------------------------------------|--|--------------------|--|
| July 26, 1973                         | 13.3   | June 29, 1976      | 2.6  |
| September 6, 1973                     | 7.6  | November 9, 1976   | 3.3  |
| October 31, 1973                      | 5.0  | May 9, 1977        | -7.2   |
| June 14, 1974                         | 14.8   | July 18, 1977      | .1   |
| September 26, 1974<br>August 26, 1975 | 1.7<br>7.9   | September 27, 1977 | -13.5  |

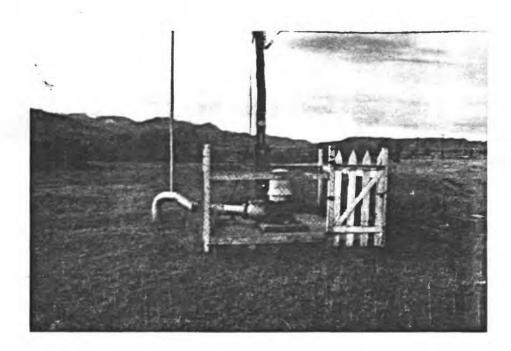
<sup>&</sup>lt;sup>1</sup>Positive number indicates amount of water gained by the stream. Negative number indicates amount of water lost to ground water.

3.2 Outflows from the Widefield Aquifer--Continued
3.2.2 Underflow to Fountain Creek Alluvium and Ground-Water Withdrawals

Water in the aquifer moves generally southeastward through the alluvium, and water leaves the study area at the southeastern boundary at a rate of about 2,500 acre-ft/yr (acre-feet per year). The amount of underflow leaving the area was estimated by using a cross-sectional area of 90,000 square feet (fig. 3.2.2-1), a hydraulic gradient of 0.005, and a hydraulic conductivity of 670 feet per day (R.A. Hogan, W.W. Wheeler and Associates, written commun., 1983).

The largest outflow of water from the Widefield aquifer is through pumpage of wells. During the past 10 years, annual mean pumpage has been about 7,100 acre-feet; from 30 to 40 percent of the water in storage has been withdrawn each year. Yet, water levels throughout the aquifer indicate rapid recovery and no lasting effects (fig. 3.2.2-2). Jenkins (1964, p. 54) observed that the water table recovered more rapidly in the northern part of the aquifer than the southern part, presumably because of recharge from Fountain Creek as it crosses the north end of the aquifer. A comparison of the hydrographs in figure 3.2.2-2 illustrates the effects of pumpage on the water table in the northern, middle, and southern parts of the aquifer. Because of extensive pumpage in the middle of the aquifer, larger water-level fluctuations occur in the middle aquifer than in either the northern (Stratmoor Hills-5 well) or southern (U.S. Geological Survey observation well) parts of the aquifer as illustrated by wells Pinello-1 and Venetucci-8.

Because 1982 was a wet year, only 5,400 acre-feet of water were withdrawn from the aquifer. Due to smaller withdrawals, the water table was generally higher in 1982 than during previous years, resulting in an increase in the amount of ground-water storage. Between December 1981 and December 1982, the change in water levels observed at 26 sites ranged from a decrease of 2 feet to an increase of 7 feet. Mean water-level change in the aquifer was an increase of about 3 feet. Using an area-weighted mean water-level change of 2.7 feet, an aquifer area of 3.5 square miles, and a specific yield of 0.25, an estimated 1,500 acre-feet increase in ground-water storage occurred during 1982.



A municipal well located on the Pinello Ranch, which is used to export water to the city of Colorado Springs.



Artificial recharge ponds located on the Pinello Ranch.

# 3.3 Summary of Inflows and Outflows

Inflows to the Widefield aquifer and outflows from the aquifer are summarized in table 3.3-1. A ground-water budget for 1982 was not computed because the data used to estimate inflows and outflows were from different time periods. However, the total of the inflows minus the actual change in storage is within 5 percent of the total of the outflows, which indicates that estimates for the inflows and outflows are reasonable.

INFLOWS: The major inflow to the Widefield aquifer is from Fountain Creek. Recharge from Fountain Creek to the aquifer was based on 10 gain-loss investigations performed between 1973 and 1977; recharge was estimated to be 8,000 acre-ft/yr (acre-feet per year). Underflow from Fountain Creek alluvium to the Widefield aquifer at a cross section located near Highway 29 was estimated to be 700 acre-ft/yr. Underflow from tributary alluvium to the Widefield aquifer was estimated to be 318 acre-ft/yr. An estimated 720 acre-ft/yr entered the aquifer as underflow from eolian deposits located east of the aquifer. Recharge to the ground water in this area was primarily from Canal No. 4. During 1982, approximately 2,200 acre-feet of water recharged the aquifer from precipitation, lawn irrigation, and agricultural irrigation. The Pinello Ranch recharge ponds contributed an estimated 180 acre-feet of water to the aquifer during 1982. Some seepage from sewage lagoons occurs in the area, but it was not possible to confidently estimate the amount. Because of a lack of clay liners, it is probable that there is more recharge from lagoons at the Widefield Sewage Treatment Plant than the Security Sewage Treatment Plant, which reportedly has clay-lined lagoons. Septic tanks in the area may contribute as much as 1 acre-ft/yr of water to the aquifer. OUTFLOWS: A significant amount of ground water flows to Fountain Creek in the 4.2-mile reach where the stream flows adjacent to the aquifer. Based on 11 gain-loss investigations performed between 1973 and 1977, the Widefield aquifer loses an estimated 2,300 acre-ft/yr to Fountain Creek. An estimated 2,500 acre-ft/yr of ground water flows out of the study area to the southeast. The largest outflow is

7,100 acre-feet. However, because of larger than normal precipitation during 1982, annual pumpage was only 5,400 acre-feet.

Table 3.3-1.--Summary of inflows and outflows, Widefield aquifer, 19821

withdrawal of ground water by pumpage. During the past 10 years, annual mean pumpage has been about

| Name of inflow             | Inflow<br>(acre-feet) | Name of outflow      | Outflow (acre-feet) |
|----------------------------|-----------------------|----------------------|---------------------|
| Fountain Creek             | 8,000                 | Fountain Creek       | 2,300               |
| Fountain Creek alluvium    | 700                   | Ground-water outflow | 2,500               |
| Sand Creek alluvium        | 28                    | Ground-water pumpage | 5,400               |
| Windmill Gulch alluvium    | 200                   |                      | •                   |
| Crews Gulch alluvium       | 90                    |                      |                     |
| Eolian deposits            | 720                   |                      |                     |
| Stratmoor Valley tributary | 5                     |                      |                     |
| B Ditch alluvium           | 3                     |                      |                     |
| Clover Ditch alluvium      | <1                    |                      |                     |
| Precipitation and lawn     |                       |                      |                     |
| irrigation                 | 1,000                 |                      |                     |
| Precipitation and agricul- |                       |                      |                     |
| tural irrigation           | 1,200                 |                      |                     |
| Pinello Ranch recharge     |                       |                      |                     |
| ponds                      | 180                   |                      |                     |
| Sewage lagoons             | Unknown               |                      |                     |
| Septic tanks               | 1                     |                      |                     |
| TOTAL2                     | 12,100                |                      | 10,200              |

<sup>&</sup>lt;sup>1</sup>Estimated 1982 change in storage equals 1,500 acre-feet.

<sup>&</sup>lt;sup>2</sup>Total rounded to nearest 100 acre-feet.

#### 4.0 NITROGEN FORMS AND TRANSFORMATIONS

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Nitrogen occurs in the hydrologic environment in several forms, which may be stable or reactive depending on the environmental conditions. Many of the reactions between nitrogen forms require specific bacteria which use the energy released in the reaction. Important nitrogen forms and potential nitrogen-transformation reactions are shown in figure 4.0-1.

During the study, nitrogen was analyzed using methods described in Skougstad and others (1979). Nitrogen analyses of surface water were made on whole (unfiltered) water samples and were expressed as total nitrogen, while ground-water samples were filtered through a 0.45-micron membrane filter before analysis, and were expressed as dissolved nitrogen. All samples were collected in opaque bottles, preserved by addition of mercuric chloride, and chilled to 4°C before shipment to the Denver Central Laboratory of the U.S. Geological Survey for analysis. The total or dissolved forms of nitrogen analyzed included: (1) Ammonia, which includes both ammonium (NH<sub>4</sub>+) and nonionized ammonia (NH<sub>3</sub>); (2) Kjeldahl nitrogen, which includes both ammonia and organic nitrogen; (3) organic nitrogen, which is determined by subtracting ammonia from Kjeldahl nitrogen; (4) nitrite; (5) nitrite plus nitrate; (6) nitrate, which is determined by substracting nitrite from nitrite plus nitrate; and (7) total or dissolved nitrogen, which is determined by adding Kjeldahl nitrogen and nitrite plus nitrate. All nitrogen concentrations in this report are expressed as the equivalent amount of nitrogen.

Because of the municipal wastewater flow into Fountain Creek, ammonia ( $\mathrm{NH}_3$ ) and ammonium ( $\mathrm{NH}_4$ +), with which it is in equilibrium, are the most abundant nitrogen forms in Fountain Creek and canals which divert water from it. Ammonia may be lost from surface water by volatilization into the atmosphere and through uptake by aquatic plants. Ammonium may react to the unstable intermediate nitrite, and then to nitrate in surface water in a process called nitrification, since adequate dissolved oxygen is generally present. Nitrate and ammonia may be used by both floating and attached aquatic plants (Kittrell, 1969), but because of short residence time of surface water and the shifting sand channel in Fountain Creek and Canal No. 4, few plants are observed, and little nitrate or ammonia are likely to be consumed in this way. However, nitrate or ammonia uptake by aquatic plants may be important in the Pinello Ranch recharge ponds and in some streams tributary to Fountain Creek.

During the process of infiltration and percolation to ground water, nitrogen in the water of streams, canals, sewage lagoons, septic tanks, artificial recharge ponds, and applied irrigation water may undergo several transformations. Ammonia in percolating water may be reversibly adsorbed onto cation-exchange sites of clays in soil or alluvial deposits (Keeney, 1981, p. 261). Adsorbtion will retard the ammonia movement until available exchange sites are filled (Lance and Whistler, 1972). Ammonia in water applied to soils may also volatilize back to the atmosphere, the amount depending on the amount of calcium carbonate in the soil and soil pH (Ryden, 1981). If oxygen and nitrosomonas and nitrobacter bacteria are present, ammonia in water moving through soil may react to form nitrate through the process of nitrification. The reaction should be essentially complete during warm months in the top inch of soil (Lance, 1972; Bouwer and others, 1974). Nitrate is not subject to adsorbtion onto clays and generally will be stable in the unsaturated zone if oxygen is present. If oxygen is not present (anaerobic conditions), nitrate may undergo denitrification to nitrogen gas or nitrousoxide gas or reduction to ammonium. Denitrification is believed to be preferred over reduction, except in organic-rich soils (Reddy and others, 1980). Denitrification requires the absence of oxygen and proceeds most rapidly at temperatures of 20° to 35°C (Broadbent and Clark, 1965) and at neutral to slightly alkaline pH (Focht and Verstraete, 1977). However, it is believed that nitrification and denitrification may occur simultaneously in close proximity, because nitrification may proceed at small oxygen concentrations that allow for micro-anaerobic zones where denitrification may take place (Broadbent and others, 1977). Additionally, both nitrate and ammonia, when present in the root zone, may be used by plants.

Once infiltrating water has reached the ground-water table, some of the same transformations that occur in the unsaturated zone may occur. Aerobic conditions will promote nitrification of any remaining ammonia to nitrate while anaerobic conditions will favor denitrification, and nitrate will be lost from the system as nitrogen gas or nitrous-oxide gas, or nitrate may be reduced to ammonium. Ammonium may be adsorbed onto clays under either aerobic or anaerobic conditions.

Nitrogen in ground water in the study area is generally present primarily as nitrate. Only small concentrations [less than 0.3 mg/L as N (milligrams per liter as nitrogen)] of ammonia and even smaller concentrations of nitrite generally are observed, suggesting that nitrification of ammonia in recharge water is mostly complete before the water enters the ground-water system. The amount of denitrification which occurs will be determined by: (1) The absence of dissolved oxygen, and (2) the availability of carbon.

## 5.0 SURFACE-WATER QUALITY

# 5.1 Fountain Creek

The water in Fountain Creek changes in quality as a result of inflows from the study area. These observed changes are especially large for nitrogen forms as shown for three sites on Fountain Creek during 1982 in figure 5.1-1 and in table 11.0-1 (Supplemental Information section).

At site 1, Fountain Creek at Colorado Springs, mean total nitrogen in monthly samples was 2.4 mg/L as N (milligrams per liter as nitrogen) during 1982, similar to the mean value of 2.6 mg/L as N, based on 36 samples collected since 1975. About 60 percent of the total nitrogen during 1982 was present as total nitrite plus nitrate (1.4 mg/L as N), with most of the remainder total organic nitrogen. This nitrogen reflects upstream municipal wastewater flows and return flows. Seasonal variations during 1982 are related to higher streamflow in the summer months (fig. 2.1-1).

The next downstream site, Fountain Creek below Janitell Road (site 10), is downstream from two small tributaries and the Colorado Springs Sewage Treatment Plant. During 1982, the observed mean total nitrogen concentration was 12.5 mg/L as N, approximately five times the concentration at site 1, upstream. During the period since 1975, 40 samples analyzed for total nitrogen at this site gave a mean concentration of 15.5 mg/L as N. The smaller mean concentration during 1982 probably resulted from higher natural flows in Fountain Creek, which diluted nitrogen discharged by the Colorado Springs Sewage Treatment Plant. About two-thirds of the total nitrogen present at Fountain Creek below Janitell Road (site 10) was in the form of total ammonia during 1982, with most of the rest present as total organic nitrogen. Concentrations of total nitrite plus nitrate at this site were slightly smaller than at site 1, because water entering Fountain Creek from the Colorado Springs Sewage Treatment Plant generally contained less total nitrite plus nitrate than Fountain Creek. Large seasonal variations in total nitrogen concentrations at this site are the result of seasonal variations in the flow of Fountain Creek which was available to dilute relatively constant nitrogen inputs from the Colorado Springs Sewage Treatment Plant.

The quality of water in Fountain Creek below Janitell Road is important, because this is the upstream end of the reach that provides most recharge to the Widefield aquifer. The following comparison of total nitrogen concentrations in water collected from Fountain Creek below Janitell Road and at the Stubbs-Miller Ditch headgate near the downstream end of the recharging reach indicates that little change in total nitrogen concentrations occurs in this reach:

| Site                 | Date     | Concentration<br>Total Kjel-<br>dahl mitrogen | Total | s per liter as<br>Total nitrite<br>plus nitrate | Total |
|----------------------|----------|---|-------|---|-------|
| Fountain Creek below | 3-24-82  | 17.0  | 13.0  | 0.94  | 18.0  |
| Janitell Road.       | 12-15-82 | 15.0  | 13.0  | 1.2   | 16.0  |
| Stubbs-Miller Ditch  | 3-24-82  | 16.9  | 12.0  | 1.1   | 17.0  |
| at headgate.         | 12-15-82 | 17.5  | 12.0  | 1.5   | 18.0  |

Fountain Creek below Widefield, site 23, is located at the downstream end of the study area. Water quality at this site is affected by inflows from additional small tributaries and outfalls from four smaller sewage treatment plants. In addition, flow from ground water to Fountain Creek in its gaining reach also may affect water quality. During 1982, the mean total nitrogen concentration of 11 mg/L as N observed at this site decreased from 12.5 mg/L as N at site 10 (Fountain Creek below Janitell Road). About one-half the total nitrogen concentration at this site during 1982 was ammonia, with approximately equal amounts of organic nitrogen and nitrite plus nitrate comprising the remainder. Changes in the relative proportion of the nitrogen forms and the decrease in total nitrogen concentration between sites 10 and 23 probably can be attributed primarily to a combination of nitrification of ammonia to nitrate, ammonia volatilization, and inflows of ground water with relatively large concentrations of total nitrite plus nitrate.

# **EXPLANATION**

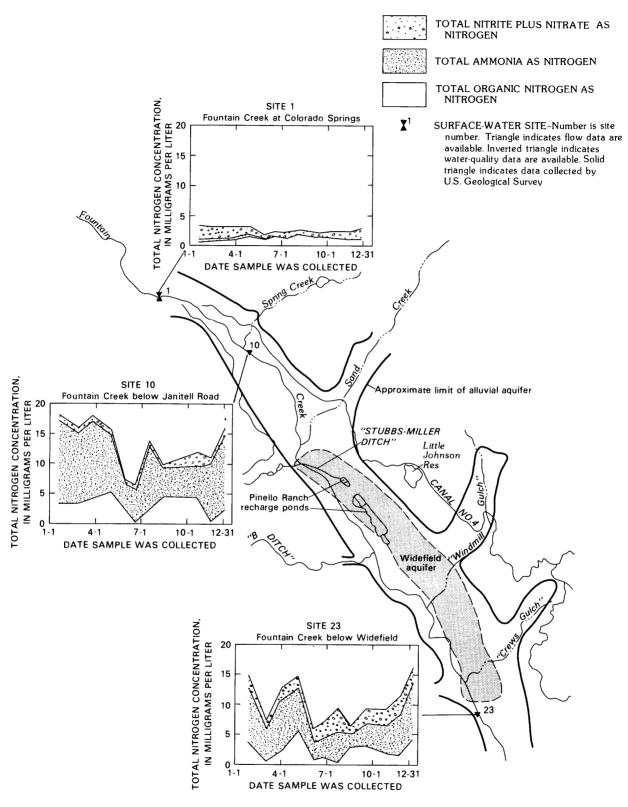


Figure 5.1-1.--Downstream and seasonal variations in total nitrogen concentrations of Fountain Creek, 1982.

## 5.0 SURFACE-WATER QUALITY--Continued 5.2 Inflows and Diversions

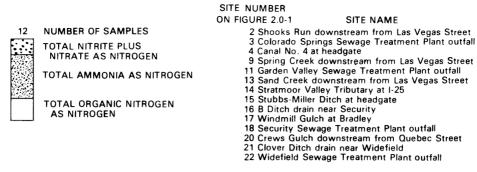
Mean concentrations of various nitrogen forms in inflows and diversions in the study area during 1982 are shown in figure 5.2-1 and in table 11.0-1 (Supplemental Information section). Concentrations of total nitrogen in the inflows are the largest at sites 3 (Colorado Springs Sewage Treatment Plant outfall), 11 (Garden Valley Sewage Treatment Plant outfall), 18 (Security Sewage Treatment Plant outfall), 21 (Clover Ditch drain near Widefield), and 22 (Widefield Sewage Treatment Plant outfall). Concentrations of total organic nitrogen were not routinely measured at sites 3, 18, and 22, but they were estimated to be 15 percent of measured total ammonia nitrogen concentrations, based on analyses of 42 samples during 1980-83 from the Colorado Springs Sewage Treatment Plant (Max Grimes, Laboratory Manager, Wastewater Division, Colorado Springs Department of Public Utilities, oral commun., 1984). Ammonia nitrogen is the dominant nitrogen form in water at all of these sites, except site 11, Garden Valley Sewage Treatment Plant outfall, where nitrite plus nitrate dominates, indicating that during 1982 this plant was nitrifying most ammonia to nitrite plus nitrate prior to discharge to Fountain Creek.

Concentration of total nitrogen and distribution of different nitrogen forms varied widely in tributary inflows (fig. 5.2-1). At sites 2 (Shooks Run), 9 (Spring Creek), 13 (Sand Creek), 14 (Stratmoor Valley tributary), and 16 (B Ditch), mean total nitrogen concentrations ranged from about 5 to 12 mg/L as N (milligrams per liter as nitrogen) with nitrite plus nitrate the dominant nitrogen form. At sites 17 (Windmill Gulch) and 20 (Crews Gulch), mean total nitrogen concentrations were less than 3 mg/L as N, with organic nitrogen the dominant form. Nitrite plus nitrate in these small tributaries may be used by aquatic plants upstream from the sampling sites.

Concentration and distribution of nitrogen forms in the two diversions--Canal No. 4 (site 4) and Stubbs-Miller Ditch (site 15)--reflect the quality of water found in Fountain Creek at their respective diversion points. Water at both of these points is similar in quality to that found in Fountain Creek below Janitell Road.

Seasonal variations in concentration and distribution of nitrogen species occurred in all inflows and diversions during 1982. Because the flow is small at these sites with the exception of the Colorado Springs Sewage Treatment Plant, even large seasonal water-quality variations did not have a major effect on the quality of water in Fountain Creek. However, because the Colorado Springs Sewage Treatment Plant contributes such a large amount of flow to Fountain Creek, seasonal variations in the effluent quality are more important. These variations are shown in figure 5.2-2 and indicate that the concentrations and distribution of nitrogen forms were relatively stable during 1982. Total nitrogen concentrations decreased somewhat during September and October. During the same period, more nitrification occurred in the plant, resulting in more total nitrite plus nitrate nitrogen and less total ammonia nitrogen being discharged to Fountain Creek.

# **EXPLANATION**



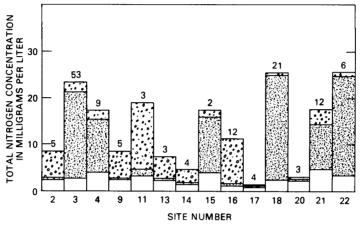


Figure 5.2-1.--Mean total nitrogen concentrations of inflows and diversions, 1982.

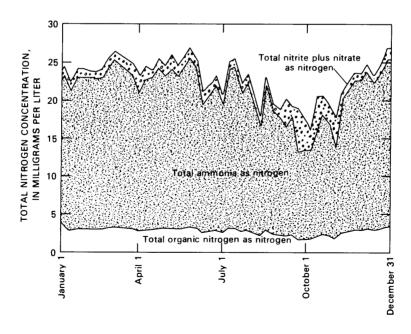


Figure 5.2-2.--Variations in total nitrogen concentrations in flow from the Colorado Springs Sewage Treatment Plant, 1982.

# 5.0 SURFACE-WATER QUALITY--Continued

## 5.3 Quantification of Nitrogen Sources in Fountain Creek and Canal No. 4

Sources of water in Fountain Creek and Canal No. 4 during 1982 were estimated in an earlier section of this report. To extend this analysis to estimate sources of nitrogen at the same points, it was necessary to calculate predicted values of daily total nitrogen concentrations for Fountain Creek at Colorado Springs, Colorado Springs Sewage Treatment Plant outfall, Shooks Run, and Spring Creek.

Daily total nitrogen concentration for Fountain Creek at Colorado Springs can be predicted using a least-squares linear regression relationship between streamflow and total nitrogen load using 1982 data (table 11.0-1, Supplemental Information section). The regression relationship was significant at the 99-percent level, and the correlation coefficient was 0.95. The equation for predicting total nitrogen concentration from this relation is:

PREDNIT = 1.68 + 25.85/QCSPGS,

where PREDNIT = Predicted total nitrogen concentration of Fountain Creek at Colorado Springs, in milligrams per liter as nitrogen; and QCSPGS = Daily flow of Fountain Creek at Colorado Springs.

Daily total nitrogen concentrations for the Colorado Springs Sewage Treatment Plant were predicted by a simple linear interpolation between weekly concentrations. A relation between daily flow and total nitrogen concentrations was statistically significant, but this relationship did not explain enough of the variation to be a useful predictor.

Daily total nitrogen concentrations for Shooks Run and Spring Creek were assumed to be equal to the mean concentration measured during 1982 at these sites. This method gave acceptable results, because the flow at these sites generally was small (fig. 2.1-2), and the coefficient of variation of total nitrogen concentration at both sites was 25 percent or less.

Results of the mass-balance calculations to estimate sources, loads, and concentrations of total nitrogen during 1982 are shown in figure 5.3-1. During 1982, an estimated 85 percent of the total nitrogen at Fountain Creek below Janitell Road (site 10) was contributed by the Colorado Springs Sewage Treatment Plant; about 13 percent was contributed from upstream sources, primarily Fountain Creek at Colorado Springs; the remaining 2 percent of the total nitrogen was contributed from Spring Creek. The estimated mean daily total nitrogen concentration at Fountain Creek below Janitell Road during 1982 was 12.1 mg/L as N (milligrams per liter as nitrogen).

An estimated 93 percent of the total nitrogen in Canal No. 4 was contributed by the Colorado Springs Sewage Treatment Plant during 1982; the remaining 7 percent was from upstream sources. The estimated mean daily total nitrogen concentration in Canal No. 4 during 1982 was 14.1 mg/L as N. Sampling at several locations along the canal during 1982 indicated that little change occurred in total nitrogen concentration between the headgate and Big Johnson Reservoir. The total nitrogen concentration at the headgate, then, was a reasonable estimate of concentrations that were available for potential recharge to the Widefield aquifer from canal leakage.

# **EXPLANATION**

ESTIMATED MEAN DAILY TOTAL NITROGEN CONCENTRATION, IN MILLIGRAMS PER

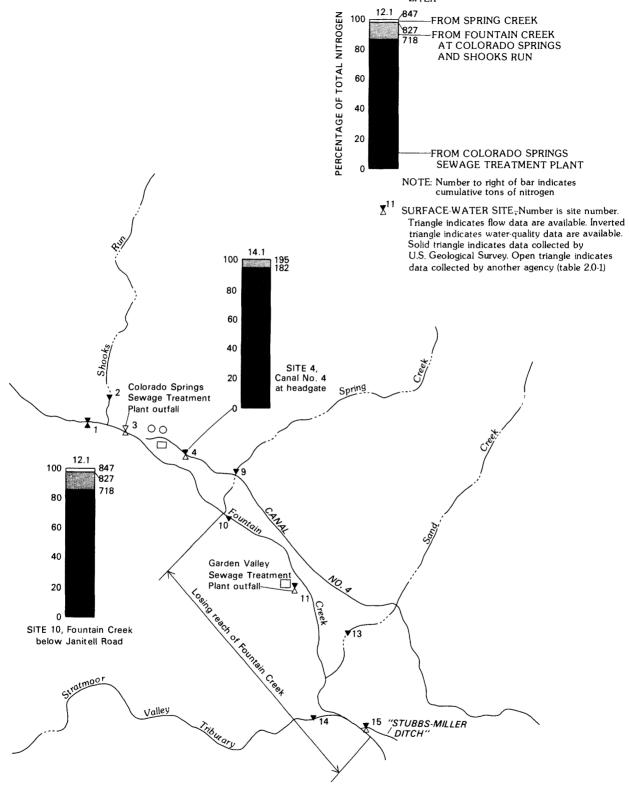


Figure 5.3-1.--Sources, estimated loads, and concentrations of total nitrogen in the upstream end of the study area.

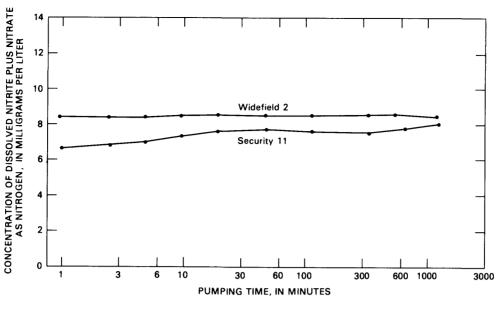
## 6.0 GROUND-WATER QUALITY

## 6.1 Nitrogen Variations in Pumping Wells and Sampling Methods

Studies of ground-water quality have shown that concentrations of chemical constituents, including nitrite plus nitrate, in water pumped from alluvial aquifers may be related to well construction and operation (Schmidt, 1977; Nightingale and Bianchi, 1980). In a given hydrologic environment, differences in well construction and operation may cause varying changes in nitrate concentration with pumping time. Such changes have been most evident for infrequently pumped, shallow wells near point or line sources of contamination (Schmidt, 1977). This type of concentration variation was minimized during the study by collecting most ground-water samples from similarly constructed and operated wells. All wells from which samples were collected in the Widefield aquifer, except one, were large capacity, municipal-supply or irrigation wells. These wells have similar construction, including large diameter casing (12 to 24 inches), perforations throughout most or all of the saturated thickness, gravelpack, and turbine pump with the intakes set below the level of drawdown. Most of these wells were in frequent use, especially during the summer months, when much of the sampling was done.

Two municipal-water-supply wells were sampled 10 times during a 24-hour period after the pump was turned on to determine dissolved nitrite plus nitrate concentration variations with time. Neither of the wells had been pumped for at least 2 days prior to the sampling. The results of the sampling (table 11.0-2 in the Supplemental Information section, fig. 6.1-1) show that only small concentration variations in dissolved nitrite plus nitrate occurred with pumping time. This indicates that dissolved nitrite plus nitrate data from large-capacity wells can be used to confidently evaluate temporal and areal trends. To help insure comparability of data between large capacity wells, samples were collected only after a pumping period of at least 10 minutes, and frequently, the pumping period was longer.

Many of the wells used to collect ground-water samples from tributary alluvium were small-capacity domestic wells or small-diameter wells without pumps. Because domestic wells are generally in continuous use, they were pumped long enough to flush the delivery system and deliver fresh water for samples. Some of these wells were equipped with pressure tanks, but no samples were collected after water had passed through water softeners. Wells without pumps were either bailed or pumped with a portable centrifugal pump or submersible pump; at least two well volumes of water, and usually more, were removed from the well before sampling.



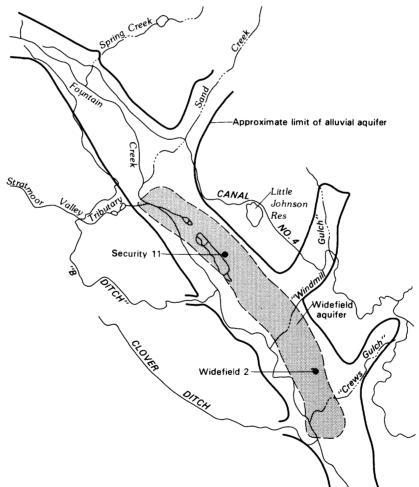


Figure 6.1-1.--Variations in concentrations of dissolved nitrite plus nitrate with pumping time in two wells.

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6.2 Temporal Variations of Nitrogen

6.2.1 Long-Term Variations in Nitrogen Data

Water-quality data for dissolved nitrite plus nitrate (fig. 6.2.1-1) and other constituents have been collected by the city of Colorado Springs from well fields on the Venetucci and Pinello Ranches, since 1965. However, interpretation of these data is limited by the samples being collected from pipelines leaving each well field, rather than individual wells and by the use of four different analytical techniques for nitrate during the period. Approximate times that the four analytical techniques were used were obtained from Monte Fryt (Laboratory Director, Colorado Springs Department of Public Utilities, Water Division, oral commun., 1983) and are shown in figure 6.2.1-1. In general, concentrations of dissolved nitrite plus nitrate were less than 1 mg/L as N (milligram per liter as nitrogen) during 1965-67 when dissolved nitrite plus nitrate was analyzed using the phenyldisulfonic-acid method. Dissolved nitrite-plus-nitrate concentrations increased rapidly during the late 1960's. During this time, samples were analyzed by both the phenyl-disulfonic-acid and Hach methods, with both methods giving similar small concentrations during 1967-68. The apparent concentration increase occurred first in the Pinello Ranch wells, which are nearer the area of recharge from Fountain Creek. Between 1970 and 1982, dissolved nitrite-plus-nitrate concentrations of water produced from both well fields were variable but have not shown a consistent trend in time.

Water-quality data have been collected previously by the U.S. Geological Survey during 1954-55, 1972, and 1977. Dissolved nitrite-plus-nitrate concentrations were determined before 1981 and again during 1981-82 on water from 17 wells in the study area, 13 in the Widefield aquifer and 4 in tributary alluvium (fig. 6.2.1-1). Only two samples were analyzed for dissolved nitrite plus nitrate during 1954-55; concentrations of dissolved nitrite plus nitrate during 1981-82 exhibited large increases since 1954-55.

Between 1972 and 1981-82, concentrations of dissolved nitrite plus nitrate increased in all five wells sampled in the Widefield aquifer. The increase in concentration from two wells in the northern one-third of the aquifer was much larger than three wells in the southern one-third. However, the increases in all five wells are similar in magnitude to seasonal variations observed on water from wells sampled monthly during 1981-82 and, as such, may not represent a long-term trend.

Concentrations of dissolved nitrite plus nitrate were measured during 1977 and 1981-82 on water produced from five wells located throughout the aquifer. Water from only one well in the north end of the aquifer increased in concentration by more than 1.2 mg/L as N. Other concentration changes during the 1977 to 1981-82 period were small.

Two additional wells, Widefield-4 and Venetucci-3, were sampled about 15 times during 1976-79 and again during 1981-82 (fig. 6.2.1-1). Sufficient samples are available to statistically evaluate time trend. Because dissolved nitrite-plus-nitrate concentrations were not normally distributed, and a data gap occurs between 1979 and 1981, the Wilcoxon rank-sum nonparametric test was chosen to evaluate the trend (SAS Institute, 1982). Results of the test and mean concentrations during both periods are shown here:

| Site        |         | trite-plus-nitrate con-<br>ams per liter as nitrogen) | Significant change<br>(95-percent confidence |
|-------------|---------|---|--|
|             | 1976-79 | 1981-82   | level, two-tailed test)                      |
| Venetucci-3 | 7.75    | 8.39  | yes  |
| Widefield-4 | 6.97    | 6.91  | no   |

Results of this test indicate that concentrations of dissolved nitrite plus nitrate have increased in well Venetucci-3, located in the northern one-half of the aquifer, while no statistically significant change was observed in well Widefield-4, located at the south end of the aquifer.

In spite of problems with changing analytical techniques, long-term data from the city of Colorado Springs and the U.S. Geological Survey indicate that concentrations of dissolved nitrate as nitrogen in water produced from the Widefield aquifer have increased. Twenty to thirty years ago, concentrations ranged from 0.5 to 3.0 mg/L as N to concentrations that approach, and occasionally exceeded, the drinking-water standard of 10 mg/L as N during 1981 and 1982. Data collected during the last 6 to 10 years also indicate that concentrations of dissolved nitrite plus nitrate may have increased more rapidly in water produced from some wells located in the northern part of the aquifer than in other places.

#### 6.0 GROUND-WATER OUALITY--Continued

6.2 Temporal Variations of Nitrogen--Continued 6.2.2 Short-Term Variations in Nitrogen

Short-term variations in dissolved-nitrogen concentrations were evaluated using monthly data from six wells and annual data from 54 wells during 1981 and 1982 (table 11.0-2, Supplemental Information section).

Variations in concentrations of dissolved nitrogen in the six wells sampled monthly are shown in figure 6.2.2-1. Consistent seasonal trends are not evident during 1981 and 1982 at any of the sites, nor are seasonal concentration trends similar between adjacent sites. Nitrite plus nitrate is the major nitrogen form present at all sites, making up between 82 and 91 percent of the total. Organic nitrogen makes up most of the remainder, with smaller concentrations of ammonia.

Concentrations of dissolved nitrite plus nitrate at the five sites sampled monthly where at least 18 analyses were available during 1981-82 were evaluated for concentration trends with time. Trends were evaluated using the Kendall tau-b correlation coefficient (SAS Institute, 1982). Because the test used only 2 years of data, results should only be considered suggestive. Results of the test and related data are shown here:

|                   |                         | dissol | trations of ved nitrite                            | Kendall tau-b t<br>test resul                                |                          |
|-------------------|-------------------------|--------|--|--|--------------------------|
| Site name         | Number<br>of<br>samples |        | grams per<br>as nitrogen)<br>Standard<br>deviation | Significant<br>trend (confidence<br>level in<br>parenthesis) | Direction<br>of<br>trend |
| Stratmoor Hills-4 | 22                      | 7.15   | 0.88   | Yes (90 percent)   | Increasing               |
| Security-14       | 22                      | 5.70   | 1.02   | Yes (90 percent)   | Increasing               |
| Venetucci-3       | 20                      | 8.38   | .79  | No (90 percent)  |                          |
| Security-2        | 18                      | 6.25   | .86  | Yes (95 percent)   | Decreasing               |
| Widefield-4       | 23                      | 6.91   | . 85   | Yes (95 percent)   | Decreasing               |

Short-term trends also were evaluated using data from 46 wells in the Widefield aquifer, and 8 wells in tributary alluvial aquifers, collected during the summers of 1981 and 1982. Mean dissolved nitrite-plus-nitrate concentrations of about 7 mg/L as N (milligrams per liter as nitrogen) in the Widefield aquifer and about 6 mg/L as N in tributary alluvium did not change significantly between 1981 and 1982. However, changes at individual wells were as large as 3.1 mg/L as N and some areal variation in these changes occurred in the Widefield aquifer as shown below:

| Concentration change,                         |                   | Northern part of aquifer |         | Southern part of aquifer |         |
|---|-------------------|--------------------------|---------|--------------------------|---------|
| 1981-82 (milligrams<br>per liter as nitrogen) | Category          | Number<br>of wells       | Percent | Number<br>of wells       | Percent |
| >1.6  | Large increase    | 3                        | 12      | 2                        | 10      |
| 0.8 to 1.6                                    | Moderate increase | 5                        | 19      | 0                        | 0       |
| 8 to .8                                       | No change         | 11                       | 42      | 8                        | 40      |
| 8 to -1.6                                     | Moderate decrease | 3                        | 12      | 4                        | 20      |
| <-1.6   | Large decrease    | 4                        | 15      | 6                        | 30      |

The aquifer was divided into southern and northern parts at the south end of the Venetucci Ranch well field. About 40 percent of wells in both areas were in the no-change category. Water from about as many wells showed moderate to large increases in concentration as moderate to large decreases in the northern part of the aquifer, while water from five times as many wells showed decreases as increases in the southern part of the aquifer. Water from 8 of 10 wells with concentration increases were in the northern area and about 60 percent of wells with decreases in concentration were in the southern part of the aquifer. While these data are too limited to be statistically significant, they indicate that future water-quality data needs to be examined carefully to evaluate these trends.

### 6.0 GROUND-WATER QUALITY--Continued 6.3 Areal Variations of Nitrogen

Concentrations of dissolved nitrite plus nitrate as nitrogen in ground water in and adjacent to the Widefield aquifer during the summer of 1982 are shown in figure 6.3-1. These concentrations are shown rather than dissolved nitrogen because dissolved nitrite plus nitrate is of greater interest in drinking waters. The distribution of dissolved nitrogen, which is used in later sections to calculate nitrogen loads, is generally similar, but the actual concentrations are larger. The general pattern of concentration was similar in 1981. The largest concentrations occurred near the north end of the Widefield aquifer near the confluence with Sand Creek. These large concentrations are consistent with recharge from Fountain Creek as the source of nitrogen. Gain-loss studies have indicated that Fountain Creek recharges the Widefield aquifer in the reach between Janitell Road and the headgate of the Stubbs-Miller Ditch. Upstream from the recharge area, concentrations of dissolved nitrite plus nitrate in ground water from the Fountain Creek alluvium were in the range of 6 to 8 mg/L as N (milligrams per liter as nitrogen) or less.

Large concentrations appear to be diluted by tributary inflows or recharge from land surface to concentrations from 8 to 10 mg/L as N, in a narrow band extending as far south as the Venetucci Ranch. During the summer of 1982, concentrations of dissolved nitrite plus nitrate were less than 8 mg/L as N in the central part of the aquifer, with concentrations between 3 and 5 mg/L as N in water produced from several wells on the west side of the aquifer, which underlie or are just downgradient from agricultural areas.

A narrow band of concentrations greater than 8 mg/L as N also occurred in the southern end of the aquifer. Concentrations reached 10 mg/L as N in one well (Widefield-14), which is located adjacent to and may be affected by seepage from the Widefield Sewage Treatment Plant lagoons.

Because other data (section 6.2.1) indicated that concentrations of dissolved nitrite plus nitrate may have increased more rapidly in the northern part of the Widefield aquifer during the last 6 to 10 years, concentrations in 1982 were tested to determine if a difference existed between the northern and southern parts of the aquifer. The test was made using the Wilcoxon rank-sum nonparametric test, and indicated no statistically significant difference existed between the areas in the concentration of dissolved nitrite plus nitrate. This lack of difference suggests that time trends noted in sections 6.2.1 and 6.2.2 may be localized and are not affecting the entire aquifer.

Concentrations of dissolved nitrite plus nitrate were less than 4 mg/L as N in the upgradient reaches of tributary alluvium along Windmill and Crews Gulches, indicating that these inflows did not increase concentrations in the Widefield aquifer. The Widefield aquifer also received inflow from water in eolian deposits recharged by leakage from Canal No. 4 between Sand Creek and Windmill Gulch. Few wells exist in this area, but two that were sampled had concentrations of dissolved nitrite plus nitrate of 9.5 and 27 mg/L as N during 1982. Larger concentrations found in one well indicated possible contamination by some localized source, such as septic systems that are used in that area. Larger concentrations found in the area were not reflected in the concentrations downgradient in the Widefield aquifer, indicating either that they were not representative of the area, or that some process, such as dilution or denitrification, was reducing concentrations downgradient.

Areal variations in the concentration of dissolved organic nitrogen and dissolved nitrite were not significant, but larger concentrations of dissolved ammonia nitrogen occurred in Stratmoor Hills-4, located in the north end of the Widefield aquifer, than in four wells as shown:

|                   | Num   | bër of samples   | Mean dissolved ammonia nitrogen  |
|-------------------|-------|--|--|
| Well              | Total | With concentra-<br>tions greater<br>than limit of<br>detection | concentration in samples with concentrations greater than limit of detection (milligram per liter as nitrogen) |
| Stratmoor Hills-4 | 22    | 19   | 0.17   |
| Security-14       | 22    | 13   | . 10   |
| Venetucci-3       | 20    | 10   | .10  |
| Security-2        | 18    | 10   | .09  |
| Widefield-4       | 23    | 14   | .09  |

This concentration difference was statistically significant at the 99-percent confidence level based on a Kruskal-Wallis nonparametric test and indicates that nitrification of ammonia nitrogen in water recharged from Fountain Creek was not always complete in the northern part of the aquifer.

### 6.0 GROUND-WATER QUALITY--Continued 6.4 Vertical Variations of Nitrogen

Vertical variations in the concentration of dissolved nitrite plus nitrate in the Widefield aquifer were evaluated by sampling four municipal-supply or irrigation wells throughout the aquifer during 1982. These wells were perforated throughout the saturated thickness, but none of the wells was equipped with pumps at the time of sampling. Two of the wells had been unused for several years (Pinello-14 and Enfield-3), and the other two had the pumps pulled for repairs and had not been used for about 6 months. Sampling of all four wells was made by first measuring the total saturated thickness in the casing using a steel tape, dividing this total into five or six equal intervals, and collecting samples with a 1-foot-long thief sampler at the center of each interval. Samples were collected from the top down to minimize disturbance in the water column. Results of the sampling are shown in figure 6.4-1. Little vertical variation of dissolved nitrite-plus-nitrate concentrations occurred in any of these wells, which were located in all parts of the aquifer and are near various sources of recharge including Fountain Creek, agricultural, and residential areas.

Lack of apparent vertical variation in dissolved nitrite-plus-nitrate concentrations in the Widefield aquifer may have resulted from the fact that most of the recharge resulted from infiltration of recharge from Fountain Creek in the northern part of the aquifer, rather than percolation from land surface in the form of irrigation return flow, artificial recharge, septic systems, and seepage from sewage lagoons. As the water recharged from Fountain Creek moves south through the aquifer, it is subject to intense pumping, which results in more mixing and less vertical stratification than would occur in a less-pumped system.

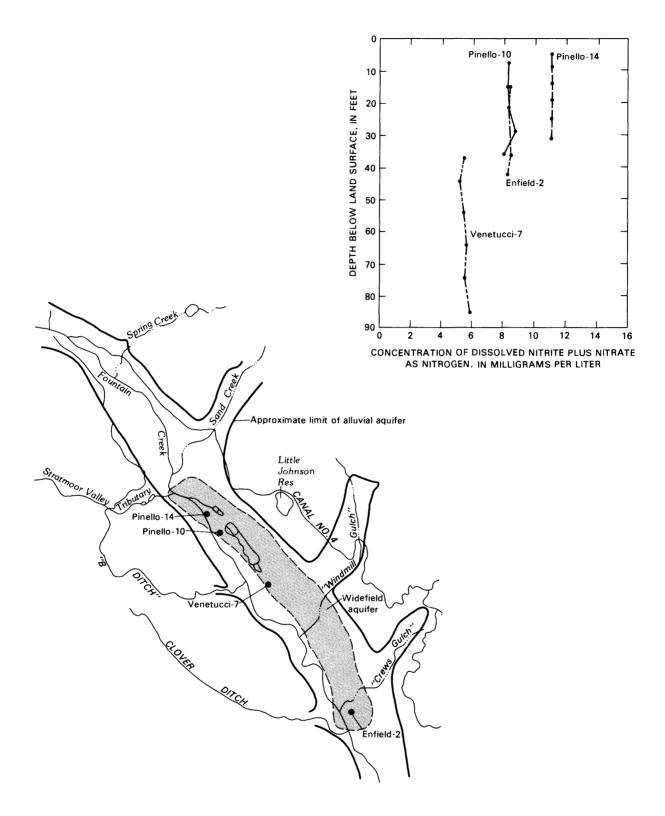


Figure 6.4-1.--Vertical variations in the concentration of dissolved nitrite plus nitrate as nitrogen in four wells.

### 7.0 NITROGEN SOURCES AND LOADS TO THE WIDEFIELD AQUIFER

Nitrogen may enter the Widefield aquifer from Fountain Creek, underflow from Fountain Creek alluvium and tributary alluvium, and recharge from land surface. For the purpose of estimating the amount of nitrogen entering the aquifer from various sources, nitrogen loads were calculated for each source, using dissolved or total nitrogen concentrations and the volume of water recharging the aquifer from each source. Load refers to the amount of nitrogen in solution or in transport; in this report, load is usually expressed in tons.

As previously discussed in section 4.0, given the right environmental conditions, nitrogen may undergo many different transformations in the unsaturated and saturated zones. Nitrogen transformations in the Widefield aquifer probably occur more readily in the unsaturated zone than in the saturated zone. The probable nitrogen pathways and transformation processes that occur in the Widefield aquifer are shown in figure 7.0-1. During infiltration and percolation, nitrogen may first be nitrified to nitrate, which then may be denitrified. Ammonium may, in addition, be reversibly adsorbed to aquifer materials, especially clays. Of these processes, only denitrification results in permanent nitrogen loss from the aquifer and, therefore, is the transformation process that may produce the greatest uncertainties in estimating nitrogen loads from various sources.

Due to the apparent presence of dissolved oxygen in most parts of the aquifer and the lack of adequate concentrations of a carbon source in the ground water in the Widefield aquifer, significant denitrification is unlikely to occur, and nitrogen in the ground water should be fairly stable. Therefore, nitrogen loads from underflows should be reasonable. The largest uncertainty in estimating nitrogen loads from underflows probably results from errors in estimating the volume of water recharging the aquifer from each source.

Because the potential exists for significant nitrogen losses in the unsaturated zone through denitrification, estimates of nitrogen loads to the aquifer from Fountain Creek, seepage from Canal No. 4, irrigation, and artificial recharge are most likely to have the greatest uncertainties. Due to the nonconservative nature of nitrogen, specifically in the unsaturated zone, and uncertainties in estimating the volume of water recharging the aquifer from various sources, it is not possible to confidently compute a nitrogen budget for the Widefield aquifer. The reader needs to be aware that nitrogen loads presented in this report may be considered only as estimates of the nitrogen contribution to the aquifer from each source.

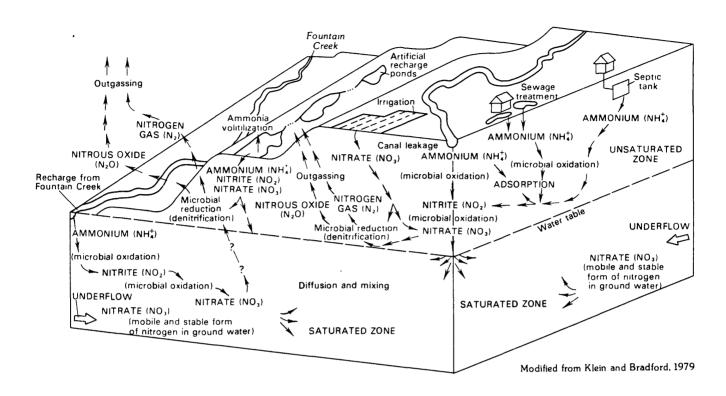


Figure 7.0-1.--Nitrogen pathways and transformation processes in the Widefield aquifer.

# 7.0 NITROGEN SOURCES AND LOADS TO THE WIDEFIELD AQUIFER--Continued 7.1 Fountain Creek and Fountain Creek Alluvium

Recharge from Fountain Creek and underflow from Fountain Creek alluvium are two sources of nitrogen to the Widefield aquifer. Nitrogen load in Fountain Creek below Janitell Road during 1982 was estimated to be 850 tons (fig. 5.3-1). The primary source of nitrogen in the losing reach of Fountain Creek (fig. 5.3-1) is the Colorado Springs Sewage Treatment Plant effluent, which made up 42 percent of the flow in Fountain Creek during 1982. During 1982, the Colorado Springs Sewage Treatment Plant contributed approximately 720 tons (fig. 5.3-1) of nitrogen to Fountain Creek. Spring Creek contributed 20 tons of nitrogen to Fountain Creek, and the nitrogen load in Fountain Creek upstream from the outfall from the Colorado Springs Sewage Treatment Plant was approximately 110 tons. Because little change in total nitrogen concentration occurred in the losing reach of Fountain Creek, the estimated mean daily total nitrogen concentration of 12.1 mg/L (milligrams per liter) (fig. 5.3-1) was used as the nitrogen concentration in water that was available to recharge the Widefield aquifer during 1982. An estimated 8,000 acre-ft/yr (acre-feet per year) of water from Fountain Creek recharged this reach of the aquifer. The resulting potential nitrogen load in water recharging the Widefield aquifer during 1982 was 130 tons (fig. 7.1-1) or about 15 percent of the nitrogen in the stream. This amount does not account for nitrogen losses through denitrification, which could reduce the concentration of nitrogen in water recharging the aquifer. If denitrification occurred during recharge, the actual amount of nitrogen from Fountain Creek recharging the aquifer could be substantially less than 130 tons.

Nitrogen in ground water of the Fountain Creek alluvium enters the Widefield aquifer near the confluence of Sand Creek and Fountain Creek. In this area, nitrogen in ground water may originate as recharge from Fountain Creek, seepage from Canal No. 4, underflow from Sand Creek alluvium, and underflow from Fountain Creek alluvium north of Highway 29. The amount of nitrogen that reaches the Widefield aquifer from Fountain Creek alluvium north of Highway 29 for 1982 was calculated by using an underflow of 700 acre-feet (cross section A-A', section 3.1.2), and from the mean dissolved-nitrogen concentration of water samples collected periodically during 1982 from four wells located near Highway 29. Mean dissolved-nitrogen concentrations in the water collected from the four wells ranged from 7.7 to 9.1 mg/L as N (milligrams per liter as nitrogen), with a mean of 8.3 mg/L as N and a standard deviation of 0.59. The resulting nitrogen load to the Widefield aquifer from ground water in the Fountain Creek alluvium north of Highway 29 during 1982 was about 8 tons.

## **EXPLANATION**

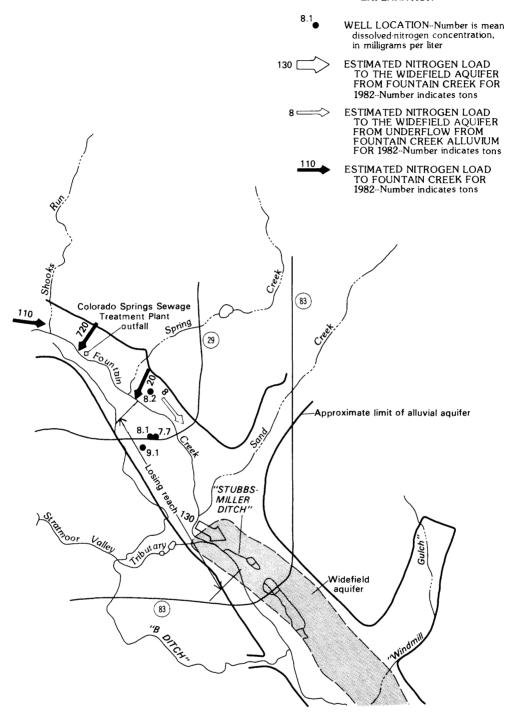


Figure 7.1-1.--Estimated nitrogen loads to the Widefield aquifer from Fountain Creek and from underflow from Fountain Creek alluvium for 1982.

# 7.0 NITROGEN SOURCES AND LOADS TO THE WIDEFIELD AQUIFER--Continued 7.2 Tributary Alluvium

Ground-water inflow to the Widefield aquifer from tributary alluvium is a source of nitrogen to the Widefield aquifer. Nitrogen loads to the aquifer for 1982 from tributary alluvium were estimated using underflows calculated in section 3.1.2, and from dissolved-nitrogen concentration of water samples collected from wells located in the tributary alluvium (fig. 7.2-1).

Nitrogen enters the Widefield aquifer from the east with underflow from Sand Creek alluvium, Windmill Gulch alluvium, Crews Gulch alluvium, and from saturated eolian deposits that are recharged by leakage from Canal No. 4. The mean dissolved-nitrogen concentration of ground water in Sand Creek alluvium was estimated to be 2.1 mg/L as N (milligrams per liter as nitrogen), based on water samples collected quarterly from a well located immediately upgradient from Canal No. 4 (fig. 7.2-1). Using an underflow of 28 acre-feet (table 3.1.2-1), and a dissolved-nitrogen concentration of 2.1 mg/L as N, the 1982 nitrogen load to the Widefield aquifer from Sand Creek alluvium was calculated to be less than 1 ton (160 pounds). The amount of nitrogen entering the Widefield aquifer from Windmill Gulch alluvium during 1982 was estimated to be almost 2 tons (3,850 pounds), using an underflow of 200 acre-feet (table 3.1.2-1) and a mean dissolved-nitrogen concentration of 7.1 mg/L as N (fig. 7.2-1). The amount of nitrogen reaching the Widefield aquifer with underflow from Crews Gulch alluvium during 1982 was estimated to be less than 1 ton (1,220 pounds). The amount is based on an underflow of 90 acre-feet and a mean dissolved-nitrogen concentration of 5.0 mg/L as N (fig. 7.2-1).

Nitrogen enters the Widefield aquifer with underflow from the saturated eolian deposits located east of the Widefield aquifer between Sand Creek and Windmill Gulch primarily as a result of seepage from Canal No. 4. During 1982, the estimated nitrogen load in Canal No. 4 was 195 tons. An estimated 93 percent of the 195 tons in Canal No. 4 was contributed by the Colorado Springs Sewage Treatment Plant: 7 percent of the load was from upstream sources (section 5.3). Assuming 880 acre-feet of canal water recharged the eolian deposits (section 3.1.2), and the mean total nitrogen concentration in the ditch water was 14 mg/L as N, the 1982 nitrogen load to the eolian deposits from Canal No. 4 was approximately 17 tons. This amount does not account for potential nitrogen losses through denitrification. Seven hundred and twenty acre-feet of water were estimated to have entered the Widefield aquifer as a result of underflow from the eolian deposits. Water samples collected from two wells located in the area indicated the ground water in the area contained large dissolved-nitrogen concentrations. A water sample from one well had a dissolved-nitrogen concentration of 11 mg/L as N; a water sample from the other well contained 29 mg/L as N, indicating some localized contamination, such as septic systems. Because the well water containing 11 mg/L of dissolved nitrogen probably was more representative of the concentration of nitrogen in the ground water in the area, it was used to calculate the 1982 nitrogen load to the aquifer from eolian deposits. The resulting nitrogen load to the aguifer was 13 tons.

Small amounts of nitrogen entered the Widefield aquifer from the west, with underflow from Stratmoor Valley tributary alluvium, B Ditch alluvium, and Clover Ditch alluvium. Although relatively large concentrations of dissolved nitrogen occurred in water produced from these alluvial deposits, the combined nitrogen load to the Widefield aquifer for 1982 from these areas was less than 1 ton, because of the small amount of water entering the Widefield aquifer from the west.

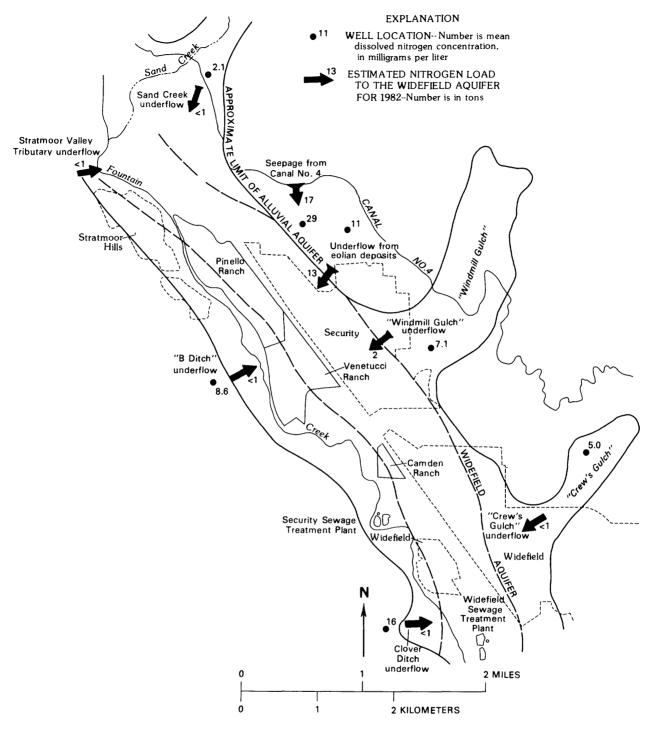


Figure 7.2-1.--Estimated nitrogen loads to the Widefield aquifer from underflow from tributary alluvium for 1982.

# 7.0 NITROGEN SOURCES AND LOADS TO THE WIDEFIELD AQUIFER--Continued 7.3 Recharge from Land Surface

Leaching of nitrogen to the Widefield aquifer from the land surface occurs as a result of infiltration and percolation of precipitation and irrigation water, artificial recharge at the Pinello Ranch, seepage from sewage lagoons, and septic systems. The amount of nitrogen that reached the aquifer as the result of deep percolation from precipitation and irrigation during 1982 was estimated separately for residential and agricultural areas. As mentioned in section 3.1.3, 435 acres of lawns and 286 acres of irrigated agricultural land overlie the aquifer. Alfalfa was grown on about 127 acres of the agricultural land; corn was grown on most of the remaining 159 acres. Because turf grass, alfalfa, and corn absorb different amounts of nitrogen, separate estimates of the 1982 nitrogen load to the aquifer were made for each crop.

Lawns in the area receive nitrogen from irrigation water and from fertilization. During 1982, the mean dissolved-nitrogen concentration of irrigation water was estimated to be 8.0 mg/L as N (milligrams per liter as nitrogen) in Security, and 8.7 mg/L as N in Widefield. Means were calculated from the dissolved-nitrogen concentration of water samples collected during the summer of 1982 from all wells supplying water to the two communities. Approximately 800 acre-feet of irrigation water, containing 8 mg/L of nitrogen, was applied to the 299 acres of lawns in Security during 1982, resulting in an application of about 58 pounds of nitrogen per acre through lawn irrigation. Approximately 100 acre-feet of irrigation water containing 8.7 mg/L of nitrogen was applied to the 136 acres of lawns in Widefield during 1982, resulting in an application of about 18 pounds of nitrogen per acre through lawn irrigation. The amount of fertilizer applied to the lawns was estimated from a national Gallup survey (Dr. John Long, O.M. Scott Inc., oral commun., 1983). Based on the survey, the maximum amount of fertilizer applied during 1 year would be about 6.8 pounds per 1,000 square feet or 296 pounds per acre. When combined with the amount of nitrogen in irrigation water, the maximum amount of applied nitrogen was estimated to be 354 pounds per acre in Security, and 314 pounds per acre in Widefield. Bouwer (1978, p. 425) noted that frequently mowed grasses may absorb as much as 560 pounds of nitrogen per acre per year. Because the maximum application rate was less than the potential annual nitrogen uptake for turf grasses, the amount of nitrogen leached to the ground water from lawn irrigation and fertilization during 1982 probably was small. However, during periods of excessive irrigation or precipitation, some nitrogen may have leached past the root zone and into the aquifer.

The leaching of nitrogen to the aquifer as a result of agricultural irrigation was estimated for each agricultural area. Because fertilizers are not presently used on any of the agricultural areas (Nick Venetucci, Ralph Chappel, and William J. McCullough, oral commun., 1982), the only source of nitrogen is the nitrogen in the irrigation water. Because of the small number of livestock in the area, the nitrogen from livestock waste was considered negligible.

One of three agricultural areas is the Camden Ranch (fig. 7.3-1), where approximately 31 acres of alfalfa were irrigated by one well. The nitrogen concentration of the irrigation water, based on one water sample during summer 1982, was 5 mg/L as N. Approximately 145 acre-feet of irrigation water was used to irrigate the 31 acres of alfalfa, resulting in an application of 63 pounds of nitrogen per acre. Alfalfa can fix atmospheric nitrogen and can use an estimated 224 pounds of nitrogen per acre during the growing season (Stewart and others, 1975). Because the application rate of nitrogen was less than the potential uptake rate, it was estimated that nitrogen applied to the alfalfa on Camden Ranch was used by the crop and not leached to the water table. However, during periods of excessive irrigation or precipitation, some nitrogen may have leached past the root zone and into the aquifer.

Alfalfa also was grown at the Pinello Ranch, where approximately 96 acres of alfalfa were irrigated during 1982. Most of the irrigation water is from the Stubbs-Miller Ditch, which is diverted from Fountain Creek; the remainder of the irrigation is ground water pumped from the Pinello Ranch wells.

### 8.0 NITROGEN OUTFLOWS FROM THE WIDEFIELD AOUIFER

Dissolved nitrogen moves out of the Widefield aquifer into Fountain Creek in those areas where water flows from the aquifer to Fountain Creek. Nitrogen also moves from the aquifer with ground-water outflows to the south, and with water withdrawn from the aquifer through pumpage. The amount of nitrogen removed by each outflow was estimated by using dissolved-nitrogen concentrations in water samples collected during the summer of 1982 from wells completed in the Widefield aquifer.

The quantity of nitrogen moving from the aquifer to Fountain Creek during 1982 was estimated, using a flow of 2,300 acre-ft/yr (acre-feet per year), as determined from gain-loss investigations and a dissolved-nitrogen concentration of 8.4 mg/L as N (milligrams per liter as nitrogen). The nitrogen concentration was the mean found in water samples collected from 44 wells completed in the Widefield aquifer, adjacent to the reach where water generally flows from the aquifer to Fountain Creek. Using these concentrations, the amount of nitrogen lost from the aquifer to Fountain Creek was estimated to be 26 tons. Because of the higher than normal water table that occurred during 1982, this estimate may be low.

The quantity of nitrogen moving from the aquifer with ground-water underflow to the south was estimated by using a mean dissolved-nitrogen concentration of 9.2 mg/L as N from analyses of samples collected from three wells located near the southern boundary of the Widefield aquifer (fig. 8.0-1). The amount of underflow was calculated earlier (section 3.2.2) to be about 2,500 acre-ft/yr. The resulting nitrogen loss from the aquifer across the southern boundary was estimated to be 31 tons during 1982.

The largest amount of nitrogen removed from the aquifer during 1982 (and probably during most years) was through pumpage; nearly 5,400 acre-feet of ground water was withdrawn from the aquifer by pumpage. Fourteen wells operated by the Security Water and Sanitation District withdrew a reported 1,399 acre-feet of ground water. Mean dissolved-nitrogen concentration of the ground water withdrawn by the Security wells was nearly 8 mg/L as N, resulting in about 15 tons of nitrogen withdrawal. Ten wells operated by the Widefield Water Company withdrew a reported 1,254 acre-feet of ground water. Mean dissolved-nitrogen concentration of the ground water withdrawn by the Widefield wells was about 9 mg/L as N, resulting in about 15 tons of nitrogen being removed from the aquifer. Four Stratmoor Hills wells pumped a reported 659 acre-feet of ground water during 1982. Mean dissolved-nitrogen concentration of the ground water withdrawn by the Stratmoor Hills wells was about 9 mg/L as N, resulting in a withdrawal of about 8 tons of nitrogen during 1982. Wells on the Pinello Ranch withdrew a reported 1,825 acre-feet of ground water during 1982. Mean dissolved-nitrogen concentration of this ground water was about 8 mg/L as N, and approximately 20 tons of nitrogen were withdrawn from the aquifer as a result of pumpage of the Pinello Ranch wells. Five wells on the Venetucci Ranch withdrew about 93 acre-feet; mean dissolved-nitrogen concentration of this ground water was about 8 mg/L as N. Thus, approximately 1 ton of nitrogen was removed from the aquifer as a result of pumpage of the Venetucci Ranch wells. The well on the Camden Ranch withdrew about 145 acre-feet of ground water during 1982; mean dissolved-nitrogen concentration was approximately 5 mg/L as N, resulting in nearly 1 ton of nitrogen being removed from the aquifer. The total amount of nitrogen removed from the aquifer as a result of well pumpage for 1982 was about 60 tons. When combined with flow to Fountain Creek and underflow to the south, ground-water outflows resulted in almost 120 tons of nitrogen being removed from the aquifer during 1982. Because 1982 was a wet year, the aquifer was not pumped as extensively as normal, and the water table was higher than normal. Thus, the amount of nitrogen removed from the aquifer during 1982 would not be representative of most vears.

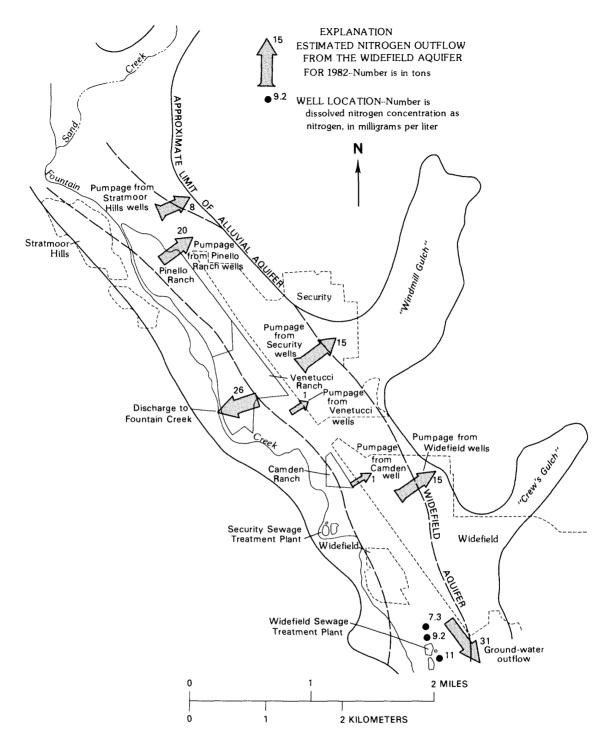


Figure 8.0-1.--Estimated amount of nitrogen removed from the Widefield aquifer during 1982 from ground-water outflow, flow to Fountain Creek, and pumpage.

### 9.0 SUMMARY OF NITROGEN SOURCES AND LOADS FOR THE WIDEFIELD AQUIFER

Nitrogen enters the Widefield aquifer from several sources. Almost all surface and ground water hydraulically connected to the aquifer contains significant concentrations of nitrogen; therefore, all these waters contribute to the overall nitrogen load of the aquifer. Because some nitrogen forms are unstable and may be transformed to other forms of nitrogen through nitrification or denitrification, the nitrogen loads from the various sources were estimated by using either total or dissolved nitrogen. Estimated 1982 nitrogen loads to the Widefield aquifer from various sources are shown in figure 9.0-1.

Effluent from the Colorado Springs Sewage Treatment Plant is the primary source of nitrogen entering the aquifer from all sources of recharge considered. Nitrogen in the effluent enters the aquifer as a result of streamflow losses from Fountain Creek, seepage from Canal No. 4, and artificial recharge ponds and irrigation at the Pinello Ranch. During 1982, the Colorado Springs Sewage Treatment Plant discharged 720 tons of nitrogen to Fountain Creek, resulting in a total nitrogen load in the losing reach of Fountain Creek of about 850 tons. Approximately 15 percent of the total nitrogen load, or about 130 tons of nitrogen, was estimated to be available to recharge the aquifer. Some of this nitrogen may not reach the ground-water system because of nitrogen loss through denitrification. The Colorado Springs Sewage Treatment Plant also discharged about 182 tons of nitrogen to Canal No. 4 during 1982. Approximately 17 tons of nitrogen were estimated to have been lost from the canal to the underlying eolian deposits as a result of seepage; an estimated 13 tons of nitrogen entered the Widefield aquifer as a result of underflow from eolian deposits. Because the predominant source of nitrogen in Canal No. 4 is from the Colorado Springs Sewage Treatment Plant, and seepage from Canal No. 4 appears to be the major source of nitrogen to the eolian deposits, the primary source of nitrogen to the aquifer from the eolian deposits is believed to be from the Colorado Springs Sewage Treatment Plant.

Water from Fountain Creek is diverted to Pinello Ranch recharge ponds via the Stubbs-Miller Ditch. Relatively small concentrations of nitrogen were detected in water samples collected from the ponds, because of consumption by aquatic plants or ammonia loss through volatilization. However, because the water is diverted from Fountain Creek, most of the nitrogen that is present can be attributed to the Colorado Springs Sewage Treatment Plant. During 1982, the amount of nitrogen reaching the aquifer from the recharge ponds was probably less than 1 ton. Approximately 5 tons of nitrogen entered the aquifer as the result of agricultural irrigation via the Stubbs-Miller Ditch.

Assuming no losses through denitrification, the total amount of nitrogen reaching the Widefield aquifer as the result of the Colorado Springs Sewage Treatment Plant effluent during 1982 would have been about 150 tons, or 93 percent of the total nitrogen load to the Widefield aquifer. Of the remaining 12 tons of nitrogen, approximately 8 tons were estimated to have entered the Widefield aquifer as a result of ground-water underflow from Fountain Creek alluvium; almost 3 tons of nitrogen were discharged to the Widefield aquifer from underflow from tributary alluvium; and about 1 ton of nitrogen was estimated to have leached to the water table by the process of infiltration and percolation from lawn irrigation, agricultural irrigation at the Venetucci Ranch and Camden Ranch, and from septic systems. Most of the nitrogen applied to the land through irrigation and fertilization probably was consumed by various crops in the area.

Nitrogen leaves the Widefield aquifer as a result of ground-water flow to Fountain Creek, ground-water outflow to the south, and ground-water pumpage. During 1982, an estimated 26 tons of nitrogen was discharged from the aquifer to Fountain Creek. Approximately 31 tons of nitrogen left the aquifer with underflow to the south, and 60 tons of nitrogen were removed from the aquifer as the result of pumpage. During most years, ground-water withdrawals have been nearly 1,700 acre-feet greater, which could result in about 20 more tons of nitrogen being removed from the aquifer as a result of pumpage. During 1982, nearly 120 tons of nitrogen were removed from the aquifer.

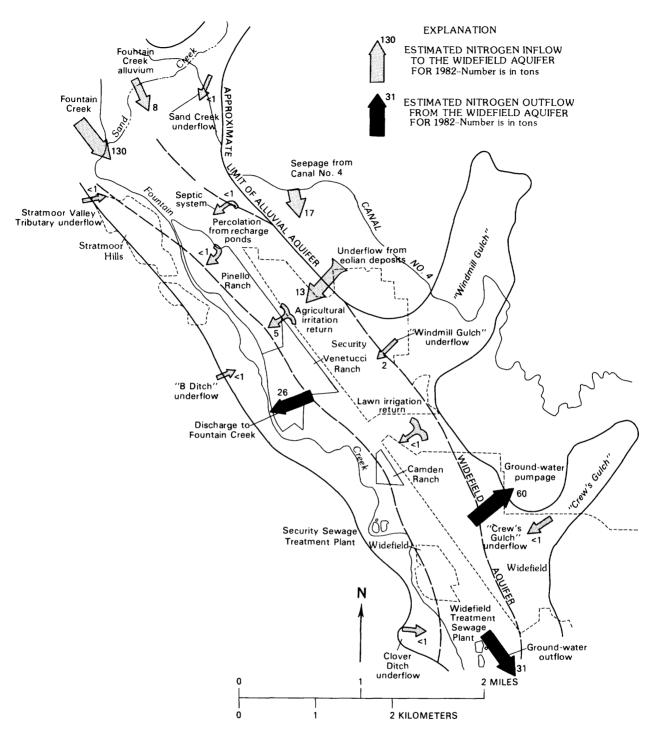


Figure 9.0-1.--Estimated nitrogen inflows and outflows to the Widefield aquifer during 1982.

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11.0 SUPPLEMENTAL INFORMATION

Table 11.0-1. -- Surface-water quality data

[ft³/s, cubic feet per second; °C, degrees Celsius; mg/L, milligrams per liter; µS/cm, microsiemens per centimeter at 25 degrees Celsius; combicate no data

|  | Total<br>nitro-<br>gen<br>(mg/L<br>as N)                                |                                    | ;        | ;        | :        | ;        | 3.4      | ;        | 1        | 4.1      | 5.6      | ;        | 3.3      | ;        | 1        | 1        | ;        | ;        | 2.3      | ;        | !<br>!   | ;        | 2.7      | 1        | ;        | 1.8      | ;        | 3.7      | 1.9      | 2.9      | 3.1      | 3.0      |
|--|---|------------------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
|  | Total ammonia and organic nitrogen (mg/L as N)                          |                                    | ;        | !        | ;        | ;        | 0.99     | ;        | ;        | 1.6      | 1.4      | ;        | 2.1      | ;        | ;        | :        | 1        | !        | 86.      | ;        | ;        | !        | 1.1      | :        | ;        | 1.1      | :        | 2.7      | .81      | 1.4      | 62.      | .57      |
|  | Total ammonia nitrogen (mg/L as N)                                      |                                    | ;        | ;        | į        | ;        | 090.0    | ;        | ;        | .510     | 060.     | ;        | . 280    | ;        | ;        | ;        | :        | ;        | 300      | ;        | :        | :        | . 160    | ;        | !        | <.060    | ;        | .520     | .360     | . 180    | .120     | .300     |
|  | Total<br>nitrogen<br>NO <sub>2</sub> +NO <sub>3</sub><br>(mg/L<br>as N) |                                    | ;        | ł        | ŧ        | :        | 2.40     | ;        | ;        | 2.50     | 1.20     | ;        | 1.20     | ;        | :        | 1        | ;        | ;        | 1.30     | ;        | ;        | :        | 1.50     | 1        | ť        | . 700    | ;        | 1.00     | 1.10     | 1.50     | 2.30     | 2.40     |
| lata]  | Total nitrite nitrogen (mg/L as N)                                      | ings                               | ;        | ŧ        | ;        | ;        | 0.020    | :        | ;        | 090.     | .020     | 1        | 070      | ;        | ;        | :        | ;        | ;        | .030     | ;        | ;        | 1        | .030     | :        | 1        | .030     | :        | .270     | 090      | .020     | <.020    | <.020    |
| dicate no d  | Dissolved<br>chloride<br>(mg/L<br>as Cl)                                | olorado Spr                        | ;        | į        | ţ        | ;        | 22       | 1        | ;        | 21       | 20       | ;        | 42       | !        | ;        | !        | !        | ;        | 18       | !        | :        | !        | 24       | ;        | !        | 11       | ;        | 13       | 12       | 18       | 21       | 23       |
| <, less than; E, estimated; dashes indicate no data] | Dissolved-solids<br>residue<br>at 105°C                                 | Fountain Creek at Colorado Springs | ;        | :        | ;        | :        | 492      | ;        | ;        | 384      | 291      | ;        | 294      | ;        | ł        | t        | ;        | ;        | 787      | t t      | ;        | !        | 405      | :        | ;        | 195      | !        | 287      | 27.7     | 425      | 538      | 897      |
| , estimated  | Specific<br>conduct-<br>ance<br>(µS/cm)                                 | 1 1                                | 650      | 620      | 750      | 800      | 740      | 570      | 199      | 635      | 995      | 450      | 485      | 180      | 550      | 510      | 009      | 069      | 711      | 009      | 580      | 730      | 783      | 350      | 200      | 465      | 640      | 867      | 470      | 667      | 672      | 684      |
| than; E  | Dis-<br>solved<br>oxygen<br>(mg/L)                                      | Station 07105500                   | ;        | ;        | ;        | ;        | 10.9     | ŧ        | :        | 9.5      | 8.3      | ;        | 7.8      | ;        | į        | ţ        | :        | ;        | 7.9      | ;        | ;        | ;        | 4.9      | ţ        | ţ        | 7.4      | :        | 8.1      | 9.6      | 9.6      | 10.6     | 10.9     |
| <, less  | pH<br>(stand-<br>ard<br>units)  | Station                            | ;        | ;        | i        | :        | 7.8      | ;        | ŧ        | 7.8      | 8.0      | ;        | 1.1      | ;        | į        | t<br>t   | ;        | ;        | 7.8      | ;        | !        | :        | 7.3      | :        | ;        | 7.3      | ;        | 7.4      | 7.5      | 7.5      | 7.8      | 7.8      |
|  | Temper-<br>ature<br>(°C)  |                                    | 9.5      | 1.0      | 5.5      | 1.0      | 2.5      | ;        | 10.0     | 10.0     | 17.5     | 7.5      | 19.5     | 15.5     | 16.5     | 22.0     | 24.0     | 23.5     | 18.0     | 19.0     | 20.0     | 25.0     | 24.5     | 25.5     | 16.5     | 20.0     | 23.0     | 12.5     | 0.9      | 4.5      | 1.0      | 2.0      |
|  | Flow,<br>instan-<br>taneous<br>(ft <sup>3</sup> /s)                     |                                    | 25       | 25       | 14       | 18       | 45       | :        | 23       | 29       | 37       | 51       | 39       | 1,280    | 214      | 108      | 28       | 17       | 17       | 31       | 64       | 31       | 14       | 89       | 246      | 113      | 38       | 95       | 29       | 16       | 14       | 34       |
|  | Time  |                                    | 1250     | 1155     | 1525     | 1500     | 1430     | 0630     | 1110     | 1500     | 1320     | 1130     | 1115     | 1815     | 0920     | 1420     | 1440     | 1540     | 1015     | 1115     | 1140     | 1255     | 1050     | 1205     | 1025     | 1045     | 1355     | 0060     | 0915     | 1045     | 1020     | 0060     |
|  | Date of<br>sample   |                                    | 10-23-80 | 12-02-80 | 01-06-81 | 02-09-81 | 02-12-81 | 02-23-81 | 03-12-81 | 03-17-81 | 04-20-81 | 05-19-81 | 05-21-81 | 05-28-81 | 06-03-81 | 06-04-81 | 06-08-81 | 06-16-81 | 06-17-81 | 06-29-81 | 07-02-81 | 07-13-81 | 07-15-81 | 08-04-81 | 08-12-81 | 08-19-81 | 09-09-81 | 09-16-81 | 10-21-81 | 11-19-81 | 12-17-81 | 01-19-82 |
|  | Site<br>number<br>on fig-<br>ure 2.0-1                                  |                                    | 1        |          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |          |

11.0 SUPPLEMENTAL INFORMATION--Continued

Table 11.0-1. -- Surface-water quality data -- Continued

| Site number Date of on fig. sample ure 2.0-1 | of Time | Flow,<br>instan-<br>taneous<br>(ft3/s) | Temper-<br>ature<br>(°C) | pH<br>(stand-<br>ard<br>units) | Dis-<br>solved<br>oxygen<br>(mg/L) | Specific<br>conduct-<br>ance<br>(µS/cm) | Dissolved-<br>solids<br>residue<br>at 105°C<br>(mg/L)        | Dissolved<br>chloride<br>(mg/L<br>as Cl) | Total<br>nitrite<br>nitrogen<br>(mg/L<br>as N) | Total<br>nitrogen<br>NO2+NO3<br>(mg/L<br>as N) | Total ammonia nitrogen (mg/L as N) | Iotal ammonia and organic nitrogen (mg/L as N) | Total nitro- gen (mg/L as N) |
|--|---------|--|--------------------------|--------------------------------|------------------------------------|---|--|--|--|--|------------------------------------|--|------------------------------|
|  |         |  | ाठ                       | ation 0710                     | 05500 Fo                           | untain Cre                              | Station 07105500 Fountain Creek at Colorado SpringsContinued | ado Springs                              | Continue                                       |  |                                    |  |                              |
| 02-23-82                                     | 82 0930 | 33                                     | 0.4                      | 7.8                            | 10.4                               | 570                                     | ;  | ;  | 0.020  | 2.00   | 0.150                              | 0.70   | 2.7                          |
| 03-24-82                                     |         | 19                                     | 7.0                      | 7.8                            | 10.1                               | 049                                     | ;  | :  | <.020  | 2.00   | .100                               | 67.  | 2.8                          |
| é  |         |  |                          | 7.4                            | 8.6                                | 655                                     | ;  | ;  | .050   | 1.40   | .170                               | 1.4  | 2.8                          |
| 05-27-82                                     |         | 120                                    | 16.5                     | 7.3                            | 8.5                                | 456                                     | 1  | ;  | 040  | . 700  | . 140                              | 06.  | 1.6                          |
| 06-16-82                                     | 82 0930 |  |                          | 9.7                            | 8.7                                | 431                                     | ;  | ;  | .030   | .810   | . 190                              | 1.3  | 2.1                          |
| 07-15-82                                     |         |  |                          | 7.7                            | 7.8                                | 573                                     | ;  | ;  | .020   | 1.10   | <.060                              | .90  | 2.0                          |
| 08-11-82                                     | 82 1530 |  |                          | 7.5                            | 8.9                                | 316                                     | ;  | ;  | 040  | . 780  | .120                               | 1.6  | 2.4                          |
| 09-13-82                                     |         | _                                      | 13.0                     | 7.6                            | 8.9                                | ;                                       | 1  | ;  | 040  | . 700  | .110                               | 1.1  | 1.9                          |
| 10-21-82                                     | 82 0915 |  | 4.5                      | 7.9                            | 12.1                               | 393                                     | ;  | ;  | .030   | 1.10   | .080                               | 1.1  | 2.2                          |
| 11-18-82                                     |         |  |                          | 7.8                            | 12.2                               | 434                                     | ;  | ;  | <.020  | 1.40   | 090.                               | .70  | 2.1                          |
| 12-15-82                                     |         |  |                          | 7.5                            | 13.5                               | 592                                     | ;  | ;  | <.020  | 1.90   | .100                               | .70  | 5.6                          |
| 03-24-82                                     | 82 1750 |  | .80 7.0                  | .0 12.5 9.7                    | 9.7                                |   | 3,670 1,280 49 .170  | 67                                       | .170   |  | .180                               | 1.1  | 5.9                          |
| 06-16-82                                     |         |  | 21.                      | 8.2                            | 6.7                                | 1,670                                   | 1,280  | 47                                       | .120   | 6.20   | .130                               | 1.9  | 8.1                          |
| 09-13-82                                     | 82 1710 | 0 <300                                 | 10.0                     | 8.8                            | ;                                  | 150                                     | 164  | 5.1                                      | .170   | .500   | .320                               | 8.1  | 8.6                          |
| 10-06-82                                     |         | .58                                    | 15.                      | 9.3                            | 8.8                                | 1,960                                   | 1,480  | <b>79</b>                                | .250   | 9.30   | . 220                              | 2.7  | 12                           |
| 12-15-82                                     |         |  | •                        | 8.6                            | 12.3                               | 1,850                                   | 1,510  | 73                                       | .110   | 8.50   | <.060                              | .70  | 9.5                          |
|  |         |  |                          | Stat                           | ion 38484                          | Station 384840104481200                 | Canal No.  | 4 at headgate                            | ate  |  |                                    |  |                              |
| 04-28-82                                     |         |  | 15.5                     | 8.9                            | 4.5                                | 800                                     | 465  | 87                                       | .050   | .380   | 15.0                               | 21   | 21                           |
| 05-10-82                                     | -       |  | 15.0                     | 7.1                            | 6.4                                | 815                                     | 470  | <b>7</b> 43                              | .050   | .210   | 17.0                               | 22   | 22                           |
| 05-27-82                                     |         | 0 10                                   | 16.0                     | 6.9                            | 5.8                                | 879                                     | 397  | 32                                       | .040   | .300   | 10.0                               | 20   | 20                           |
| 06-16-82                                     |         |  | 18.5                     | 7.0                            | 5.5                                | 721                                     | 445  | 29                                       | .080   | 5.40   | 10.0                               | 9.1  | 15                           |
| 07-15-82                                     | 82 1115 | 5 12                                   | 20.0                     | 8.9                            | 5.4                                | 778                                     | 416  | 34                                       | :  | 5.40   | 12.0                               | 18   | 23                           |
| 08-11-82                                     | 82 1430 |  | 20.5                     | 8.9                            | 5.3                                | 765                                     | 787  | 32                                       | .220   | .670   | 9.30                               | 9.3  | 10                           |
| 09-29-82                                     |         | 5 12                                   | 12.5                     | 7.1                            | 7.8                                | 691                                     | 428  | 32                                       | . 280  | .900   | 07.9                               | 8.3  | 9.5                          |
| 10-21-82                                     |         |  | 14.5                     | 4.9                            | 5.9                                | 777                                     | 471  | 36                                       | 1.30   | 2.00   | 10.0                               | 15   | 17                           |
| 11-18-82                                     |         |  | 13.0                     | 6.9                            | 0.9                                | 795                                     | 767  | 41                                       | <.020  | .500   | 14.0                               | 17   | 18                           |
|  |         |  | St                       | Station 384720104455400        | 720104455                          | 6400 Canal No                           |  | 4 downstream from                        | Sand Creek                                     | וע   |                                    |  |                              |
| 05-10-82                                     | 82 1130 | 0 7.9                                  |                          | 7.3                            | 7.2                                | 725                                     | 7443   | 30                                       | .130   | .880   | 9.40                               | 11   | 12                           |
| 06-16-82                                     |         |  |                          | 7.0                            | 4.4                                | 707                                     | 435  | 28                                       | .180   | . 600  | 9.50                               | 14   | 15                           |
| 09-29-82                                     |         |  | 13.0                     | : ;                            | ; ;                                | 720                                     | 433  | 87 87                                    | 700  | 1.10   | 6.50                               | 2 5  | 3 =                          |
| ì  |         |  |                          |                                |                                    | )<br>1                                  | )  | )  | •  | •  | )<br>;                             | <b>;</b>                                       | ;                            |

11.0 SUPPLEMENTAL INFORMATION--Continued

Table 11.0-1.--Surface-water quality data--Continued

| Site<br>number<br>on fig-<br>ure 2.0-1 | Date of<br>sample | Time | Flow,<br>instan-<br>taneous<br>(ft³/s) | Temper-<br>ature<br>(°C) | pH<br>(stand-<br>ard<br>units) | Dis-<br>solved<br>oxygen<br>(mg/L) | Specific<br>conduct-<br>ance<br>(µS/cm) | Dissolved-<br>solids<br>residue<br>at 105°C<br>(mg/L)                            | Dissolved<br>chloride<br>(mg/L<br>as Cl) | Total<br>nitrite<br>nitrogen<br>(mg/L<br>as N) | Total<br>nitrogen<br>NO <sub>2</sub> +NO <sub>3</sub><br>(mg/L<br>as N) | Total ammonia nitrogen (mg/L as N) | Total ammonia and organic nitrogen (mg/L as N) | Total<br>nitro-<br>gen<br>(mg/L<br>as N) |
|--|-------------------|------|--|--------------------------|--------------------------------|------------------------------------|---|--|--|--|---|------------------------------------|--|--|
|  |                   |      |  | Stat                     | Station 384610104441700        | 01044417                           | 00 Canal No.                            | 1 1  | 4 downstream from Hancock Road           | Jancock Roa                                    | שַּ   |                                    |  |  |
|  | 05-10-82          | 1245 | 8.5                                    |                          | 7.6                            | 8.1                                | 770                                     | 760  | 32                                       | 0.250  | 3.00  | 11.0                               | 14   | 17                                       |
|  | 06-16-82          | 1720 | 30                                     | 19.0                     | 7.0                            | 9.4                                | 969                                     | 420  | 28                                       | .190   | .620  | 8.60                               | 12   | 13                                       |
|  | 09-29-82          | 1430 | 12                                     |                          | ;                              | 1                                  | 730                                     | 433  | 32                                       | .340   | 1.20  | 6.40                               | 10   | 11                                       |
|  |                   |      |  | Stat                     | Station 384458104423000        | 81044230                           | 00 Canal No.                            | - 1  | 4 near Fountain Valley School            | lley School                                    |   |                                    |  |  |
|  | 05-10-82          | 1345 | 8.2                                    | 19.5                     | 7.6                            | 9.0                                | 814                                     | 461  | 70                                       | .210   | .560  | 17.0                               | 21   | 22                                       |
|  | 06-16-82          | 1810 | 31                                     | 18.5                     | 7.1                            | 6.4                                | 799                                     | 407  | 28                                       | . 240  | . 780   | 8.00                               | 11   | 12                                       |
|  | 09-29-82          | 1905 | 11                                     | ;                        | :                              | :                                  | 720                                     | 433  | 32                                       | .310   | 1.40  | 6.80                               | 11   | 12                                       |
|  |                   |      |  |                          | Station                        | Station 384450104415300            | 1                                       | Big Johnson  | Johnson Reservoir outflow                | utflow   |   |                                    |  |  |
| œ                                      | 05-10-82          | 1500 | 31                                     |                          | 7.6                            | 8.9                                | 810                                     | 519  | 42                                       | .120   | .900  | 9.60                               | 8.3  | 9.5                                      |
|  | 06-16-82          | 0920 | 8.4                                    | .16.5                    | 7.5                            | 9.9                                | 775                                     | 504  | 42                                       | .180   | .790  | 6.80                               | 7.0  | 7.8                                      |
|  | 10-06-82          | 1045 | 14                                     | 14.0                     | 7.8                            | 7.5                                | 705                                     | 977  | 34                                       | .270   | 2.40  | 1.80                               | 4.1  | 6.5                                      |
|  |                   |      |  | Station                  | Station 384833104473900        | 4473900                            | Spring Cr                               | Spring Creek downstream from Las Vegas Street                                    | eam from La                              | s Vegas St                                     | eet   |                                    |  |  |
| 6                                      | 03-24-82          | 1710 | 1.8                                    | 10.0                     | 8.5                            | 9.5                                | 1,100                                   | 698  | 29                                       | 009.   | 9.60  | 080                                | .95  | 9.7                                      |
|  | 06-16-82          | 1400 | 2.7                                    | 22.5                     | 8.1                            | 4.9                                | 1,050                                   | 790  | 20                                       | .120   | 4.70  | 060.                               | 2.0  | 6.7                                      |
|  | 09-13-82          | 1630 | <110                                   | 15.0                     | 7.9                            | 1                                  | 170                                     | 277  | 8.0                                      | 090  | . 800   | .140                               | 7.3  | 8.1                                      |
|  | 10-06-82          | 1530 | 2.7                                    | 16.5                     | 8.6                            | <b>8</b> .3                        | 1,400                                   | 981  | 28                                       | 060.   | 8.70  | <.060                              | 2.0  | Ξ  |
|  | 12-15-82          | 1545 | 1.6                                    | 3.0                      | 8.4<br>Station                 | 10.8                               | 1,350<br>0 Fountai                      | 8.4 10.8 1,350 1,010 50 .<br>Station 07105530 Fountain Creek below Janitell Road | 50<br>Janitell                           | . 100<br>Road                                  | 11.0  | <.060                              | 1.0  | 12                                       |
|  |                   |      | ć                                      |                          |                                |                                    |   |  |  |  | •   | 6                                  | č  | L  |
| 2                                      | 02-17-61          | 1030 | 0 / 8                                  | 11.0                     |                                | 0.0                                | 027                                     | 515  | <b>?</b> • •                             | 100  | 1.10  | 10.0                               | <b>*</b> 7 -                                   | 15                                       |
|  | 04-20-81          | 1415 | 7.                                     | 17.0                     | 7.                             |                                    | 2 1                                     | 627  | 3.                                       | 080  | 076   | 2 1                                | 7 7  | 15                                       |
|  | 05-21-81          | 1215 | 79                                     | 18.0                     | 7.1                            | 7.1                                | ;                                       | 1.200  | 27                                       | 080  | 086   | ;                                  | 15   | 16                                       |
|  | 06-17-81          | 1200 | 89                                     | 20.0                     | 7.1                            | 6.5                                | 869                                     | 539  | 39                                       | 060.   | .620  | ;                                  | 14   | 15                                       |
|  | 07-15-81          | 1215 | 99                                     | 24.5                     | 7.1                            | 6.0                                | ;                                       | 580  | 70                                       | .130   | .780  | 8.90                               | 11   | 12                                       |
|  | 08-19-81          | 1220 | 143                                    | 20.0                     | 7.1                            | 6.9                                | 1                                       | 333  | 23                                       | 090.   | .620  | 4.50                               | 8.9  | 7.4                                      |
|  | 09-16-81          | 1020 | 124                                    | 14.5                     | 7.3                            | 7.9                                | 623                                     | 426  | 33                                       | . 180  | .910  | 6.10                               | 10   | 11                                       |
|  | 10-21-81          | 1040 |  | 9.5                      | 7.3                            | 8.8                                | 641                                     | 426  | 36                                       | . 140  | .830  | :                                  | 11   | 12                                       |
|  | 11-19-81          | 1145 | 38                                     | 12.0                     | 7.2                            | 7.2                                | :                                       | 687  | 20                                       | .180   | 066.  | 12.0                               | 16   | 17                                       |
|  | 12-17-81          | 1115 |  | 9.0                      | 7.2                            | 8.1                                | ;                                       | 523  | 39                                       | .110   | 1.70  | 12.0                               | 14   | 16                                       |
|  | 01-19-82          | 1000 | 98                                     | 8.5                      | 7.2                            | 8.7                                | 804                                     | 487  | 45                                       | 020.   | 1.10  | 1                                  | 17   | 18                                       |
|  | 02-23-82          | 1045 | 91                                     | 9.0                      | 7.0                            | 8.6                                | 729                                     | 677  | 42                                       | 090.   | .990  | 12.0                               | 15   | 16                                       |
|  |                   |      |  |                          |                                |                                    |   |  |  |  |   |                                    |  |  |

11.0 SUPPLEMENTAL INFORMATION--Continued

Table 11.0-1.--Surface-water quality data--Continued

| Site<br>number<br>on fig-<br>ure 2.0-1 | Date of<br>sample | Тіте | Flow,<br>instan-<br>taneous<br>(ft³/s) | Temper-<br>ature<br>(°C) | pH<br>(stand-<br>ard<br>units) | Dis-<br>solved<br>oxygen<br>(mg/L) | Specific<br>conduct-<br>ance<br>(µS/cm) | Dissolved-<br>solids<br>residue<br>at 105°C<br>(mg/L)        | Dissolved<br>chloride<br>(mg/L<br>as Cl) | Total<br>nitrite<br>nitrogen<br>(mg/L<br>as N) | Total<br>nitrogen<br>NO2+NO3<br>(mg/L<br>as N) | Total ammonia nitrogen (mg/L as N) | Total ammonia and organic nitrogen (mg/L as N) | Total<br>nitro-<br>gen<br>(mg/L<br>as N) |
|--|-------------------|------|--|--------------------------|--------------------------------|------------------------------------|---|--|--|--|--|------------------------------------|--|--|
|  |                   |      |  | Sta                      | tion 0710                      | 5530 For                           | untain Cre                              | Station 07105530 Fountain Creek below Janitell RoadContinued | nitell Road                              | Continue                                       |  |                                    |  |  |
| 10                                     | 03-24-82          | 1030 | 19                                     |                          | 7.0                            | 8.0                                | 770                                     | 495  | 94                                       | 0.080  | 0.940  | 13.0                               | 17   | 18                                       |
|  | 04-28-82          | 1230 | 9/                                     | 17.0                     | 7.3                            | 7.1                                | 793                                     | 487  | 04                                       | 060.   | 1.20   | 10.0                               | 15   | 16                                       |
|  | 05-27-82          | 1245 | 149                                    |                          | 7.4                            | 8.3                                | 1                                       | 303  | 17                                       | 090.   | .700   | 6.60                               | 6.5  | 7.2                                      |
|  | 06-16-82          | 1100 | 111                                    |                          | 7.4                            | 7.8                                | :                                       | 385  | 31                                       | .070   | .890   | 5.50                               | 5.5  | 6.4                                      |
|  | 07-15-82          | 1200 | 69                                     |                          | 7.0                            | 6.7                                | 798                                     | 493  | 34                                       | .210   | 096.   | 11.0                               | 13   | 14                                       |
|  | 08-11-82          | 1315 | 136                                    | 20.5                     | 7.0                            | 6.9                                | 595                                     | 385  | 24                                       | .170   | .880   | 5.10                               | 9.3  | 10                                       |
|  | 09-13-82          | 1115 | 172                                    | 14.0                     | 7.5                            | 8.6                                | ;                                       | 376  | 21                                       | .550   | 1.30   | 5.20                               | 4.6  | 11                                       |
|  | 10-21-82          | 1100 | 95                                     | 11.0                     | 6.9                            | 8.8                                | 677                                     | 438  | 29                                       | .950   | 2.00   | 5.30                               | 9.5  | 12                                       |
|  | 11-18-82          | 1140 | 78                                     | 10.5                     | 7.3                            | 9.5                                | 146                                     | 874  | 36                                       | <.020  | 1.30   | 9.80                               | 10   | 11                                       |
|  | 12-15-82          | 1030 | 98                                     | 8.5                      | 7.1                            | 10.1                               | 813                                     | 521  | 77                                       | .130   | 1.20   | 13.0                               | 15   | 16                                       |
|  |                   |      |  | Statio                   | tation 384747104470500         | 04470500                           |   | Garden Valley Sewage Treatment                               | P Treatment                              | Plant outfall                                  | [a11]  |                                    |  |  |
| 11                                     | 06-16-82          | 1550 | .03                                    | 17.0                     | 6.9                            | 7.4                                | 864                                     | 527  | 97                                       | 3.90   | 13.0   | 2.90                               | 9.5  | 23                                       |
|  | 09-13-82          | 1245 | .10                                    | 16.5                     | 8.9                            | 8.4                                | 901                                     | 979  | 110                                      | .330   | 10.0   | 1.20                               | 3.8  | 14                                       |
|  | 12-15-82          | 1215 | .16                                    | 4.5                      | 7.0                            | 12.4                               | 1,160                                   | 780  | 200                                      | .020   | 19.0   | 060.                               | 1.1  | 20                                       |
|  |                   |      |  | Statio                   | tation 384758104452900         | 04452900                           | - 1                                     | Sand Creek downstream from Academy Boulevard                 | am from Acad                             | demy Bouler                                    | rard   |                                    |  |  |
| 12                                     | 03-24-82          | 1630 | .05                                    | 10.5                     | 8.5                            | 13.4                               | 980                                     | 747  | 18,                                      | <.020  | 3.70   | <.060                              | .89  | 9.4                                      |
|  | 06-16-82          | 1330 | 80.                                    | 25.5                     | 7.5                            | 5.7                                | ;                                       | 693  | 15                                       | .030   | 3.60   | 070.                               | 1.6  | 5.5                                      |
|  | 09-13-82          | 1415 | E.80                                   | 11.0                     | 8.0                            | 7.8                                | 550                                     | 488  | 11                                       | <.020  | 3.90   | 080.                               | 1.1  | 5.1                                      |
|  | 12-15-82          | 1515 | .33                                    | 3.0                      | 7.0                            | 10.7                               | 1,860                                   | 1,150  | 21                                       | .050   | 5.30   | 090.                               | 06.  | 6.2                                      |
|  |                   |      |  | Station                  |                                | 384713104463200                    | Sand Creek                              | eek downstream   | from Las                                 | Vegas Street                                   | eet  |                                    |  |  |
| 13                                     | 03-24-82          | 1540 | .31                                    | 12.5                     | 8.2                            | 9.5                                | 335                                     | 239  | 9.3                                      | .040   | 11.0   | .860                               | 1.5  | 13                                       |
|  | 06-16-82          | 1225 | .71                                    | 25.0                     | 7.5                            | 9.9                                | 138                                     | 361  | 3.9                                      | . 230  | . 280  | . 421                              | 8.4  | 5.1                                      |
|  | 09-13-82          | 1500 | <.60                                   | 15.0                     | 8.3                            | 7.9                                | :                                       | 250  | 7.1                                      | .040   | 2.30   | .070                               | 1.7  | 0.4                                      |
|  |                   |      |  | Ωİ                       | Station 38                     | 384633104464800                    |   | Stratmoor Valley Tributary                                   | ey Tributar                              | y at I-25                                      |  |                                    |  |  |
| 14                                     | 03-24-82          | 1500 | .13                                    | 14.0                     | 8.4                            | 9.1                                | 1,260                                   | 978  | 35                                       | .020   | 3.30   | .110                               | 1.3  | 9.4                                      |
|  | 06-16-82          | 1145 | .41                                    | 21.5                     | 8.7                            | 9.8                                | 1,690                                   | 1,350  | 32                                       | 090.   | 1.00   | 080                                | 2.4  | 3.4                                      |
|  | 10-06-82          | 1220 | 77.                                    |                          | 8.8                            | 10.4                               | 1,850                                   | 1,440  | 35                                       | 090.   | 3.50   | . 100                              | 2.2  | 5.7                                      |
|  | 12-15-82          | 1400 | 1.1                                    |                          | 8.2                            | 12.2                               | 1,490                                   | 1,160  | 35                                       | 090.   | 4.50   | . 200                              | 1.4  | 5.9                                      |

11.0 SUPPLEMENTAL INFORMATION--Continued

Table 11.0-1.--Surface-water quality data--Continued

| Site<br>number<br>on fig-<br>ure 2.0-1 | Date of<br>sample | Time  | Flow,<br>instan-<br>taneous<br>(ft³/s) | Temper-<br>ature<br>(°C) | pH<br>(stand-<br>ard<br>units) | Dis-<br>solved<br>oxygen<br>(mg/L) | Specific<br>conduct-<br>ance<br>(µS/cm) | Dissolved-<br>solids<br>residue<br>at 105°C<br>(mg/L) | Dissolved<br>chloride<br>(mg/L<br>as Cl) | Total nitrite nitrogen (mg/L as N) | Total<br>nitrogen<br>NO <sub>2</sub> +NO <sub>3</sub><br>(mg/L<br>as N) | Total ammonia nitrogen (mg/L as N) | Total annonia and organic nitrogen (mg/L as N) | Total nitro- gen (mg/L as N) |
|--|-------------------|-------|--|--------------------------|--------------------------------|------------------------------------|---|---|--|------------------------------------|---|------------------------------------|--|------------------------------|
|  |                   |       |  |                          | Station 384617104460600        | 84617104                           |   | Stubbs-Miller Ditch at headgate                       | Ditch at h                               | eadgate                            |   |                                    |  |                              |
| 15                                     | 03-24-82          | 1410  | 1.3                                    | 11.0                     | 8.0                            | 8.3                                | 1 0                                     | 482   | 39                                       | 0.210                              | 1.10  | 12.0                               | 16   | 17                           |
|  | 79-51-71          | 1310  | cı                                     | o. v                     | ·.                             | 7.                                 | 820                                     | 200   | <b>7</b>                                 | 0/1.                               | 1.50  | 17.0                               | 91   | 81                           |
|  |                   |       |  |                          | Sta                            | Station 07105780                   |   | B Ditch Drain near Security                           | near Securi                              | ţ                                  |   |                                    |  |                              |
| 16                                     | 04-02-81          | 1415  | .07                                    | 14.5                     | :                              | ;                                  | 6,500                                   | ;   | ;  | :                                  | :   | :                                  | ;  | ;                            |
|  | 04-23-81          | 0845  | 60.                                    | 10.5                     | ;                              | :                                  | 4,250                                   | 1   | :  | ;                                  | ;   | :                                  | ;  | ;                            |
|  | 05-20-81          | 0840  | . 10                                   | <b>8</b><br>5.5          | :                              | 1                                  | 2,000                                   | ;   | ;  | ;                                  | ;   | :                                  | ;  | ;                            |
|  | 06-04-81          | 1545  | 1.3                                    | 22.0                     | : :                            | : :                                | 2,700                                   | 1 1   | : :                                      | : :                                | : :   | : :                                | ; ;  | : :                          |
|  | 10 77 10          | 0000  | 5 !                                    | 2.                       |                                |                                    | 2011                                    |   |  |                                    |   |                                    |  |                              |
|  | 08-03-81          | 1010  | .45                                    | 21.0                     | :                              | :                                  | 2,000                                   | ;   | :  | :                                  | ;   | ;                                  | ŧ  | ł                            |
|  | 08-07-81          | 1455  | .76                                    | 24.0                     | ;                              | ;                                  | 2,000                                   | 1   | ;  | :                                  | ;   | ;                                  | <b>:</b>                                       | :                            |
|  | 08-21-81          | 1810  | .20                                    | 24.0                     |                                | 1 ;                                | 000,9                                   | 1   | 1 6                                      | i (                                | 1 4   | 1                                  |  | 1                            |
|  | 10-23-81          | 0930  | . 0.<br>                               | 0.0                      | × •                            | 10.5                               | 021 9                                   | 5,920   | 120                                      | .020                               | 17.0  | <.060<br>220                       | 2.1  | 19                           |
|  | 19-91-11          | crer  | Τ.                                     | ٥.                       | ٥٠/                            | 7.01                               | 0,1,0                                   | 0,420   | 190                                      | 000.                               | 19.0  | 077.                               | 0.1  | 17                           |
|  | 12-14-81          | 1220  | .17                                    | 3.5                      | 7.9                            | 13.1                               | 1                                       | 7,170   | 160                                      | .020                               | 27.0  | .170                               | 1.5  | 53                           |
|  | 01-18-82          | 1130  | . 18                                   | 1.0                      | 7.6                            | 9.1                                | 5,410                                   | 2,090   | 120                                      | 1.70                               | 4.20  | .180                               | 1.6  | 5.8                          |
|  | 02-22-82          | 1315  | .17                                    | 7.0                      | 7.8                            | 12.2                               | 4,830                                   | 4,520   | 82                                       | . 160                              | 12.0  | . 140                              | 1.6  | 7 7                          |
|  | 03-24-82          | 1215  | = :                                    | 8.5                      | 7.5                            | 15.0                               | 6,590                                   | 6,650   | 110                                      | . 100                              | 15.0  | .110                               | 1:1  | 16                           |
|  | 04-28-82          | 1400  | 90.                                    | 20.5                     | 7.6                            | 6.5                                | 3,640                                   | 1   | :  | . 130                              | 7.50  | .210                               | 2.1  | 9.6                          |
|  | 05-28-82          | 1210  | .21                                    | 23.0                     | 7.4                            | 10.8                               | 4,430                                   | 3,870   | 85                                       | .130                               | 7.70  | .220                               | 1.8  | 9.5                          |
|  | 06-16-82          | 1515  | .25                                    | 24.0                     | 7.5                            | 7.2                                | 4,390                                   | 3,900   | 65                                       | . 120                              | 7.70  | .170                               | 1.0  | 8.7                          |
|  | 07-15-82          | 1345  | .35                                    | 25.5                     | 9.6                            | × .5                               | 4,650                                   | 1 7   | : 5                                      | .060                               | 11.0  | .150                               | 2.1  | 13                           |
|  | 08-24-82          | 1525  | . 53.                                  | 19.0                     | ? !                            | : :                                | 5,500                                   | 3,140   | 6 1                                      | 1 1                                | 0.0   | : :                                | 7 :  | 0: 1                         |
|  | 00-13-82          | 127.5 | 7.3                                    | . 01                     | 7 5                            | 9                                  | 076 6                                   | 1 300   | 0  | 0,0                                | 07. 3   | 040                                | -  | œ                            |
|  | 10-16-82          | 1340  | 36.                                    | 13.0                     | ? ;                            | ; ;                                | 5,500                                   | 2001  | 3  |                                    | ?<br>:  |                                    | ?<br>• •                                       | ?<br>; ;                     |
|  | 10-21-82          | 1415  | E.31                                   | 14.0                     | 7.8                            | 10.4                               | 4,000                                   | 3,520   | 58                                       | .200                               | 11.0  | 060.                               | 1.8  | 13                           |
|  | 11-18-82          | 1325  | .31                                    | 8.0                      | 8.3                            | 14.5                               | 3,400                                   | 3,010   | 63                                       | .120                               | 10.0  | . 100                              | 1.6  | 12                           |
|  | 12-15-82          | 1300  | 07.                                    | 0.                       | 8.0                            | !                                  | 4,560                                   | 4,270   | 95                                       | .240                               | 15.0  | 090.                               | .80  | 16                           |
|  |                   |       |  |                          | Statio                         | n 384531                           | Station 384531104432200                 | Windmill Gulch at Bradley                             | ulch at Bra                              | dley                               |   |                                    |  |                              |
| 17                                     | 03-24-82          | 1150  | .15                                    | 8.0                      | 8.3                            | 10.8                               | 520                                     | 360   | 13                                       | <.020                              | <.100   | 080                                | .88  | ;                            |
|  | 06-16-82          | 1100  | 60.                                    | 16.0                     | 7.3                            | 3.9                                | 264                                     | 382   | 11                                       | <.020                              | <.100   | <.060                              | 1.3  | ;                            |
|  | 09-13-82          | 1200  | E.60                                   | 13.0                     | 7.9                            | 8.9                                | 009                                     | 519   | 16                                       | <.020                              | <.100   | 090.                               | 1.3  | ; ;                          |
|  | 12-15-82          | 1130  | E.05                                   | 2.0                      | 7.4                            | 11.1                               | 642                                     | 391   | 13                                       | .030                               | . 700   | . 120                              | . 70   | 1.4                          |

11.0 SUPPLEMENTAL INFORMATION--Continued

Table 11.0-1. -- Surface-water quality data -- Continued

| 917-82 1200  | Date of<br>sample | Time | Flow,<br>instan-<br>taneous<br>(ft³/s) | Temper-<br>ature<br>(°C) | pH<br>(stand-<br>ard<br>units) | Dis-<br>solved<br>oxygen<br>(mg/L) | Specific<br>conduct-<br>ance<br>(µS/cm) | Dissolved-<br>solids<br>residue<br>at 105°C<br>(mg/L) | Dissolved chloride (mg/L as Cl) | Total<br>nitrite<br>nitrogen<br>(mg/L<br>as N) | Total<br>nitrogen<br>NO <sub>2</sub> +NO <sub>3</sub><br>(mg/L<br>as N) | Total ammonia nitrogen (mg/L as N) | Total ammonia and organic nitrogen (mg/L as N) | Total<br>nitro-<br>gen<br>(mg/L<br>as N) |
|--|-------------------|------|--|--------------------------|--------------------------------|------------------------------------|---|---|---------------------------------|--|---|------------------------------------|--|--|
| 1200   |                   |      |  | Stat                     | ion 38441                      | 81044407                           |   | ty Sewage T   | reatment Pl                     | ant outfal                                     | 1   |                                    |  |  |
| 1200   | 3-17              | 200  | :                                      | ;                        | ;                              | ;                                  | :                                       | ;   | ;                               | ;  | 0.290   | 25.0                               | ;  | :  |
| 1200   | 3-29              | 200  | ;                                      | ;                        | ;                              | ;                                  | 1                                       | ;   | ;                               | ;  | .420  | 25.0                               | ;  | ;  |
| 1200               180     23.0  | 4-15              | 200  | :                                      | ;                        | ;                              | 1                                  | ;                                       | ;   | :                               | ;  | .230  | 24.0                               | ;  | ;  |
| 1200   | 07-50             | 200  | :                                      | ;                        | ;                              | ;                                  | ;                                       | ;   | ;                               | ;  | . 180   | 23.0                               | :  | ;  |
| 1200   | 35-05             | 200  | ;                                      | ;                        | ;                              | :                                  | ;                                       | ;   | ;                               | . 100  | <.100   | 21.0                               | ;  | ;  |
| 1200                 140   22.0       130     12.0             140     18.0           13.0   | 5-19              | 200  | :                                      | ;                        | :                              | ;                                  | ;                                       | 1   | 1                               | 1  | .390  | 22.0                               | ;  | ;  |
| 1100   | 96-03             | 200  | ;                                      | ;                        | ;                              | 1                                  | 1                                       | ;   | ;                               | ;  | <.100   | 23.0                               | :  | ;  |
| 1330   | 6-15              | 100  | ;                                      | :                        | ;                              | ;                                  | ;                                       | ;   | ;                               | ;  | .140  | 22.0                               | ;  | ;  |
| 1330                 140   19.0       1310   17.0   13.0   17.0   13.0   17.0   13.0   17.0   13.0   17.0   13.0   17.0   13.0   17.0   13.0   17.0   13.0   17.0   13.0   17.0   13.0   17.0   13.0   17.0   13.0   17.0   13.0   17.0   13.0   1 | 96-28             | 330  | ;                                      | ;                        | ;                              | ;                                  | :                                       | ;   | ;                               | ;  | .410  | 18.0                               | ;  | ;  |
| 1200                   140   19.0     130   17.0   17.0         | 7-15              | 130  | :                                      | ;                        | :                              | ;                                  | :                                       | ;   | 1                               | ;  | .170  | 22.0                               | ;  | :  |
| 130                     1310   17.0         1310   17.0       1310   17.0       1310   17.0       1310   17.0       1310   17.0       1310   17.0       1310   17.0     1310   17.0       1310   17.0       1310   17.0     1310   17.0     17.0             | 37-29             | 200  | :                                      | ;                        | ;                              | ;                                  | ;                                       | ;   | ;                               | ;  | .140  | 19.0                               | ;  | ;  |
| 1500   | 8-10              | 130  | ;                                      | ;                        | ;                              | ;                                  | ;                                       | ;   | ;                               | ;  | .310  | 17.0                               | :  | ;  |
| 9550 100 21.0 100 11.5 100 23.0 100 23.0 100 23.0 100 23.0 100 23.0 100 23.0 100 23.0 100 23.0 100 23.0 100 23.0 100 23.0 100 23.0 100 24.0 100 24.0 100 24.0 100 24.0   | 9-07              | 200  | :                                      | ;                        | ;                              | ;                                  | ;                                       | ;   | ;                               | :  | <.100   | 20.0                               | ;  | ;  |
| 1115   | 9-21              | 550  | ;                                      | {                        | ;                              | ;                                  | :                                       | ;   | ;                               | ;  | . 100   | 21.0                               | :  | ;  |
| 1115   | 90-0              | 006  | :                                      | ;                        | :                              | :                                  | !                                       | ;   | ;                               | ;  | .200  | 20.0                               | :  | ;  |
| 1345   | 0-21              | 115  | :                                      | :                        | :                              | :                                  | ;                                       | ;   | ;                               | ;  | .100  | 24.0                               | ;  | ;  |
| 0830   | 1-02              | 345  | ;                                      | :                        | ;                              | 1                                  | -                                       | ;   | ;                               | ;  | .100  | 23.0                               | :  | :  |
| 1125   | 1-15              | 830  | ;                                      | !                        | :                              | ł                                  | 1                                       | ;   | :                               | ;  | .200  | 24.0                               | :  | :  |
| Station 384356104425400 Crews Gulch downstream from Quebec Street  120   | 1-29              | 125  | :                                      | ;                        | 1                              | :                                  | !                                       | ;   | ;                               | :  | .200  | 23.0                               | :  | ;  |
| Station 384356104425400 Crews Gulch downstream from Quebec Street  1120    .43    13.0    8.4    8.1    1,320    916    49    .030    .150    .220    1.5  | 2-15              | 000  | !                                      | :                        | ;                              | ;                                  | :                                       | ;   | ;                               | :  | <.100   | 24.0                               | :  | :  |
| Station 384356104425400 Crews Gulch downstream from Quebec Street  1120 .43 13.0 8.4 8.1 1,320 916 49 .030 .150 .220 1.5  1000 .87 16.0 7.6 7.1 1,310 965 49 .090 .220 .260 1.5  1000 .84 14.5 8.4 7.3 1,100 882 50 .040 .100 .360 3.9  1000 .87 16.0 7.6 7.1 1,310 965 49 .090 .220 .260 1.5  1000 .87 16.0 7.6 7.1 1,310 882 50 .040 .100 .360 3.9  1150 5.1 15.0 1,210 1,210 1,210 1.20  1150 5.2 14.0 840 1,290 1,290 1.30  1150 6.1 21.0 1,290 1,290 1,290 1.30  1140 3.6 25.0 1,290 1,290 1,290 1.30  1140 3.6 25.0 1,290 1,290 1.30  1150 5.3 25.0 1,290  | 2-28              | 830  | ;                                      | :                        | :                              | ;                                  | :                                       | ;   | ;                               | !  | .300  | 24.0                               | :  | ;  |
| 1120 .43 13.0 8.4 8.1 1,320 916 49 .030 .150 .220 1.5 0900 .87 16.0 7.6 7.1 1,310 965 49 .090 .220 .260 1.5 1000 .84 14.5 8.4 7.3 1,100 882 50 .040 .100 .360 3.9 0945 1.1 2.5 8.5 11.7 1,330 1,020 56 .020 .200 .120 2.8  1150 5.1 15.0 1,210 1,210 1,210 1,290   |                   |      |  | Stati                    | on 384356                      | 10442540                           | ĺ                                       | Gulch downst  | ream from Q                     | uebec Stre                                     | انة   |                                    |  |  |
| 0900 .87 16.0 7.6 7.1 1,310 965 49 .090 .220 .260 1.5 1000 .84 14.5 8.4 7.3 1,100 882 50 .040 .100 .360 3.9 0945 1.1 2.5 8.5 11.7 1,330 1,020 56 .020 .200 .120 2.8  Station 07105820 Clover Ditch Drain near Widefield  1150 5.1 15.0 1,210 840 1,210 1,210 130 6.1 21.0 1,290 1,290 1,290 1,290 1,290 1,290 1,290 1,290 1,290 1,290 1,290 1,290 1,290 1,290 1,290  | 3-24              | 120  | .43                                    |                          | 8.4                            | 8.1                                | 1,320                                   | 916   | 67                              | .030   | . 150   | .220                               | 1.5  | 1.7                                      |
| 1000 .84 14.5 8.4 7.3 1,100 882 50 .040 .100 .360 3.9   0945 1.1 2.5 8.5 11.7 1,330 1,020 56 .020 .200 .120 2.8    Station 07105820 Clover Ditch Drain near Widefield  | 91-90             | 006  | .87                                    |                          | 9.7                            | 7.1                                | 1,310                                   | 965   | 67                              | 060.   | .220  | .260                               | 1.5  | 1.7                                      |
| 0945 1.1 2.5 8.5 11.7 1,330 1,020 56 .020 .200 .120 2.8  1150 5.1 15.0 1,210 1,210 1,210 1,210 15.5 5.0 20.5 14.0 1,290 1,290 1,130 15.5 5.0 20.5 1,130 1,13   | 9-13              | 000  | .84                                    |                          | 8.4                            | 7.3                                | 1,100                                   | 882   | 20                              | 040.   | . 100   | .360                               | 3.9  | <b>7</b> .0                              |
| 1150 5.1 15.0 1,21   | 12-15             | 945  | 1.1                                    |                          | 8.5                            | 11.7                               | 1,330                                   | 1,020   | 26                              | .020   | .200  | . 120                              | 2.8  | 3.0                                      |
| 1150 5.1 15.0 1,210 840 1- 15.0 14.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15   |                   |      |  |                          | Statio                         | n 071058                           | - 1                                     | r Ditch Drai  | n near Wide                     | field  |   |                                    |  |  |
| 1605 5.5 14.0 840 1,290 1,290 1,290 1,130 1,130 1,130 1,290 1,290 1,290 1,290 1,290 1,290  | 04-01             | 150  | 5.1                                    | 15.0                     | ;                              | ;                                  | 1,210                                   | ;   | ;                               | ;  | :   | ;                                  | ;  | ;  |
| 1535 5.0 20.5 1,290 1,13   | 04-22             | 605  | 5.5                                    | 14.0                     | ;                              | :                                  | 840                                     | ;   | ;                               | ;  | ;   | ;                                  | :  | :  |
| 1130 6.1 21.0 1,130 1,130 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.   | )2-5(             | 535  | 5.0                                    | 20.5                     | !                              | :                                  | 1,290                                   | ;   | ;                               | :  | :   | :                                  | :  | :  |
| 1345 5.8 20.0 1,290 1,400 3.6 25.0 1,470 1,470 1,470 1,470 1,470 1,470 1,470   | 35-26             | 130  | 6.1                                    | 21.0                     | ;                              | :                                  | 1,130                                   | ;   | ;                               | ;  | 1   | ;                                  | :  | :  |
| 1400 3.6 25.0 1,470 1,470 1340 4.3 25.0 650 650  | 32-58             | 345  | 5.8                                    | 20.0                     | ;                              | :                                  | 1,290                                   | ;   | ;                               | :  | :   | :                                  | ;  | ;  |
| 1340 4.3 25.0 650 67.0   | 07-05             | 400  | 3.6                                    | 25.0                     | ;                              | :                                  | 1.470                                   | ;   | ;                               | ;  | ;   | ;                                  | !  | :  |
| 0001 0.761   | 07-23             | 340  | ۲,                                     | 25.0                     | ;                              | ;                                  | 650                                     | ;   | ;                               | ;  | ;   | :                                  | :  | ;  |
|  | 10-80             | 270  | איר<br>יי                              | 25.50                    | ;                              | ;                                  | 000                                     | ;   | ;                               | ;  | ;   | ;                                  | ì  | ;  |

11.0 SUPPLEMENTAL INFORMATION -- Continued

Table 11.0-1. -- Surface-water quality data -- Continued

| Site<br>number<br>on fig-<br>ure 2.0-1 | Date of<br>sample | Time | Flow,<br>instan-<br>taneous<br>(ft <sup>3</sup> /s) | Temper-<br>ature<br>(°C) | pH<br>(stand-<br>ard<br>units) | Dis-<br>aolved<br>oxygen<br>(mg/L) | Specific<br>conduct-<br>ance<br>(µS/cm) | Dissolved-<br>solids<br>residue<br>at 105°C<br>(mg/L)            | Dissolved<br>chloride<br>(mg/L<br>as Cl) | Total<br>nitrite<br>nitrogen<br>(mg/L<br>as N) | Total<br>nitrogen<br>NO <sub>2</sub> +NO <sub>3</sub><br>(mg/L<br>as N) | Total ammonia nitrogen (mg/L as N) | Total ammonia and organic nitrogen (mg/L as N) | Total<br>nitro-<br>gen<br>(mg/L<br>as N) |
|--|-------------------|------|---|--------------------------|--------------------------------|------------------------------------|---|--|--|--|---|------------------------------------|--|--|
|  |                   |      |   | Stal                     | Station 07105820               |                                    | over Ditch                              | Clover Ditch Drain near WidefieldContinued                       | Widefield-                               | -Continued                                     |   |                                    |  |  |
| 21                                     | 08-07-81          | 1120 | 2.8   | 23.0                     | ;                              | ;                                  | 1.350                                   | ;  | ł  | ;  | }   | ;                                  | ;  | ;  |
|  | 08-20-81          | 1440 | 3.7   | 22.0                     | ;                              | ;                                  | 1,400                                   | ;  | ;  | !  | }   | ;                                  | ;  | ;  |
|  | 10-23-81          | 1110 | 3.0   | 11.0                     | 7.3                            | 8.6                                | 1,540                                   | 1,110  | 87                                       | 0.720  | 2.70  | 1.20                               | 9.7  | 12                                       |
|  | 11-18-81          | 1415 | 3.6   | 13.5                     | 7.4                            | 6.0                                | 1,300                                   | 922  | 51                                       | 096.   | 2.90  | 1                                  | 14   | 17                                       |
|  | 12-14-81          | 1345 | 4.3   | 11.0                     | 7.3                            | 6.5                                | 1,190                                   | 860  | 41                                       | 1.00   | 3.70  | 14.0                               | 16   | 70                                       |
|  | 01-15-82          | 1230 | 3.3   | 8.5                      | 7.0                            | 8.6                                | 1,260                                   | 818  | 39                                       | .450   | 2.00  | 21.0                               | 19   | 21                                       |
|  | 02-22-82          | 1400 | 4.7   | 13.5                     | 7.5                            | 9.3                                | 1,250                                   | 858  | 42                                       | 077  | 3.40  | 14.0                               | 18   | 21                                       |
|  | 03-24-82          | 1445 | 3.5   | 15.0                     | 7.2                            | 8.5                                | 1,210                                   | 1  | ;  | .480   | 3.20  | 14.0                               | 18   | 21                                       |
|  | 04-28-82          | 1445 | 4.5   | 20.0                     | 7.5                            | 6.5                                | 1,280                                   | 867  | 09                                       | .610   | 4.00  | 9.90                               | 15   | 19                                       |
|  | 05-27-82          | 1415 | 5.8   | 20.0                     | 7.3                            | 7.6                                | 1,310                                   | ;  | 1  | .680   | 3.70  | 9.90                               | 11   | 15                                       |
|  | 06-16-82          | 1430 | 6.4   | 21.0                     | 7.4                            | 6.5                                | 1,360                                   | 1  | ť  | 1.10   | 4.50  | 8.30                               | =  | 16                                       |
|  | 07-16-82          | 1230 | 2.0   | 24.5                     | 7.4                            | 6.2                                | 1,530                                   | 1,120  | 62                                       | 1.60   | 5.90  | 2.20                               | 5.5  | 11                                       |
|  | 08-12-82          | 1215 | 6.0   | 23.5                     | 7.3                            | 9.0                                | 1,480                                   | . !  | ;  | .500   | 2.60  | 4.20                               | 11   | 14                                       |
|  | 09-13-82          | 1420 | 4.3   | 18.0                     | 7.4                            | 6.9                                | 1,410                                   | ;  | 1  | .510   | 2.40  | 8.50                               | 17   | 19                                       |
|  | 10-21-82          | 1710 | 4.2   | i5.0                     | 7.7                            | 7.4                                | 1                                       | 1  | ;  | .500   | 2.10  | 2.20                               | 17   | 19                                       |
|  | 11-18-82          | 1405 | 3.3   | 12.5                     | 7.9                            | 9.5                                | 1,550                                   | ;  | ;  | 800  | 3.30  | 11.0                               | 14   | 17                                       |
|  | 12-15-82          | 1345 | 1.0   | 8.5                      | 7.5                            | 11.0                               | 1,420                                   | ;  | ;  | 079.   | 2.90  | 9.80                               | 14   | 17                                       |
|  |                   |      |   | Stati                    | ion 38431                      | 21044321                           | 00 Widef                                | Station 384312104432100 Widefield Sewage Treatment Plant outfall | Treatment P                              | lant outfa                                     | =   |                                    |  |  |
| 22                                     | 03-26-82          | 1000 | ;   | ;                        | ł                              | ;                                  | ł                                       | ;  | ;  | ł  | <.100   | 21.0                               | ;  | ;  |
|  | 04-09-82          | 0800 | ;   | ;                        | ł                              | 1                                  | 1                                       | ;  | 1  | ;  | <.100   | 21.0                               | ;  | ;  |
|  | 04-20-82          | 1100 | ;   | ;                        | ;                              | ;                                  | ;                                       | ;  | ;  | ;  | <.100   | 21.0                               | ;  | ;  |
|  | 05-19-82          | 1    | ;   | ;                        | 1                              | ;                                  | 1                                       | 1  | 1 3                                      | 1  | <. 100  | 22.0                               | 1 ;  | ;  |
|  | 06-16-82          | 1240 | . ;<br>8: ;   | 18.0                     | Ξ:                             | 4.6                                | 2,320                                   | 1,400  | 3/0                                      | 070.   | . 790   | 23.0                               | 67   | : :                                      |
|  |                   |      |   |                          | Stati                          | on 07105                           | 825 Foun                                | Station 07105825 Fountain Creek below Widefiel                   | elow Widefi                              | eld  |   |                                    |  |  |
| 23                                     | 02-17-81          | 1415 | 87  | 12.0                     | 7.6                            | <b>60</b>                          | 096                                     | 591  | 14                                       | .350   | 2.30  | 9.70                               | 15   | 17                                       |
|  | 03-18-81          | 1330 | 104   | 13.0                     | 7.7                            | 8.5                                | 890                                     | 530  | 67                                       | .340   | 2.40  | 7.20                               | 19   | 21                                       |
|  | 04-21-81          | 1315 | 88  | 17.0                     | 7.6                            | 6.7                                | 821                                     | 493  | 36                                       | .510   | 2.20  | 5.50                               | 11   | 13                                       |
|  | 05-21-81          | 1630 | 62  | 21.5                     | 7.3                            | 5.5                                | 824                                     | 541  | 97                                       | 1.00   | 3.10  | 3.90                               | 10   | 13                                       |
|  | 06-18-81          | 1030 | 34  | 18.0                     | 7.8                            | 6.9                                | 1,010                                   | 678  | 62                                       | 076.   | 2.30  | 5.70                               | 10   | 12                                       |
|  | 07-15-81          | 1520 | <b>8</b>  | 29.5                     | 7.3                            | 4.5                                | 916                                     | 598  | 47                                       | 1.60   | 2.50  | 9.60                               | 8.5  | 11                                       |
|  | 08-20-81          | 1245 | 122   | 23.5                     | 7.1                            | 5.8                                | 682                                     | 428  | 35                                       | 7490   | 2.00  | 1.90                               | 3.9  | 5.9                                      |
|  | 09-16-81          | 1410 | 124   | 14.0                     | 7.3                            | 7.1                                | 745                                     | 485  | 32                                       | .370   | 2.20  | 3.60                               | 8.9  | 11                                       |
|  | 10-21-81          | 1410 | 100   | 7.5                      | 7.3                            | 9.0                                | 140                                     | 765  | 36                                       | .280   | 2.40  | 6.10                               | 7.3  | 6.7                                      |

11.0 SUPPLEMENTAL INFORMATION--Continued

Table 11.0-1. -- Surface-water quality data -- Continued

117 118 119 119 119 119 110 110 Total nitro-gen (mg/L as N) nitrogen (mg/L as N) Total ammonia and organic 115 8.5 113 5.9 4.2 4.2 4.3 7.2 5.3 6.8 8.7 Total
ammonia
nitrogen
(mg/L
as N) 11.0 6.60 9.50 8.80 7.40 3.20 2.00 2.00 6.80 6.80 Total nitrogen  $NO_2+NO_3$  (mg/L as N)Total
nitrite
nitrogen
(mg/L
as N) Creek below Widefield--Continued 0.170 .280 .250 .120 .420 .360 .370 .990 .310 .500 .510 .150 Dissolved chloride (mg/L as Cl) 84 448 448 449 333 333 51 Dissolved-solids residue at 105°C (mg/L) 697 643 592 592 567 600 491 491 419 419 419 630 Specific conduct-Fountain ance (µS/cm) 929 924 920 800 874 929 929 631 631 648 894 878 Dis-solved oxygen (mg/L) Station 07105825 pH (stand-ard units) Temper-ature (°C) 4.0 8.0 8.0 9.0 15.0 15.0 22.0 26.0 26.0 17.0 11.0 6.5 Flow, instan-taneous (ft³/s) 0900 1400 1300 1215 1315 1530 1530 1740 1730 Time Date of sample 111-20-81 12-17-81 01-19-82 03-23-82 03-24-82 04-28-82 05-28-82 06-16-82 07-15-82 09-13-82 10-21-82 11-18-82 12-15-82 on fig-ure 2.0-1 Site number 23

Table 11.0-2.--Ground-water quality data

[Ground-water quality data are presented by well owners, in ascending order, generally from the north to the south in the study area, in the following order: Stratmoor Hills, Pinello, Venetucci, Security, Widefield, and miscellaneous; °C, degrees Celsius; µS/cm, microsiemens per centimeter at 25 degrees Celsius; mg/L, milligrams per liter; Cl, chloride; N, nitrogen; lat, latitude; long, longitude]

| Date     | Time     | Temper-<br>ature<br>(°C) | pH<br>(stand-<br>ard<br>units) | Specific<br>conduct-<br>ance<br>(µS/cm) | Dissolved-<br>solids<br>residue<br>at 105°C<br>(mg/L) | Dissolved<br>chloride<br>(mg/L<br>as Cl) | Dissolved<br>nitrite<br>nitrogen<br>(mg/L<br>as N) | Dissolved<br>nitrogen<br>NO <sub>2</sub> +NO <sub>3</sub><br>(mg/L<br>as N) | Dissolved<br>ammonia<br>nitrogen<br>(mg/L<br>as N) | Dissolved nitrogen, ammonia and organic (mg/L as N) | Dis-<br>solved<br>nitrogen<br>(mg/L<br>as N) |
|----------|----------|--------------------------|--------------------------------|---|---|--|--|---|--|---|--|
|          |          | Site 3846                | 171044559                      | 001; well S                             | C01506603CAD  | 1 Stratmoo                               | r Hills 4 (  | lat 38°46'1   | 7", long 10  | 4°45'59")   |  |
| 02-13-81 | 1140     | 13.0                     | 7.0                            | 1,000                                   | 694   | 33                                       | 0.000  | 8.80  | 0.180  | 1.3   | 10   |
| 03-19-81 | 1045     | 13.0                     | 6.6                            | 1,020                                   | 668   | 34                                       | .000   | 7.50  | .270   | .94   | 8.4  |
| 05-21-81 | 1545     | 13.5                     | 6.6                            | 901                                     | 651   | 37                                       | .000   | 6.10  | .090   | 1.4   | 7.5  |
| 06-18-81 | 1200     | 13.0                     | 6.6                            |   | 703   | 31                                       | .000   | 6.60  | .210   | .90   | 7.5  |
| 07-17-81 | 1130     | 13.0                     | 6.5                            |   | 659   | 37                                       | .010   | 6.50  | . 260  | 1.2   | 7.7  |
| 09-04-81 | 1055     | 14.0                     | 6.6                            | 943                                     | 651   | 37                                       | .010   | 6.20  | <.060  | 1.1   | 7.3  |
| 09-18-81 | 1050     | 13.5                     | 6.4                            | 945                                     | 661   | 32                                       | .030   | 6.10  | . 230  | 1.2   | 7.3  |
| 10-26-81 | 1145     | 14.0                     | 6.5                            | 934                                     | 648   | 40                                       | <.020  | 6.90  | . 200  | 1.4   | 8.3  |
| 11-24-81 | 1155     | 14.0                     | 6.5                            | 921                                     | 66 <b>6</b>   | 32                                       | .020   | 7.60  | . 360  | .33   | 7.9  |
| 12-21-81 | 1100     | 13.5                     | 6.3                            | 9,76                                    | 664   | 26                                       | <.020  | 6.10  | .270   | 1.3   | 7.4  |
| 01-20-82 | 1125     | 13.5                     | 6.3                            | 929                                     | 628   | 38                                       | <.020  | 6.80  | . 230  | .51   | 7.3  |
| 02-24-82 | 1155     | 13.0                     | 6.2                            | 991                                     | 701   | 34                                       | <.020  | 7.40  | .080   | .72   | 8.1  |
| 03-26-82 | 1210     | 13.0                     | 6.1                            | 1,020                                   | 721   | 33                                       | <.020  | 7.60  | . 190  | 2.6   | 10   |
| 04-30-82 | 0935     | 13.0                     | 6.7                            | 1,010                                   | 729   | 39                                       | <.020  | 7.60  | .130   | 1.4   | 9.0  |
| 05-28-82 | 1110     | 13.0                     | 6.6                            | 928                                     | 636   | 42                                       | <.020  | 5.20  | .070   |   |  |
| 06-23-82 | 1130     | 14.0                     | 7.1                            | 1,100                                   | 715   | 31                                       | <.020  | 7.70  | .090   | 1.6   | 9.3  |
| 07-16-82 | 1100     | 13.0                     | 6.7                            | 933                                     | 677   | 32                                       | <.020  | 7.50  | .200   | .90   | 8.4  |
| 08-13-82 | 1120     | 13.0                     | 6.6                            | 950                                     | 738   | 32                                       | <.020  | 7.50  | .130   | 1.8   | 9.3  |
| 09-17-82 | 1220     | 13.0                     | 6.6                            | 940                                     | 771   | 35                                       | .020   | 7.40  | .090   | 1.9   | 9.3  |
| 10-22-82 | 1240     | 14.0                     |                                |   | 662   | 32                                       | <.020  | 8.20  | <.060  | 2.0   | 10   |
| 11-19-82 | 1130     | 14.0                     | 6.8                            | 930                                     | 651   | 33                                       | <.020  | 8.50  | <.060  | .60   | 9.1  |
| 12-17-82 | 1130     | 13.5                     | 6.8                            | 865                                     | 603   | 40                                       | <.020  | 7.50  | <.060  | .60   | 8.1  |
|          |          | Site 3846                | 191044602                      | :01; well S                             | C01506603CAA  | Stratmoor                                | Hills 5 (1   | at 38°46'19'  | ', long 104  | °46'02")  |  |
| 07-02-81 | 1235     | 15.0                     | 7.0                            | 1,070                                   | 792   | 35                                       | <.010  | 11.0  | <.060  | .98   | 12   |
| 09-04-81 | 1120     | 14.5                     | 6.8                            | 1,120                                   | 806   | 30                                       | .000   | 6.80  | <.060  | 1.4   | 8.2  |
| 12-21-81 | 1040     | 13.5                     | 6.4                            | 1,120                                   | 808   | 24                                       | <.020  | 6.90  | <.060  | 1.1   | 8.0  |
| 06-23-82 | 1230     | 13.0                     | 7.0                            | 1,100                                   | 790   | 23                                       | <.020  | 8.40  | <.060  | 1.5   | 9.9  |
|          |          | Site 3846                | 121044618                      | 01; well S                              | C01506603CBD  | Stratmoor                                | Hills 7 (1   | at 38°46'12'  | ', long 104  | °46'18")  |  |
| 06-18-81 | 1045     | 13.0                     | 6.8                            | 1,500                                   | 1,140   | <b>7</b> 7                               | .000   | 4.80  | .690   | 1.3   | 6.1  |
| 06-23-82 | 1310     | 12.0                     | 6.9                            | 1,700                                   | 1,240   | 87                                       | <.020  | 6.10  | .280   | 1.4   | 7.5  |
|          | <u>s</u> | ite 38461                | 110445460                      | 1; well SC                              | 01506603DCA1  | Stratmoor                                | Hills 10 (   | lat 38°46'11  | l", long 10  | <u>4°45'46")</u>                                    |  |
| 06-18-81 | 1120     | 14.0                     | 7.2                            | 494                                     | 329   | 11                                       | .000   | 6.00  | <.060  | . 68  | 6.7  |
| 06-23-82 | 1030     | 14.0                     | 7.5                            |   | 337   | 12                                       | <.020  | 8.40  | <.060  | 1.6   | 10   |
|          |          | Site                     | 384538104                      | 450101; we                              | 11 SC0150661  | 1BCD1 Pine                               | llo 1 (lat   | 38°45'38", ]  | long 104°45  | <u>'01")</u>  |  |
| 11-24-81 | 1225     | 13.5                     | 6.5                            | 425                                     | 283   | 78                                       | .020   | 9.80  | . 160  | . 26  | 10   |
| 09-17-82 | 1300     | 13.5                     | 6.5                            | 405                                     | 352   | 11                                       | <.020  | 7.90  | .090   | 2.1   | 10   |

Table 11.0-2.--Ground-water quality data--Continued

| Date                 | Time | Temper-<br>ature<br>(°C) | pH<br>(stand-<br>ard<br>units) | Specific<br>conduct-<br>ance<br>(µS/cm) | Dissolved-<br>solids<br>residue<br>at 105°C<br>(mg/L) | Dissolved<br>chloride<br>(mg/L<br>as Cl) | Dissolved<br>nitrite<br>nitrogen<br>(mg/L<br>as N) | Dissolved<br>nitrogen<br>NO <sub>2</sub> +NO <sub>3</sub><br>(mg/L<br>as N) | Dissolved<br>ammonia<br>nitrogen<br>(mg/L<br>as N) | Dissolved nitrogen, ammonia and organic (mg/L as N) | Dis-<br>solved<br>nitroger<br>(mg/L<br>as N) |
|----------------------|------|--------------------------|--------------------------------|---|---|--|--|---|--|---|--|
|                      |      | Site                     | 384538104                      | 4451301; we                             | 11 SC0150661  | 11CBA3 Pine                              | ello 2 (lat  | 38°45'38",  | long 104°45  | '13")   |  |
| 06-22-81<br>06-21-82 |      | 13.5<br>13.0             | 6.7<br>7.3                     | 562<br>580                              | 402<br>370  | 22<br>16                                 | .000<br><.020                                      | 5.90<br>6.50  | <.060<br>.100                                      | 1.2<br>1.5  | 7.1<br>8.0                                   |
|                      |      | Site                     | 384534104                      | 4452101; we                             | 11 SC0150661  | 11BCC2 Pine                              | llo 5 (lat   | 38°45'34",  | long 104°45  | (21")   |  |
| 06-19-81<br>06-21-82 |      | 13.0<br>14.0             | 7.1<br>7.0                     | 680<br>560                              | 442<br>370  | 26<br>18                                 | .000<br><.020                                      | 5.00<br>5.00  | .110<br>.250                                       | 1.4<br>1.7  | 6.4<br>6.7                                   |
|                      |      | Site                     | 384538104                      | 4452201; we                             | 11 SC0150661  | 11BCC1 Pine                              | ello 6 (lat  | 38°45'38",  | long 104°45  | '22")   |  |
| 06-19-81<br>06-22-82 |      | 12.5<br>11.0             | 6.7<br>6.9                     | 720<br>640                              | 467<br>401  | 28<br>18                                 | 0.000<br><.020                                     | 5.20<br>6.70  | 0.340<br>.070                                      | 1.4<br>1.5  | 6.6<br>8.2                                   |
|                      |      | Site                     | 384548104                      | 4452801; we                             | 11 SC0150661  | OADD Pinel                               | lo 7 (lat 3  | 38°45'48", ]  | long 104°45'                                       | 23")  |  |
| 06-18-81<br>06-21-82 |      | 13.0<br>12.0             | 7.0<br>7.2                     | 630<br>570                              | 409<br>364  | 22<br>17                                 | .000<br><.020                                      | 6.20<br>6.90  | .060<br>.150                                       | .91<br>1.4  | 7.1<br>8.3                                   |
|                      |      | Site                     | 384554104                      | 4453601; we                             | 11 SC0150661  | OAAB Pinel                               | lo 8 (lat 3  | 38°45'54", 3  | long 104°45'                                       | 36")  |  |
| 06-18-81<br>06-21-82 |      | 13.5<br>13.0             | 7.0<br>7.2                     | 626<br>                                 | 396<br>341  | 18<br>14                                 | .000<br><.020                                      | 9.80<br>9.50  | <.060<br>.100                                      | 1.3<br>1.4  | 11<br>11                                     |
|                      |      | Site                     | 384543104                      | 4451801; we                             | 11 SC0150661  | 11BCB Pinel                              | lo 9 (lat 3  | 38°45'43", ]  | long 104°45'                                       | 18")  |  |
| 06-19-81<br>06-22-82 |      | 14.0<br>12.5             | 7.1<br>7.3                     | 525<br>500                              | 347<br>332  | 19<br>14                                 | .000<br><.020                                      | 7.70<br>7.80  | .060<br><.060                                      | 1.6<br>1.5  | 9.3<br>9.3                                   |
|                      |      | Site 3                   | 845581044                      | 53901; wel                              | 1 SC01506610  | AAB2 Pinel                               | lo 10 (lat   | 38°45'58",  | long 104°45  | '39")   |  |
| 06-19-81<br>06-21-82 |      | 14.0<br>12.5             | 6.8<br>7.1                     | 690<br>520                              | 460<br>347  | 23<br>13                                 | .010<br><.020                                      | 7.30<br>8.00  | .140<br><.060                                      | 1.5<br>1.3  | 8.8<br>9.3                                   |
|                      |      | Site                     | 384606104                      | 4455201; we                             | 11 SC0150660  | 3DCC Pinel                               | lo 11 (lat   | 38°46'06",  | long 104°45  | '52")   |  |
| 06-18-81<br>06-21-82 |      | 12.5<br>11.0             | 6.9<br>7.1                     | 805<br>650                              | 534<br>477  | 32<br>24                                 | .000<br><.020                                      | 4.40<br>4.20  | 1.20<br>.850                                       | 1.9<br>1.8  | 6.3<br>6.0                                   |
|                      |      | Site 3                   | 846081044                      | 454801; wel                             | 1 SC01506603  | BDCA2 Pinel                              | lo 12 (lat   | 38°46'08",  | long 104°45  | '48")   |  |
| 06-18-81<br>06-21-82 |      | 13.5<br>12.5             | 7.1<br>7.3                     | 650<br>440                              | 421<br>336  | 14<br>11                                 | .000<br><.020                                      | 11.0<br>8.10  | <.060<br>.060                                      | 1.5<br>.80  | 2.6<br>8.9                                   |
|                      |      | Site                     | 384559104                      | 4453201; we                             | 11 SC0150660  | 3DDD Pinel                               | lo 13 (lat   | 38°45'59",  | long 104°45  | '32")   |  |
| 06-19-81<br>06-21-82 |      | 13.5<br>12.0             | 7.1<br>7.5                     | 549<br>550                              | 344<br>355  | 16<br>18                                 | .000<br><.020                                      | 5.80<br>4.80  | .070<br>.120                                       | 1.5<br>1.4  | 7.3<br>6.2                                   |
|                      |      | Site 3                   | 845181044                      | 50501; wel                              | 1 SC01506611  | CDB Venetu                               | cci 1 (lat   | 38°45'18",  | long 104°45  | '05")   |  |
| 06-23-81<br>06-24-82 |      | 13.0<br>12.0             | 6.7<br>6.5                     | 714<br>760                              | 509<br>486  | 32<br>29                                 | .000<br><.020                                      | 4.80<br>3.20  | .070<br><.060                                      | 1.5<br>1.7  | 6.3<br>4.9                                   |

Table 11.0-2.--Ground-water quality data--Continued

| Date     | Time | Temper-<br>ature<br>(°C) | pH<br>(stand-<br>ard<br>units) | Specific<br>conduct-<br>ance<br>(µS/cm) | Dissolved-<br>solids<br>residue<br>at 105°C<br>(mg/L) | Dissolved<br>chloride<br>(mg/L<br>as Cl) | Dissolved<br>nitrite<br>nitrogen<br>(mg/L<br>as N) | Dissolved<br>nitrogen<br>NO <sub>2</sub> +NO <sub>3</sub><br>(mg/L<br>as N) | Dissolved<br>ammonia<br>nitrogen<br>(mg/L<br>as N) | Dissolved nitrogen, ammonia and organic (mg/L as N) | Dis-<br>solved<br>nitroger<br>(mg/L<br>as N) |
|----------|------|--------------------------|--------------------------------|---|---|--|--|---|--|---|--|
|          |      | Site 3                   | 8845221044                     | 50601; wel                              | 1 SC01506611  | ICAC Venetu                              | icci 2 (lat  | 38°45'22",  | long 104°45  | '06")   |  |
| 06-23-81 | 1350 | 13.5                     | 6.6                            | 716                                     | 529   | 33                                       | .000   | 5.40  | .070   | 1.2   | 6.6  |
| 06-24-82 | 1240 | 12.5                     | 6.8                            | 690                                     | 437   | 21                                       | <.020  | 4.50  | .060   | 1.4   | 5.9  |
|          |      | Site 3                   | 845351044                      | 50801; wel                              | 1 SC01506611  | IBCD2 Venet                              | ucci 3 (lat  | 38°45'35",  | long 104°4   | 5'08")  |  |
| 02-13-81 | 1115 | 13.0                     | 6.8                            | 460                                     | 294   | 13                                       | .000   | 9.10  | <.060  | 1.1   | 10   |
| 03-19-81 | 1130 | 13.0                     | 6.5                            | 422                                     | 275   | 13                                       | .000   | 8.30  | <.060  | .78   | 9.1  |
| 04-21-81 | 1045 | 13.5                     | 6.7                            | 417                                     | 292   | 12                                       | . 160  | 8.70  | . 160  | 1.2   | 9.9  |
| 05-19-81 | 1345 | 12.5                     | 6.3                            | 449                                     | 316   | 14                                       | .010   | 7.60  | .090   | 1.1   | 8.7  |
| 06-19-81 | 1535 | 14.0                     | 6.6                            | 430                                     | 282   | 11                                       | .000   | 8.20  | .070   | 1.6   | 9.8  |
| 07-17-81 | 1200 | 13.0                     | 6.5                            |   | 288   | 13                                       | .010   | 8.60  | .060   | .63   | 9.2  |
| 08-19-81 | 1135 | 13.5                     | 6.8                            | 420                                     | 281   | 11                                       | .030   | 7.90  | . 130  | 1.0   | 8.9  |
| 09-18-81 | 1125 | 13.0                     | 6.3                            | 407                                     | 287   | 11                                       | .020   | 6.80  | .130   | 1,2   | 8.0  |
| 10-26-81 | 1210 | 13.0                     | 6.5                            | 431                                     | 303   | 14                                       | <.020  | 7.80  | <.060  | 1.2   | 9.0  |
| 11-24-81 | 1250 | 13.5                     | 6.6                            | 425                                     | 270   | 12                                       | .020   | 9.80  | .080   |   |  |
|          | Sit  | e 3845351                | 04450801;                      | well SC01                               | 506611BCD2  | Venetucci 3                              | (lat 38°45   | '35", long  | 104°45'08")  | Continued   |  |
| 12-21-81 | 1125 | 13.5                     | 6.3                            | 444                                     | 271   | 11                                       | <0.020   | 6.70  | 0.090  | 0.87  | 7.6  |
| 01-20-82 | 0950 | 13.5                     | 6.4                            | 403                                     | 284   | 11                                       | <.020  | 8.40  | . 130  | . 79  | 9.2  |
| 02-24-82 | 1135 | 13.5                     | 6.3                            | 406                                     | 287   | 11                                       | <.020  | 8.40  | <.060  | .92   | 9.3  |
| 03-26-82 | 1050 | 14.0                     | 6.3                            | 460                                     | 313   | 13                                       | <.020  | 8.60  | <.060  | .57   | 9.2  |
| 04-30-82 | 1000 | 13.0                     | 6.5                            | 435                                     | 311   | 14                                       | <.020  | 8.40  | <.060  | 1.1   | 9.5  |
| 05-28-82 | 1130 | 13.0                     | 6.7                            | 415                                     | 286   | 10                                       | <.020  | 9.70  | .070   |   |  |
| 06-24-82 | 0950 | 13.5                     | 7.0                            | 420                                     | 293   | 10                                       | <.020  | 8.40  | <.060  | 1.1   | 9.5  |
| 10-22-82 | 1315 | 13.0                     |                                | 420                                     | 276   | 10                                       | <.020  | 8.20  | <.060  | 1.2   | 9.4  |
| 11-19-82 | 1145 | 13.5                     | 6.7                            | 469                                     | 319   | 14                                       | <.020  | 9.10  | <.060  | .90   | 10   |
| 12-17-82 | 1340 | 14.0                     | 6.6                            | 400                                     | 277   | 10                                       | <.020  | 9.00  | <.060  | . 70  | 9.7  |
|          |      | Site 3                   | 845171044                      | 45501; wel                              | 1 SC01506611  | CDA1 Venet                               | ucci 4 (lat  | . 38°45'17",  | long 104°4   | 4'55")  |  |
| 06-19-81 | 1330 | 15.5                     | 6.8                            | 770                                     | 502   | 32                                       | .000   | 7.50  | .090   | 1.4   | 8.9  |
|          |      | Site 3                   | 845321044                      | 50801; wel                              | 1 SC01506611  | CBA1 Venet                               | ucci 6 (lat  | . 38°45'32",  | long 104°4   | 5'08")  |  |
| 08-19-81 | 1220 | 13.5                     | 6.7                            | 715                                     | 468   | 30                                       | .030   | 6.30  | .140   | 1.0   | 7.3  |
| 06-24-82 | 1005 | 11.5                     | 6.9                            | 605                                     | 399   | 21                                       | <.020  | 8.80  | <.060  | 1.4   | 10   |
|          |      | Site 3                   | 845111044                      | 44301; wel                              | 1 SC01506611  | DCC Venetu                               | cci 7 (lat   | 38°45'11",  | long 104°44  | ' 43")  |  |
| 06-22-81 | 1000 | 14.5                     | 6.4                            | 743                                     | 530   | 33                                       | .000   | 5.10  | .060   | 1.5   | 6.6  |
|          |      | Site 3                   | 845151044                      | 44801; wel                              | 1 SC01506611  | DCB1 Venet                               | ucci 8 (lat  | 38°45'15",  | long 104°4   | 4'48")  |  |
| 06-19-81 | 1410 | 14.0                     | 7.0                            | 785                                     | 515   | 32                                       | .000   | 5.80  | .090   | 2.8   | 8.6  |
|          |      | Site 3                   | 845311044                      | 50301; wel                              | 1 SC01506611  | .CAB Venetu                              | cci 9 (lat   | 38°45'31",  | long 104°45  | '03")   |  |
| 06-19-81 | 1455 | 14.5                     | 6.6                            | 630                                     | 420   | 26                                       | .000   | 9.10  | .080   | 1.5   | 11   |
| 06-24-82 | 1105 | 14.0                     | 6.9                            | 479                                     | 316   | 13                                       | <.020  | 8.10  | <.060  | 1.8   | 9.9  |

Table 11.0-2.--Ground-water quality data--Continued

| Date                 | Time  | Temper-<br>ature<br>(°C) | pH<br>(stand-<br>ard<br>units) | Specific<br>conduct-<br>ance<br>(µS/cm) | Dissolved-<br>solids<br>residue<br>at 105°C<br>(mg/L) | Dissolved<br>chloride<br>(mg/L<br>as Cl) | Dissolved<br>nitrite<br>nitrogen<br>(mg/L<br>as N) | Dissolved<br>nitrogen<br>NO <sub>2</sub> +NO <sub>3</sub><br>(mg/L<br>as N) | Dissolved<br>ammonia<br>nitrogen<br>(mg/L<br>as N) | Dissolved nitrogen, ammonia and organic (mg/L as N) | Dis-<br>solved<br>nitrogen<br>(mg/L<br>as N) |
|----------------------|-------|--------------------------|--------------------------------|---|---|--|--|---|--|---|--|
|                      |       | Site                     | 384458104                      | 442601; we                              | 11 SC0150661  | 14AAD Secur                              | ity 2 (lat   | 38°44'58",  | long 104°44  | '26")   |  |
| 02-13-81             | 1025  | 13.0                     | 6.8                            | 650                                     | 407   | 24                                       | .000   | 7.00  | <.060  | .82   | 7.8  |
| 03-19-81             | 1330  | 13.0                     | 6.3                            |   | 401   | 26                                       | .000   | 4.80  | <.060  | . 72  | 5.5  |
| 05-21-81             | 1500  | 14.0                     | 6.6                            | 642                                     | 440   | 19                                       | .000   | 7.00  | . 100  | 2.2   | 9.2  |
| 06-22-81             | 1105  | 14.5                     | 6.2                            |   | 400   | 22                                       | .000   | 7.10  | <.060  | 1.6   | 8.7  |
| 07-17-81             | 0955  | 13.0                     | 6.4                            |   | 362   | 20                                       | .000   | 8.00  | .080   | 1.0   | 9.0  |
| 11-24-81             | 1050  | 13.0                     | 6.5                            | 635                                     | 428   | 22                                       | .020   | 7.70  | . 160  | .42   | 8.1  |
| 12-21-81             | 0950  | 13.5                     | 6.2                            | 668                                     | 416   | 20                                       | <.020  | 4.90  | .080   | 1.0   | 5.9  |
| 01-20-82             | 1020  | 13.5                     | 6.2                            | 661                                     | 445   | 27                                       | <.020  | 6.10  | .120   | 1.0   | 7.1  |
| 02-24-82             | 0920  | 13.0                     | 6.5                            | 647                                     | 438   | 23                                       | <.020  | 6.40  | <.060  | 1.0   | 7.4  |
| 03-26-82             | 0945  | 13.5                     | 6.3                            | 646                                     | 427   | 29                                       | <.020  | 6.00  | .060   | . 37  | 6.4  |
| 04-30-82             | 1020  | 13.5                     | 6.4                            | 638                                     | 439   | 26                                       | <.020  | 5.80  | .070   | 1.0   | 6.8  |
| 05-28-82             | 1040  | 13.5                     | 6.3                            | 648                                     | 436   | 26                                       | <.020  | 6.50  | .070   | 1.1   | 7.6  |
| 06-22-82             | 1025  | 14.0                     | 6.7                            | 663                                     | 446   | 24                                       | <.020  | 5.70  | .080   | 1.4   | 7.1  |
| 07-16-82             | 0950  | 13.0                     | 6.5                            | 638                                     | 447   | 28                                       | <.020  | 6.30  | <.060  | 1.4   | 7.7  |
| 09-17-82             | 1010  | 13.0                     | 6.3                            | 653                                     | 513   | 28                                       | <.020  | 6.00  | .070   | 2.1   | 8.1  |
| 10-22-82             | 1050  | 13.0                     |                                | 660                                     | 446   | 29                                       | <.020  | 5.80  | <.060  | 2.1   | 7.9  |
| 11-19-82             | 1115  | 13.5                     | 6.5                            | 670                                     | 443   | 29                                       | <.020  | 5.70  | <.060  | . 70  | 6.4  |
| 12-17-82             | 1045  | 13.5                     | 6.5                            | 633                                     | 429   | 28                                       | <.020  | 5.70  | <.060  | 1.2   | 6.9  |
|                      |       | Site                     | 384524104                      | 445101; we                              | 11 SC0150661  | 1CAD Secur                               | ity 4 (lat   | 38°45'24",  | long 104°44  | <u>'51")</u>  |  |
| 06-22-81             | 1320  | 14.5                     | 6.6                            | 455                                     | 329   | 17                                       | .000   | 7.90  | .060   | 1.4   | 9.3  |
| 06-22-82             | 1330  | 14.0                     | 6.8                            | 491                                     | 322   | 14                                       | <.020  | 8.10  | .080   | 1.4   | 9.5  |
|                      |       | Site                     | 384527104                      | 445601; we                              | 11 SC0150 <b>661</b>                                  | 1CAA Secur                               | ity 7 (lat   | 38°45'27",  | long 104°44  | <u>'56")</u>  |  |
| 06-22-81             | 1350  | 14.5                     | 6.5                            | 490                                     | 354   | 19                                       | 0.000  | 8.10  | <0.060   | 1.6   | 9.7  |
| 06-22-82             |       | 14.0                     | 6.9                            | 470                                     | 322   | 11                                       | <.020  | 8.40  | <.060  | 1.7   | 10   |
|                      |       | Site 3                   | 8845211044                     | 44301; wel                              | 1 'SC01506611   | DCB2 Secur                               | ity 8 (lat   | 38°45'21",  | long 104°44  | '43")   |  |
| 06-22 01             | .,,,, | 1/ 5                     |                                | 507                                     |   | 2/                                       | 200  | ( (0  | . 060  | 1.0   | 0 5  |
| 06-22-81<br>06-22-82 |       | 14.5<br>14.0             | 6.5<br>6.7                     | 597<br>630                              | 424<br>416  | 24<br>21                                 | .000<br><.020                                      | 6.60<br>7.50  | <.060<br><.060                                     | 1.9<br>1.5  | 8.5<br>9.0                                   |
| 00-22-62             | 1313  | 14.0                     | 0.7                            | 630                                     | 410   | 21                                       | 1.020  | 7.30  | 1.000  | 1.5   | 9.0  |
|                      |       | Site                     | 384422104                      | 435201; we                              | 11 SC0150661  | 3CDA Secur                               | ity 9 (lat   | 38°44'22",  | long 104°43  | '52")   |  |
| 06-22-81             | 1550  | 14.0                     | 6.6                            | 627                                     | 447   | 27                                       | .000   | 8.10  | .060   | 1.7   | 9.8  |
| 06-21-82             | 1445  | 14.0                     | 6.9                            | 640                                     | 428   | 38                                       | <.020  | 7.10  | .070   | 1.5   | 8.6  |
|                      |       | Site 3                   | 844161044                      | 34701; wel                              | 1 SC01506613  | CDD Securi                               | ty 10 (lat   | 38°44'16",  | long 104°43  | <u>'47")</u>  |  |
| 06-22-81             | 1525  | 14.5                     | 6.7                            | 740                                     | 532   | 29                                       | .000   | 6.90  | <.060  | 1.4   | 8.3  |
| 06-21-82             |       | 14.5                     | 6.6                            | 765                                     | 512   | 28                                       | <.020  | 8.60  | .070   | 1.1   | 9.7  |
|                      |       |                          |                                |   |   |  |  |   |  |   |  |

Table 11.0-2.--Ground-water quality data--Continued

| Site 384553104451801; well SC01506611BBB2   Security 11 (lat 38*45*53", long 104*45*18")   O6-22-81 1430  | Date     | Time | Temper-<br>ature<br>(°C) | pH<br>(stand-<br>ard<br>units) | Specific<br>conduct-<br>ance<br>(µS/cm) | Dissolved-<br>solids<br>residue<br>at 105°C<br>(mg/L) | Dissolved<br>chloride<br>(mg/L<br>as Cl) | Dissolved<br>nitrite<br>nitrogen<br>(mg/L<br>as N) | Dissolved<br>nitrogen<br>NO <sub>2</sub> +NO <sub>3</sub><br>(mg/L<br>as N) | Dissolved<br>ammonia<br>nitrogen<br>(mg/L<br>as N) | Dissolved nitrogen, ammonia and organic (mg/L as N) | Dis-<br>solved<br>nitroger<br>(mg/L<br>as N) |
|---|----------|------|--------------------------|--------------------------------|---|---|--|--|---|--|---|--|
| 04-14-82 0930 6.9 441 6.60 110 04-14-82 0930 6.9 435 6.60 0.000 04-14-82 0937 6.6 423 7.30 060 04-14-82 0947 6.6 417 7.30 060 04-14-82 1017 6.6 417 7.60 060 04-14-82 1017 6.6 417 7.60 060 04-14-82 1017 6.6 417 7.70 060 04-14-82 1127 14.5 6.7 411 7.70 060 04-14-82 127 15.5 6.7 411 7.50 060 04-14-82 127 15.5 6.7 411 7.50 060 04-14-82 127 15.5 6.7 411 7.50 060 04-14-82 127 15.5 6.7 411 7.50 060 04-14-82 127 15.5 6.7 416 7.50 060 04-14-82 127 15.0 6.6 414 7.50 060 04-14-82 127 15.0 6.6 514 4 7.50 060 04-14-82 127 15.0 6.6 514 4 7.50 060 04-14-82 127 15.0 6.6 514 4 7.50 060 04-14-82 127 15.0 6.6 514 4 7.50 060 04-14-82 127 15.0 6.6 514 4 7.50 060 04-14-82 127 15.0 6.6 514 4 7.50 060 04-14-82 127 15.0 6.6 514 4 7.50 060 04-14-82 127 15.0 6.6 514 4 7.50 060 04-14-82 127 15.0 6.6 514 4 1.0 6.6 514 4 1.0 6.6 5.0 514 4.0 6.9 530 349 15   |          |      | Site 3                   | 845531044                      | 51801; wel                              | 1 SC01506611  | BBB2 Secur                               | ity ll (lat  | . 38°45'53",  | long 104°4   | 5'18")  |  |
| 04-14-82 0930 6.9 441   | 06-22-01 | 1/20 | 1/. 0                    | 4 0                            | 404                                     | 202   | 12                                       | 000  | 7 70  | < 060  | 1.6   | 9.3  |
| 04-14-82 0932 6.9 435 6.80 .080 04-14-82 0932 6.3 431 7.00 .060 04-14-82 0937 6.6 423 7.30 .060 04-14-82 0937 6.6 423 7.30 .060 04-14-82 1017 6.6 417 7.00 .060 04-14-82 1017 6.6 417 7.70 .060 04-14-82 1127 14.5 6.7 417 7.50 .060 04-14-82 1527 14.5 6.7 411 7.50 .060 04-14-82 1527 14.5 6.7 411 7.50 .060 04-14-82 1527 14.5 6.7 411 7.50 .060 04-14-82 1217 15.0 6.6 414 7.70 .060 050  |          |      |                          |                                |   |   |  |  |   |  |   | 9.3<br>                                      |
| 04-14-82 0937 6.6 423 7.00 .060 04-14-82 0947 6.6 423 7.7.00 .060 04-14-82 0947 6.6 417 7.7.00 .060 04-14-82 1017 6.6 417 7.7.00 .060 04-14-82 1017 6.6 417 7.7.00 .060 04-14-82 1127 14.5 6.7 411 7.7.00 .060 04-14-82 1227 15.0 6.6 414 7.7.0 .060 04-14-82 1227 15.0 6.6 414 7.7.0 .060 04-14-82 1227 15.0 6.6 414 7.7.0 .060 04-14-82 1227 15.0 6.6 414 7.7.0 .060 04-14-82 1227 15.0 6.6 414 7.7.0 .060 04-14-82 1227 15.0 6.6 414 7.7.0 .060 04-14-82 1227 15.0 6.6 414 7.7.0 .060 04-14-82 1227 15.0 6.6 414 7.7.0 .060 04-14-82 1227 15.0 6.6 414 7.7.0 .060 04-14-82 1227 15.0 6.6 414 7.7.0 .060 05-06-02-82 1410 14.0 6.9 530 349 15 <- 0.02 5.00 5.00 .060 05-06-02-82 1415 14.0 6.9 530 349 15 <- 0.02 5.00 5.00 .060 1.1 06-02-82 1435 14.0 6.9 535 346 16 <- 0.02 5.50 .060 1.4 08-13-82 1020 13.0 6.5 501 435 19 <- 0.02 5.00 5.00 .100 1.3 06-02-82 1435 14.0 6.9 535 346 16 <- 0.02 5.50 .060 1.4 08-13-82 1020 13.0 6.5 501 435 19 <- 0.02 5.00 5.00 .100 1.3 06-02-82 1435 13.0 6.7 485 306 13 .000 4.70 <- 0.60 .59 04-21-81 0930 13.5 7.1 488 336 17 .060 5.70 .100 1.3 06-19-81 1320 12.5 6.7 485 306 13 .000 4.70 <- 0.60 .59 04-21-81 0930 13.5 7.1 488 336 17 .060 5.70 .120 1.1 06-06-23-81 1030 14.0 7.2 324 22 .000 5.00 5.00 .060 1.4 06-06-19-19-81 1230 12.5 6.7 480 324 13 .010 6.10 .120 1.6 06-23-81 1030 14.0 7.2 322 15 .000 6.80 .70 .000 1.4 07 .75 09-18-81 1030 14.0 7.2 322 15 .000 6.80 .70 .000 1.2 1.5 09-18-81 1030 14.0 7.2 322 15 .000 6.80 .70 .000 1.2 1.5 09-18-81 1030 14.0 0.5 6.8 498 330 14 .000 4.70 .70 .70 .75 09-18-81 1030 14.0 6.8 498 330 14 .000 7.0 .000 1.2 1.5 09-18-81 1030 14.0 6.8 498 330 14 .000 7.0 0.00 1.2 1.5 09-18-81 1005 13.5 6.8 511 336 15 .000 6.00 6.00 6.00 0.00 0.00 0.00 0.0   | _        |      |                          |                                |   |   |  |  |   |  |   |  |
| 04-14-82 0937 6.6 423 7.30 .060 04-14-82 1017 6.6 417 7.50 .060 .070 04-14-82 1127 14.5 6.7 417 7.50 .060 04-14-82 1127 14.5 6.7 417 7.50 .060 04-14-82 127 15.0 6.6 414 7.50 .060 04-14-82 127 15.0 6.6 414 7.70 .060 04-14-82 127 15.0 6.6 414 7.70 .060 04-14-82 127 15.0 6.6 414 7.70 .060 04-15-82 1027 13.5 6.7 416 7.70 .060 04-15-82 1010 14.0 6.9 530 349 15 .020 5.60 .250 2.1  |          |      |                          |                                |   |   |  |  |   |  |   |  |
| 04-14-82 1017  6.6 417  7.70 0.60  04-14-82 1527 14.5 6.7 417  7.70 0.60 0 04-14-82 1527 14.5 6.7 417  7.70 0.60 0 04-14-82 1527 14.5 6.7 411   7.70 0.60  04-14-82 1527 15.0 6.6 414   7.70 0.60  04-15-82 0.927 13.5 6.7 416     7.70 0.60  06-22-82 1410 14.0 6.9 530 349 15   |          |      |                          |                                |   |   |  |  |   |  |   |  |
| 04-14-82 1017  6.6 417  7.70 0.60  04-14-82 1527 14.5 6.7 417  7.70 0.60 0 04-14-82 1527 14.5 6.7 417  7.70 0.60 0 04-14-82 1527 14.5 6.7 411   7.70 0.60  04-14-82 1527 15.0 6.6 414   7.70 0.60  04-15-82 0.927 13.5 6.7 416     7.70 0.60  06-22-82 1410 14.0 6.9 530 349 15   | 04-14-82 | 0947 |                          | 6.6                            | 417                                     |   |  |  | 7.60  | . 070  |   |  |
| 04-14-82 1127 14.5 6.7 417 7.60 .060 04-14-82 1527 14.5 6.7 411 7.50 .060 04-14-82 2127 15.0 6.6 414 7.50 .060 04-15-82 2127 15.0 6.6 414 7.770 .060 04-15-82 2127 13.5 6.7 416 7.770 .060 06-22-82 1410 14.0 6.9 530 349 15 <0.000 .060 0.060 .250 .21   |          | _    |                          |                                |   |   |  |  |   |  |   |  |
| 04-14-82 1527 14.5 6.7 411 7.50 .060 04-14-82 127 15.0 6.6 414 7.70 .060 04-15-82 0927 13.5 6.7 416 7.70 .060 06-22-82 1410 14.0 6.9 530 349 15 <0.020 5.60 .250 2.1     Site 384606104453101; well SC01506603DDA   Security 13 (lat 38*46*06", long 104*45*31")  |          |      | 14.5                     |                                |   |   |  |  |   |  |   |  |
| 04-15-82 0927 13.5 6.7 416 8.00 .060 8.00 .250 2.1    Comparison of the | 04-14-82 | 1527 |                          |                                |   |   |  |  |   |  |   |  |
|   | 04-14-82 | 2127 |                          |                                | 414                                     |   |  |  |   | .060   |   |  |
|   | 04-15-82 | 0927 | 13.5                     | 6.7                            | 416                                     |   |  |  | 8 00  | 060  |   |  |
| Site 384606104453101;   well SC01506603DDA   Security 13 (lat 38°46'06", long 104°45'31")   |          |      |                          |                                |   |   |  |  |   |  |   | 7.7  |
| 06-23-81 1055 14.0 6.7 513 351 21 .000 4.70 .060 1.1 06-22-82 1435 14.0 6.9 535 346 16 <.020 5.50 .060 1.4 08-13-82 1020 13.0 6.5 501 435 19 <.020 5.20 .100 1.3  **Site 384610104453501; well SC01506603DDB** Security 14 (lat 38°46'10", long 104°45'35")**  02-13-81 1100 13.0 7.3 500 326 12 .000 5.00 <.060 .97 03-19-81 1355 13.0 6.7 485 306 13 .000 4.70 <.060 .59 04-21-81 0930 13.5 7.1 488 336 17 .060 5.70 .120 1.1 05-19-81 1220 12.5 6.7 480 324 13 .010 6.10 .120 1.6 06-23-81 1030 14.0 7.2 324 22 .000 5.30 .060 1.4 07-17-81 1025 13.0 6.8 322 15 .000 6.80 .060 .64 08-19-81 1005 12.5 6.9 500 317 14 .030 4.70 .070 .75 09-18-81 0945 12.5 6.8 468 323 23 .030 4.20 .120 1.5 10-26-81 1105 12.5 6.8 468 325 11 <.020 5.50 <.060 1.2 11-24-81 1120 13.0 6.8 498 330 14 .020 7.40 .160 .72 11-24-81 1120 13.0 6.8 498 330 14 .020 7.40 .160 .72 12-21-81 1005 13.5 6.6 504 336 17 <.020 6.40 .150 .12 11-24-81 1120 13.5 6.6 511 336 15 <.020 6.40 .150 .41 07-22-82 1050 13.5 6.6 511 336 15 <.020 6.40 .150 .070 .76 04-30-82 1045 13.5 6.8 511 340 16 <.020 3.30 .060 2.1 06-22-82 1051 13.5 6.6 511 340 16 <.020 5.90 <.060 2.1 06-22-82 1050 13.5 6.6 511 340 16 <.020 5.90 <.060 2.1 06-22-82 1050 13.5 6.8 511 340 16 <.020 5.90 <.060 2.1 06-22-82 1050 13.5 6.8 511 340 16 <.020 5.90 <.060 2.1 06-22-82 1050 13.5 6.8 511 340 16 <.020 5.90 <.060 2.1 07-16-82 1020 13.0 6.8 511 340 16 <.020 5.90 <.060 2.1 07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 2.1 07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 2.1 07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 1.4 09-17-82 1030 12.5 6.8 496 403 16 <.020 5.40 .100 1.2 11-19-82 1030 12.5 6.8 496 403 16 <.020 5.40 .100 1.2 11-19-82 1030 12.5 6.8 496 403 16 <.020 5.40 .100 1.2 11-19-82 1030 13.5 6.9 525 349 19 <.020 7.00 <.060 1.1  | 00 22 02 | 1410 | 14.0                     | 0.,                            | 330                                     | 347   |  | 1.020  | 3.00  | .230   |   | , , ,  |
| 06-22-82 1435 14.0 6.9 535 346 16   |          |      | Site 3                   | 846061044                      | 53101; wel                              | 1 SC01506603  | DDA Securi                               | ty 13 (lat   | 38°46'06",  | long 104°45  | '31")   |  |
| 06-22-82 1435 14.0 6.9 535 346 16   | 06-23-81 | 1055 | 14.0                     | 6.7                            | 513                                     | 351   | 21                                       | .000   | 4.70  | .060   | 1.1   | 5.8  |
| 08-13-82 1020 13.0 6.5 501 435 19 <0.020 5.20 .100 1.3    Site 384610104453501; well SC01506603DDB   Security 14 (lat 38°46'10", long 104°45'35")   |          |      |                          |                                |   |   |  |  |   |  |   | 6.9  |
| 02-13-81 1100 13.0 7.3 500 326 12000 5.00 <.06097 03-19-81 1355 13.0 6.7 485 306 13000 4.70 <.06059 04-21-81 0930 13.5 7.1 488 336 17   | 08-13-82 | 1020 | 13.0                     | 6.5                            |   | 435   | 19                                       | <.020  | 5.20  | .100   | 1.3   | 6.5  |
| 03-19-81 1355 13.0 6.7 485 306 13 .000 4.70 <.060 .59 04-21-81 0930 13.5 7.1 488 336 17 .060 5.70 .120 1.1 06-23-81 1030 12.5 6.7 480 324 13 .010 6.10 .120 1.6 06-23-81 1030 14.0 7.2 324 22 .000 5.30 .060 1.4  07-17-81 1025 13.0 6.8 322 15 .000 6.80 .060 .64 08-19-81 1005 12.5 6.9 500 317 14 .030 4.70 .070 .75 09-18-81 0945 12.5 6.8 468 323 23 .030 4.20 .120 1.5 10-26-81 1105 12.5 6.8 486 325 11 <.020 5.50 <.060 1.2 11-24-81 1120 13.0 6.8 498 330 14 .020 7.40 .160 .72  12-21-81 1005 13.5 6.6 504 336 17 <.020 6.40 .150 .41 01-20-82 1050 13.5 6.6 511 336 15 <.020 6.40 .150 .41 02-24-82 0950 13.5 6.6 511 336 15 <.020 6.40 .150 .40 03-26-82 1045 13.5 6.8 512 348 17 <.020 6.40 .060 2.0 03-26-82 1045 13.5 6.8 512 348 17 <.020 6.40 .070 .95 05-28-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 .70  Site 384610104453501; well SC01506603DDB Security 14 (lat 38°46'10", long 104°45'35")Continued  06-22-82 1450 13.5 6.8 496 403 16 <.020 5.90 <0.060 2.1 07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 1.4 09-17-82 1030 12.5 6.8 496 403 16 <.020 5.40 <.060 1.4 09-17-82 1030 12.5 6.8 496 403 16 <.020 5.40 <.060 1.4 11-19-82 1120 13.5 6.9 525 349 19 <.020 6.40 <.060 1.1   |          |      |                          |                                |   |   |  |  |   |  |   |  |
| 04-21-81 0930 13.5 7.1 488 336 17 .060 5.70 .120 1.1 05-19-81 1230 12.5 6.7 480 324 13 .010 6.10 .120 1.6 06-23-81 1030 14.0 7.2 324 22 .000 5.30 .060 1.4  07-17-81 1025 13.0 6.8 322 15 .000 6.80 .060 .64 08-19-81 1005 12.5 6.9 500 317 14 .030 4.70 .070 .75 09-18-81 0945 12.5 6.8 468 323 23 .030 4.20 .120 1.5 10-26-81 1105 12.5 6.8 486 325 11 <.020 5.50 <.060 1.2 11-24-81 1120 13.0 6.8 498 330 14 .020 7.40 .160 .72 12-21-81 1005 13.0 6.5 530 324 10 <.020 4.70 .070 .72 12-21-81 1005 13.5 6.6 504 336 17 <.020 4.70 .070 1.1 01-20-82 1050 13.5 6.6 504 336 17 <.020 6.40 .150 .41 02-24-82 0950 13.5 6.6 511 336 15 <.020 6.40 <.060 2.0 03-26-82 1015 13.5 6.8 512 348 17 <.020 6.10 .070 .95 05-28-82 1020 13.0 6.8 511 340 16 <.020 5.90 <0.060 2.0  03-26-82 1045 13.5 6.8 512 348 17 <.020 6.10 .070 .95 05-28-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 2.1 07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 1.4 09-17-82 1030 12.5 6.8 496 403 16 <.020 5.90 <0.060 2.1 07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 1.4 09-17-82 1030 12.5 6.8 496 403 16 <.020 5.90 <0.060 2.1 07-16-82 1010 13.0 6.9 493 350 17 <.020 6.40 <.060 1.4 09-17-82 1030 12.5 6.8 496 403 16 <.020 5.90 <0.060 2.1 07-16-82 1110 13.0 530 336 17 <.020 6.40 <.060 1.1 11-19-82 1120 13.5 6.9 525 349 19 <.020 7.00 <0.060 .60   |          |      |                          |                                |   |   |  |  |   |  |   | 6.0  |
| 05-19-81 1230 12.5 6.7 480 324 13 .010 6.10 .120 1.6 06-23-81 1030 14.0 7.2 324 22 .000 5.30 .060 1.4  07-17-81 1025 13.0 6.8 322 15 .000 6.80 .060 .64 08-19-81 1005 12.5 6.9 500 317 14 .030 4.70 .070 .75 09-18-81 0945 12.5 6.8 468 323 23 .030 4.20 .120 1.5 10-26-81 1105 12.5 6.8 486 325 11 .020 5.50 .060 1.2 11-24-81 1120 13.0 6.8 498 330 14 .020 7.40 .160 .72  12-21-81 1005 13.0 6.5 530 324 10 .020 7.40 .160 .72  12-21-81 1005 13.5 6.6 504 336 17 .020 6.40 .150 .41 02-24-82 0950 13.5 6.7 503 338 15 .020 6.40 .150 .41 02-24-82 1015 13.5 6.6 511 336 15 .020 6.40 .060 2.0 03-26-82 1015 13.5 6.8 512 348 17 .020 6.10 .070 .95 04-30-82 1045 13.5 6.8 512 348 17 .020 6.10 .070 .95 05-28-82 1020 13.0 6.8 511 340 16 .020 3.30 .060  Site 384610104453501; well SC01506603DDB Security 14 (lat 38°46'10", long 104°45'35")Continued  06-22-82 1450 13.5 6.8 496 403 16 .020 5.40 .060 1.4 09-17-82 1030 12.5 6.8 496 403 16 .020 5.40 .000 1.2 10-22-82 1110 13.0 530 336 17 .020 6.40 .060 1.4 10-22-82 1110 13.0 530 336 17 .020 6.40 .060 1.1 11-19-82 1120 13.5 6.9 525 349 19 .020 7.00 .060 .60  |          |      |                          |                                |   |   |  |  |   |  |   | 5.3  |
| 06-23-81 1030 14.0 7.2 324 22 .000 5.30 .060 1.4  07-17-81 1025 13.0 6.8 322 15 .000 6.80 .060 .64  08-19-81 1005 12.5 6.9 500 317 14 .030 4.70 .070 .75  09-18-81 0945 12.5 6.8 468 323 23 .030 4.20 .120 1.5  10-26-81 1105 12.5 6.8 486 325 11 <.020 5.50 <.060 1.2  11-24-81 1120 13.0 6.8 498 330 14 .020 7.40 .160 .72  12-21-81 1005 13.0 6.5 530 324 10 <.020 4.70 .070 1.1  01-20-82 1050 13.5 6.6 504 336 17 <.020 6.40 .150 .41  02-24-82 0950 13.5 6.7 503 338 15 <.020 6.40 <.060 2.0  03-26-82 1015 13.5 6.6 511 336 15 <.020 6.40 <.060 2.0  03-26-82 1015 13.5 6.8 512 348 17 <.020 6.10 .070 .95  05-28-82 1020 13.0 6.8 511 340 16 <.020 3.30 .060  Site 384610104453501; well SC01506603DDB Security 14 (lat 38°46'10", long 104°45'35")Continued  06-22-82 1450 13.5 6.9 493 350 17 <.020 6.40 <.060 2.1  07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 1.4  09-17-82 1030 12.5 6.8 496 403 16 <.020 5.90 <0.060 2.1  07-16-82 1030 12.5 6.8 496 403 16 <.020 5.40 <.060 1.4  10-22-82 1110 13.0 530 336 17 <.020 6.40 <.060 1.1  11-9-82 1120 13.5 6.9 525 349 19 <.020 7.00 <.060 .60  |          |      |                          |                                |   |   |  |  |   |  |   | 6.8  |
| 07-17-81 1025 13.0 6.8 322 15 .000 6.80 .060 .64 08-19-81 1005 12.5 6.9 500 317 14 .030 4.70 .070 .75 09-18-81 0945 12.5 6.8 468 323 23 .030 4.20 .120 1.5 10-26-81 1105 12.5 6.8 486 325 11 <.020 5.50 <.060 1.2 11-24-81 1120 13.0 6.8 498 330 14 .020 7.40 .160 .72 12-21-81 1005 13.0 6.5 530 324 10 <.020 4.70 .070 1.1 01-20-82 1050 13.5 6.6 504 336 17 <.020 6.40 .150 .41 02-24-82 0950 13.5 6.6 511 336 15 <.020 6.40 <.060 2.0 03-26-82 1015 13.5 6.6 511 336 15 <.020 5.10 .100 .76 04-30-82 1045 13.5 6.8 512 348 17 <.020 6.10 .070 .95 05-28-82 1020 13.0 6.8 511 340 16 <.020 3.30 .060   Site 384610104453501; well SC01506603DDB Security 14 (lat 38°46'10", long 104°45'35")Continued  06-22-82 1450 13.5 6.8 496 403 16 <.020 5.40 <.060 2.1 07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 1.4 09-17-82 1030 12.5 6.8 496 403 16 <.020 5.40 <.060 1.4 10-22-82 1110 13.0 530 336 17 <.020 6.40 <.060 1.2 11-19-82 1120 13.5 6.9 525 349 19 <.020 7.00 <.060 .60  |          |      |                          |                                |   |   |  |  |   |  |   | 7.7  |
| 08-19-81 1005 12.5 6.9 500 317 14 .030 4.70 .070 .75 09-18-81 0945 12.5 6.8 468 323 23 .030 4.20 .120 1.5 10-26-81 1105 12.5 6.8 486 325 11   | 06-23-81 | 1030 | 14.0                     |                                |   | 324   |  | .000   |   |  |   | 6.7  |
| 09-18-81 0945 12.5 6.8 468 323 23 .030 4.20 .120 1.5 10-26-81 1105 12.5 6.8 486 325 11 <.020 5.50 <.060 1.2 11-24-81 1120 13.0 6.8 498 330 14 .020 7.40 .160 .72  12-21-81 1005 13.0 6.5 530 324 10 <.020 4.70 .070 1.1 01-20-82 1050 13.5 6.6 504 336 17 <.020 6.40 .150 .41 02-24-82 0950 13.5 6.7 503 338 15 <.020 6.40 <.060 2.0 03-26-82 1015 13.5 6.6 511 336 15 <.020 6.40 <.060 2.0 03-26-82 1015 13.5 6.8 512 348 17 <.020 6.10 .070 .95 05-28-82 1020 13.0 6.8 511 340 16 <.020 3.30 .060  Site 384610104453501; well SC01506603DDB Security 14 (lat 38°46'10", long 104°45'35")Continued  06-22-82 1450 13.5 7.2 540 349 14 <0.020 5.90 <0.060 2.1 07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 1.4 09-17-82 1030 12.5 6.8 496 403 16 <.020 5.40 <.060 1.4 09-17-82 1030 12.5 6.8 496 403 16 <.020 5.40 .100 1.2 11-19-82 1120 13.5 6.9 525 349 19 <.020 7.00 <.060 .60  |          |      |                          |                                |   |   |  |  |   |  |   | 7.4  |
| 10-26-81 1105 12.5 6.8 486 325 11 <.020 5.50 <.060 1.2   11-24-81 1120 13.0 6.8 498 330 14 .020 7.40 .160 .72    12-21-81 1005 13.0 6.5 530 324 10 <.020 4.70 .070 1.1   01-20-82 1050 13.5 6.6 504 336 17 <.020 6.40 .150 .41   02-24-82 0950 13.5 6.7 503 338 15 <.020 6.40 <.060 2.0   03-26-82 1015 13.5 6.6 511 336 15 <.020 5.10 .100 .76   04-30-82 1045 13.5 6.8 512 348 17 <.020 6.10 .070 .95   05-28-82 1020 13.0 6.8 511 340 16 <.020 3.30 .060    Site 384610104453501; well SC01506603DDB Security 14 (lat 38°46'10", long 104°45'35")Continued    06-22-82 1450 13.5 6.8 496 403 16 <.020 5.90 <0.060 2.1   07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 1.4   09-17-82 1030 12.5 6.8 496 403 16 <.020 5.40 .100 1.2   10-22-82 1110 13.0 530 336 17 <.020 6.40 <.060 1.1   11-19-82 1120 13.5 6.9 525 349 19 <.020 7.00 <.060 .60   |          |      |                          |                                |   |   |  |  |   |  |   | 5.5  |
| 11-24-81 1120 13.0 6.8 498 330 14 .020 7.40 .160 .72  12-21-81 1005 13.0 6.5 530 324 10 <.020 4.70 .070 1.1  01-20-82 1050 13.5 6.6 504 336 17 <.020 6.40 .150 .41  02-24-82 0950 13.5 6.7 503 338 15 <.020 6.40 <.060 2.0  03-26-82 1015 13.5 6.6 511 336 15 <.020 5.10 .100 .76  04-30-82 1045 13.5 6.8 512 348 17 <.020 6.10 .070 .95  05-28-82 1020 13.0 6.8 511 340 16 <.020 3.30 .060  Site 384610104453501; well SC01506603DDB Security 14 (lat 38°46'10", long 104°45'35")Continued  06-22-82 1450 13.5 7.2 540 349 14 <0.020 5.90 <0.060 2.1  07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 1.4  09-17-82 1030 12.5 6.8 496 403 16 <.020 5.40 .100 1.2  10-22-82 1110 13.0 530 336 17 <.020 6.40 <.060 1.1  11-19-82 1120 13.5 6.9 525 349 19 <.020 7.00 <.060 .60  |          |      |                          |                                |   |   |  |  |   |  |   | 5.7  |
| 12-21-81 1005 13.0 6.5 530 324 10 <.020 4.70 .070 1.1 01-20-82 1050 13.5 6.6 504 336 17 <.020 6.40 .150 .41 02-24-82 0950 13.5 6.7 503 338 15 <.020 6.40 <.060 2.0 03-26-82 1015 13.5 6.6 511 336 15 <.020 5.10 .100 .76 04-30-82 1045 13.5 6.8 512 348 17 <.020 6.10 .070 .95 05-28-82 1020 13.0 6.8 511 340 16 <.020 3.30 .060  Site 384610104453501; well SC01506603DDB Security 14 (lat 38°46′10″, long 104°45′35″)Continued  06-22-82 1450 13.5 7.2 540 349 14 <0.020 5.90 <0.060 2.1 07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 1.4 09-17-82 1030 12.5 6.8 496 403 16 <.020 5.40 .100 1.2 10-22-82 1110 13.0 530 336 17 <.020 6.40 <.060 1.1 11-19-82 1120 13.5 6.9 525 349 19 <.020 7.00 <.060 .60   |          |      |                          |                                |   |   |  |  |   |  |   | 6.7  |
| 01-20-82 1050 13.5 6.6 504 336 17 <.020 6.40 .150 .41 02-24-82 0950 13.5 6.7 503 338 15 <.020 6.40 <.060 2.0 03-26-82 1015 13.5 6.6 511 336 15 <.020 5.10 .100 .76 04-30-82 1045 13.5 6.8 512 348 17 <.020 6.10 .070 .95 05-28-82 1020 13.0 6.8 511 340 16 <.020 3.30 .060  Site 384610104453501; well SC01506603DDB Security 14 (lat 38°46'10", long 104°45'35")Continued  06-22-82 1450 13.5 7.2 540 349 14 <0.020 5.90 <0.060 2.1 07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 1.4 09-17-82 1030 12.5 6.8 496 403 16 <.020 5.40 .100 1.2 10-22-82 1110 13.0 530 336 17 <.020 6.40 <.060 1.1 11-19-82 1120 13.5 6.9 525 349 19 <.020 7.00 <.060 .60   |          |      |                          |                                |   |   |  |  |   |  |   | 8.1  |
| 02-24-82 0950 13.5 6.7 503 338 15 <.020 6.40 <.060 2.0 03-26-82 1015 13.5 6.6 511 336 15 <.020 5.10 .100 .76 04-30-82 1045 13.5 6.8 512 348 17 <.020 6.10 .070 .95 05-28-82 1020 13.0 6.8 511 340 16 <.020 3.30 .060  Site 384610104453501; well SC01506603DDB Security 14 (lat 38°46′10″, long 104°45′35″)Continued  06-22-82 1450 13.5 7.2 540 349 14 <0.020 5.90 <0.060 2.1 07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 1.4 09-17-82 1030 12.5 6.8 496 403 16 <.020 5.40 .100 1.2 10-22-82 1110 13.0 530 336 17 <.020 6.40 <.060 1.1 11-19-82 1120 13.5 6.9 525 349 19 <.020 7.00 <.060 .60   |          |      |                          |                                |   |   |  |  |   |  |   | 5.8  |
| 03-26-82 1015 13.5 6.6 511 336 15 <.020 5.10 .100 .76 04-30-82 1045 13.5 6.8 512 348 17 <.020 6.10 .070 .95 05-28-82 1020 13.0 6.8 511 340 16 <.020 3.30 .060  Site 384610104453501; well SC01506603DDB Security 14 (lat 38°46'10", long 104°45'35")Continued  06-22-82 1450 13.5 7.2 540 349 14 <0.020 5.90 <0.060 2.1 07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 1.4 09-17-82 1030 12.5 6.8 496 403 16 <.020 5.40 .100 1.2 10-22-82 1110 13.0 530 336 17 <.020 6.40 <.060 1.1 11-19-82 1120 13.5 6.9 525 349 19 <.020 7.00 <.060 .60  |          |      |                          |                                |   |   |  |  |   |  |   | 6.8  |
| 04-30-82 1045 13.5 6.8 512 348 17 <.020 6.10 .070 .95 05-28-82 1020 13.0 6.8 511 340 16 <.020 3.30 .060  Site 384610104453501; well SC01506603DDB Security 14 (lat 38°46'10", long 104°45'35")Continued  06-22-82 1450 13.5 7.2 540 349 14 <0.020 5.90 <0.060 2.1 07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 1.4 09-17-82 1030 12.5 6.8 496 403 16 <.020 5.40 .100 1.2 10-22-82 1110 13.0 530 336 17 <.020 6.40 <.060 1.1 11-19-82 1120 13.5 6.9 525 349 19 <.020 7.00 <.060 .60  |          |      |                          |                                |   |   |  |  |   |  |   | 8.4  |
| 05-28-82 1020 13.0 6.8 511 340 16 <.020 3.30 .060  Site 384610104453501; well SC01506603DDB Security 14 (lat 38°46'10", long 104°45'35")Continued  06-22-82 1450 13.5 7.2 540 349 14 <0.020 5.90 <0.060 2.1  07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 1.4  09-17-82 1030 12.5 6.8 496 403 16 <.020 5.40 .100 1.2  10-22-82 1110 13.0 530 336 17 <.020 6.40 <.060 1.1  11-19-82 1120 13.5 6.9 525 349 19 <.020 7.00 <.060 .60  |          |      |                          |                                |   |   |  |  |   |  |   | 5.8  |
| Site 384610104453501; well SC01506603DDB Security 14 (lat 38°46'10", long 104°45'35")Continued  06-22-82 1450 13.5 7.2 540 349 14 <0.020 5.90 <0.060 2.1  07-16-82 1020 13.0 6.9 493 350 17 <.020 6.40 <.060 1.4  09-17-82 1030 12.5 6.8 496 403 16 <.020 5.40 .100 1.2  10-22-82 1110 13.0 530 336 17 <.020 6.40 <.060 1.1  11-19-82 1120 13.5 6.9 525 349 19 <.020 7.00 <.060 .60   |          |      |                          |                                |   |   |  |  |   |  |   | 7.1  |
| 06-22-82     1450     13.5     7.2     540     349     14     <0.020  | 05-28-82 | 1020 | 13.0                     | 6.8                            | 511                                     | 340   | 16                                       | <.020  | 3.30  | .060   |   |  |
| 07-16-82     1020     13.0     6.9     493     350     17     <.020   |          | Si   | te 384610                | 104453501                      | ; well SCO                              | 1506603DDB  | Security 14                              | (lat 38°46   | '10", long  | 104°45'35")  | Continued   |  |
| 09-17-82     1030     12.5     6.8     496     403     16     <.020   | 06-22-82 | 1450 | 13.5                     | 7.2                            | 540                                     | 349   | 14                                       | <0.020   | 5.90  | <0.060   | 2.1   | 8.0  |
| 09-17-82     1030     12.5     6.8     496     403     16     <.020   | 07-16-82 | 1020 | 13.0                     | 6.9                            | 493                                     | 350   | 17                                       | <.020  | 6.40  | <.060  | 1.4   | 7.8  |
| 11-19-82 1120 13.5 6.9 525 349 19 <.020 7.00 <.060 .60  | 09-17-82 | 1030 |                          | 6.8                            |   |   | 16                                       | <.020  |   |  | 1.2   | 6.6  |
|   |          |      | 13.0                     |                                |   |   | 17                                       |  | 6.40  |  |   | 7.5  |
| 12-17-82 1110 13.5 7.0 522 351 18 <.020 7.00 <.060 .90  |          |      |                          |                                |   |   |  |  |   |  |   | 7.6  |
|   | 12-17-82 | 1110 | 13.5                     | 7.0                            | 522                                     | 351   | 18                                       | <.020  | 7.00  | <.060  | . 90  | 7.9  |

Table 11.0-2.--Ground-water quality data--Continued

| Date                 | Time         | Temper-<br>ature<br>(°C) | pH<br>(stand-<br>ard<br>units) | Specific<br>conduct-<br>ance<br>(µS/cm) | Dissolved-<br>solids<br>residue<br>at 105°C<br>(mg/L) | Dissolved<br>chloride<br>(mg/L<br>as Cl) | Dissolved<br>nitrite<br>nitrogen<br>(mg/L<br>as N) | Dissolved<br>nitrogen<br>NO <sub>2</sub> +NO <sub>3</sub><br>(mg/L<br>as N) | Dissolved<br>ammonia<br>nitrogen<br>(mg/L<br>as N) | Dissolved nitrogen, ammonia and organic (mg/L as N) | Dis-<br>solved<br>nitroger<br>(mg/L<br>as N) |
|----------------------|--------------|--------------------------|--------------------------------|---|---|--|--|---|--|---|--|
|                      |              | Site 3                   | 3845071044                     | 443501; wel                             | 1 SC01506611  | IDCD Securi                              | ty 15 (lat   | 38°45'07",  | long 104°44  | <u>''35")</u>                                       |  |
| 06-22-81             | 1130         | 14.0                     | 6.5                            | 518                                     | 367   | 19                                       | .000   | 9.30  | .020   | 1.6   | 2.5  |
| 08-19-81             | 0940         | 13.0                     | 6.9                            | 690                                     | 452   | 26                                       | .030   | 6.20  | . 170  | 1.2   | 7.4  |
| 06-22-82             | 1130         | 13.5                     | 6.8                            | 705                                     | 453   | 26                                       | <.020  | 6.30  | .090   | 1.6   | 7.9  |
|                      |              | Site 3                   | 8844591044                     | 43401; wel                              | 1 SC01506614  | AAC1 Secur                               | ity 16 (lat  | 38°44'59",  | long 104°4   | 4'34")  |  |
| 08-19-81             | 0905         | 13.5                     | 6.8                            | 670                                     | 424   | 25                                       | .030   | 6.60  | . 160  | 1.0   | 7.6  |
| 09-18-81             | 0915         | 13.0                     | 6.6                            |   | 474   | 29                                       | .020   | 4.90  | .110   | 1.2   | 6.1  |
| 10-26-81             | 1040         | 13.0                     | 6.5                            | 730                                     | 470   | 32                                       | <.020  | 6.00  | <.060  | 1.1   | 7.1  |
| 11-24-81             | 1030         | 13.0                     | 6.5                            | 695                                     | 483   | 27                                       | .020   | 9.00  | . 160  | .81   | 9.8  |
| 06-22-82             | 1110         | 14.0                     | 6.8                            | 750                                     | 476   | 25                                       | <.020  | 5.40  | .060   | 1.6   | 7.0  |
| 08-13-82             | 1050         | 13.0                     | 6.5                            | 680                                     | 506   | 29                                       | <.020  | 5.10  | . 120  | 1.4   | 6.5  |
|                      |              | Site 3                   | 8844421044                     | 41201; wel                              | 1 SC01506613  | BBCC1 Secur                              | rity 17 (lat                                       | 38°44'42",  | long 104°4   | 4'12")  |  |
| 06-23-81             | 1125         | 14.0                     | 6.5                            | 610                                     | 427   | 25                                       | .000   | 7.00  | <.060  | 1.0   | 8.0  |
| 06-21-82             | 1510         | 13.5                     | 6.7                            | 730                                     | 484   | 31                                       | <.020  | 4.90  | .070   | 2.0   | 6.9  |
|                      |              | Sit                      | e 3844271                      | 104440301;                              | well SC01506  | 6613CAA REA                              | M 1 (lat 38  | 3°44'27", 1c  | ong 104°44'0                                       | <u>13")</u>   |  |
| 06-23-81             | 1145         | 14.0                     | 7.0                            | 860                                     | 619   | 41                                       | .000   | 7.00  | .070   | 1.4   | 8.4  |
| 06-21-82             |              | 15.0                     | 6.7                            | 930                                     | 584   | 38                                       | <.020  | 4.20  | <.060  | 1.3   | 5.5  |
|                      |              | <u>S</u> it              | e 3844161                      | 104435401;                              | well SC01506  | 6613CDC REA                              | M 2 (lat 38  | 3°44'16", lo  | ong 104°43'5                                       | (4")  |  |
| 06-22-81             | 1455         | 14.0                     | 6.9                            | 678                                     | 487   | 31                                       | .000   | 6.60  | <.060  | 1.2   | 7.8  |
| 06-21-82             | 1320         | 14.0                     | 6.8                            | 760                                     | 503   | 34                                       | <.020  | 5.00  | .070   | 1.7   | 6.7  |
|                      |              | Site 3                   | 8844131044                     | 34601; wel                              | 1 SC01506624  | 4BAA1 Widef                              | ield 1 (lat  | : 38°44'13",  | long 104°4   | 3'46")  |  |
| 06 07 01             | 00/5         | 1/ 5                     | <i>(</i> 0                     | 705                                     | 501   | 27                                       | 000  | 0.00  | . 110  | 1.6   | 10   |
| 06-24-81<br>06-24-82 | 0945<br>0930 | 14.5<br>13.0             | 6.8<br>7.3                     | 795<br>740                              | 581<br>530  | 37<br>28                                 | .000<br><.020                                      | 8.80<br>9.40  | <.060  | 1.6   | 11   |
| 00 24 02             | 0930         |                          |                                |   |   |  |  |   |  |   | ••   |
|                      |              | Site 3                   | 3844111044                     | 34301; wel                              | 1 SC01506624  | BAA2 Widef                               | ield 2 (lat  | 38°44'11",  | long 104°4   | 3'43")  |  |
| 06-24-81             | 1015         | 14.5                     | 7.1                            | 850                                     | 623   | 36                                       | .000   | 7.20  | .110   | 1.1   | 8.3  |
| 05-06-82             | 0903         |                          | 6.8                            | 907                                     |   |  |  | 8.40  | . 130  |   |  |
| 05-06-62             | 0905         | 13.0                     | 6.7                            | 900                                     |   | ~-                                       | ~-   | 8.40  | .080   |   |  |
| 05-06-82             | 0907         | 13.0                     | 6.7                            | 905                                     |   | ~ ~                                      | ~=   | 8.40  | .080   |   |  |
| 05-06-82             | 0912         | 13.0                     | 6.7                            | 900                                     |   |  |  | 8.50  | .070   |   |  |
| 05-06-82             | 0922         | 13.0                     | 6.8                            | 903                                     | -~  |  |  | 8.50  | .070   |   | ~-   |
| 05-06-82             | 0952         | 12.5                     | 6.7                            | 902                                     |   |  |  | 8.50  | <.060  |   |  |
| 05-06-82             | 1102         | 13.5                     | 6.7                            | 891                                     |   |  | ~-   | 8.50  | <.060  |   |  |
| 05-06-82             | 1502         | 14.0                     | 6.8                            | 890                                     |   |  |  | 8.50  | <.060  |   |  |
| 05-06-82             | 1902         | 14.5                     | 6.8                            | 908                                     |   |  |  | 8.50  | <.060  |   |  |
| 05-07-82<br>06-24-82 | 0902<br>1030 | 13.0<br>14.0             | 6.8<br>7.4                     | 883<br>870                              | 600   | 35                                       | <.020  | 8.40<br>8.90  | .060<br><.060                                      | 1.9   | 11   |
| 00-24-82             | 1030         |                          |                                |   |   |  |  |   |  |   | **   |
|                      |              | Site 3                   | 844021044                      | 34801; wel                              | 1 SC01506624  | BAD2 Widef                               | ield 3 (lat  | 38°44'02",  | long 104°4   | 3'48")  |  |
| 06-24-81             | 1110         | 13.5                     | 6.7                            | 650                                     | 454   | 27                                       | .000   | 7.50  | . 120  | 1.2   | 8.7  |
| 06-24-82             |              | 14.0                     | 7.0                            | 660                                     | 453   | 26                                       | <.020  | 7.30  | <.060  | 1.7   | 9.0  |

Table 11.0-2.--Ground-water quality data--Continued

| Date     | Time | Temper-<br>ature<br>(°C)                | pH<br>(stand-<br>ard<br>units) | Specific<br>conduct-<br>ance<br>(µS/cm) | Dissolved-<br>solids<br>residue<br>at 105°C<br>(mg/L) | Dissolved<br>chloride<br>(mg/L<br>as Cl) | Dissolved<br>nitrite<br>nitrogen<br>(mg/L<br>as N) | Dissolved<br>nitrogen<br>NO <sub>2</sub> +NO <sub>3</sub><br>(mg/L<br>as N) | Dissolved<br>ammonia<br>nitrogen<br>(mg/L<br>as N) | Dissolved nitrogen, ammonia and organic (mg/L as N) | Dis-<br>solved<br>nitroger<br>(mg/L<br>as N) |
|----------|------|---|--------------------------------|---|---|--|--|---|--|---|--|
|          |      | Site :                                  | 38440710 <u>4</u> 4            | 34801; wel                              | 1 SC01506624  | 4BAD1 Wider                              | field 4 (lat                                       | 38°44'07"   | , long 104°4                                       | 3'48")  |  |
| 02-13-81 | 0905 | 13.0                                    | 6.8                            |   | 571   | 38                                       | 0.000  | 8.70  | <0.060   | 1.1   | 9.8  |
| 03-19-81 | 0955 | 12.5                                    | 6.7                            | 910                                     | 586   | 39                                       | .000   | 7.80  | .060   | 1.0   | 8.8  |
| 04-21-81 | 1000 | 13.0                                    | 6.8                            | 770                                     | 534   | 33                                       | .000   | 7.60  | .070   | 1.2   | 8.8  |
| 05-19-81 | 1315 | 12.5                                    | 6.5                            | 771                                     | 525   | 34                                       | .010   | 6.20  | .060   | 1.3   | 7.5  |
| 06-24-81 | 1040 | 13.5                                    | 6.7                            | 727                                     | 515   | 34                                       | .000   | 6.70  | .100   | 1.1   | 7.8  |
| 07-17-81 | 1100 | 13.0                                    | 6.4                            |   | 518   | 36                                       | .000   | 7.00  | .110   | 1.0   | 8.0  |
| 08-19-81 | 1055 | 14.0                                    | 6.9                            | 810                                     | 524   | 36                                       | .030   | 7.00  | .130   | 1.2   | 8.2  |
| 09-18-81 | 1030 | 13.5                                    | 6.4                            | 803                                     | 549   | 35                                       | .020   | 6.00  | .120   | 1.3   | 7.3  |
| 10-26-81 | 1300 | 14.0                                    | 6.8                            | 774                                     | 497   | 37                                       | <.020  | 7.50  | <.060  | 1.3   | 8.8  |
| 11-24-81 | 1330 | 13.0                                    | 6.6                            | 716                                     | 487   | 26                                       | .020   | 9.20  | . 150  | .57   | 9.8  |
| 12-21-81 | 1140 | 13.0                                    | 6.4                            | 773                                     | 497   | 26                                       | <.020  | 5.90  | <.070  | .83   | 6.7  |
| 01-20-82 | 1200 | 13.5                                    | 6.3                            | 787                                     | 534   | 34                                       | <.020  | 7.20  | .120   | .95   | 8.2  |
| 02-24-82 | 1030 | 12.5                                    | 6.4                            | 794                                     | 531   | 33                                       | <.020  | 6.90  | <.060  | .81   | 7.7  |
| 03-26-82 | 1140 | 13.0                                    | 6.2                            | 782                                     | 521   | 31                                       | <.020  | 6.70  | .060   | .56   | 7.3  |
| 04-30-82 | 1115 | 13.0                                    | 6.5                            | 728                                     | 486   | 30                                       | <.020  | 6.70  | .070   | 1.1   | 7.8  |
| 05-28-82 | 0945 | 13.0                                    | 6.6                            | 737                                     | 464   | 31                                       | <.020  | 6.90  | .060   | 1.2   | 8.1  |
| 06-24-82 | 1100 | 13.5                                    | 7.1                            | 750                                     | 502   | 31                                       | <.020  | 6.20  | <.060  | 1.5   | 7.7  |
| 07-16-82 | 1130 | 13.0                                    | 6.7                            | 751                                     | 522   | 35                                       | <.020  | 6.60  | <.060  | 1.9   | 8.5  |
| 08-13-82 | 1215 | 15.0                                    | 6.6                            | 835                                     | 618   | 34                                       | <.020  | 6.00  | . 110  | 1.6   | 7.6  |
| 09-17-82 | 1115 | 13.0                                    | 6.5                            | 788                                     | 611   | 35                                       | <.020  | 5.60  | .070   | 1.8   | 7.4  |
| 10-22-82 | 1140 | 13.0                                    |                                | 770                                     | 508   | 34                                       | <.020  | 6.60  | <.060  | 2.6   | 9.2  |
| 11-19-82 | 1000 | 14.0                                    | 7.0                            | 769                                     | 460   | 35                                       | <.020  | 7.00  | <.060  | 1.1   | 8.1  |
| 12-17-82 | 1025 | 13.5                                    | 6.7                            | 771                                     | 516   | 36                                       | <.020  | 7.00  | <.060  | 1.0   | 8.0  |
|          |      | Site 3                                  | 3843231044                     | 32201: wel                              | 1 SC01506625  | SAAR Widefi                              | ield 5 (lat  | 38943123".  | lone 104°43  | (' 22")   |  |
|          |      |   |                                |   |   |  |  |   |  | <del></del>   |  |
| 07-21-82 | 1330 | 14.0                                    | 6.9                            | 1,350                                   | 1,020   | 53                                       | <.020  | 8.00  | .060   | 1.2   | 9.2  |
|          |      | Site 3                                  | 3843431044                     | 32501; wel                              | 1 SC01506624  | DAB Widefi                               | eld 7 (lat   | 38°43'43",  | long 104°43  | 3'25")  |  |
| 06-24-81 | 1335 | 15.0                                    | 7.2                            | 703                                     | 485   | 24                                       | .000   | 7.20  | .120   | 1.4   | 8.6  |
| 06-02-82 | 1530 | 14.0                                    | 7.3                            | 720                                     | 520   | 28                                       | <.020  | 6.80  | <.060  | 1.4   | 8.2  |
|          |      | Site 3                                  | 3846101044                     | 32401; wel                              | 1 SC01506601  | DDB Widefi                               | ield 8 (lat  | 38°46'10",  | long 104°43  | 3'24")  |  |
| 06-24-81 | 1550 | 1/. 0                                   | 7.0                            | 661                                     | 222   | 6.2                                      | 000  | 5 10  | 120  | 1.2   | 6.3  |
| 06-24-81 |      | 14.0<br>13.0                            | 7.2<br>7.6                     | 441<br>440                              | 323<br>292  | 6.2<br>6.5                               | .000<br><.020                                      | 5.10<br>5.30  | .120<br>.060                                       | 1.2<br>1.9  | 7.2  |
|          |      |   |                                |   |   |  |  |   |  |   |  |
|          |      | Site 3                                  | 3845531044                     | 32901; wel                              | 1 SC01506602  | ZABA Widefi                              | leld 9 (lat  | 38°45'53",  | long 104°43  | 3129")  |  |
| 06-24-81 | 1610 | 13.5                                    | 7.2                            | 448                                     | 305   | 5.9                                      | .000   | 5.00  | .110   | 1.1   | 6.1  |
| 06-25-82 | 1100 | 13.0                                    | 7.6                            | 460                                     | 290   | 6.6                                      | <.020  | 5.00  | <.060  | 2.4   | 7.4  |
|          |      | Site 3                                  | 3846281044                     | 32301; wel                              | 1 SC01506601  | ADC Widefi                               | eld 11 (lat  | 38°46'28",  | long 104°4   | 3'23")  |  |
| 06-25-81 | 1025 | 15.0                                    | 7.4                            | 486                                     | 306   | 6.3                                      | .000   | 4.20  | .070   | .92   | 5.1  |
| 06-25-82 |      | 13.0                                    | 7.6                            | 480                                     | 290   | 6.0                                      | <.020  | 3.70  | .070   | 1.6   | 5.3  |
|          |      | Site 3                                  | 3845441044                     | 33101; wel                              | 1 SC01506612  | ACA Widefi                               | eld 12 (lat  | . 38°45'44''.   | long 104°4   | 3'31")  |  |
| 07 07 07 |      | *************************************** |                                |   |   |  |  |   |  | <del></del>   | 0.5  |
| 07-07-82 | 1530 | 17.0                                    | 7.2                            | 580                                     | 388   | 13                                       | <.020  | 7.20  | .070   | 1.3   | 8.5  |

Table 11.0-2.--Ground-water quality data--Continued

| Date     | Time | Temper-<br>ature<br>(°C) | pH<br>(stand-<br>ard<br>units) | Specific<br>conduct-<br>ance<br>(µS/cm) | Dissolved-<br>solids<br>residue<br>at 105°C<br>(mg/L) | Dissolved<br>chloride<br>(mg/L<br>as Cl) | Dissolved<br>nitrite<br>nitrogen<br>(mg/L<br>as N) | Dissolved<br>nitrogen<br>NO <sub>2</sub> +NO <sub>3</sub><br>(mg/L<br>as N) | Dissolved<br>ammonia<br>nitrogen<br>(mg/L<br>as N) | Dissolved nitrogen, ammonia and organic (mg/L as N) | Dis-<br>solved<br>nitrogen<br>(mg/L<br>as N) |
|----------|------|--------------------------|--------------------------------|---|---|--|--|---|--|---|--|
|          |      | Site 3                   | 3843131044                     | 31801; wel                              | 1 SC01506625  | SAAD Widefi                              | eld 14 (lat  | . 38°43'13",  | long 104°4   | 3'18")  |  |
| 06-24-81 | 1425 | 14.0                     | 7.1                            | 1,240                                   | 937   | 45                                       | .000   | 10.0  | .110   | 1.0   | 11   |
| 01-20-82 |      | 13.5                     | 6.5                            | 1,510                                   | 1,150   | 50                                       | <.020  | 10.7  | . 110  | 1.1   | 12   |
| 02-24-82 | 1105 | 13.5                     | 6.5                            | 1,550                                   | 1,190   | 50                                       | <.020  | 11.0  | .060   | 1.1   | 12   |
| 03-26-82 | 1115 | 14.0                     | 6.4                            | 1,500                                   | 1,150   | 49                                       | <.020  | 10.0  | .080   | .32   | 10   |
| 04-30-82 | 1140 | 14.0                     | 6.7                            | 1,400                                   | 1,040   | 49                                       | <.020  | 9.20  | .060   | 1.1   | 10   |
|          | Sit  | e 3843131                | 04431801;                      | well SC01                               | 506625AAD V   | Videfield 14                             | (lat 38°43   | '13", long  | 104°43'18")  | Continued   |  |
| 05-28-82 | 0930 | 14.0                     | 6.6                            | 1,370                                   | 1,030   | 50                                       | <0.020   | 9.10  | 0.090  | 1.6   | 11   |
| 06-25-82 | 1230 | 13.0                     | 7.3                            |   | 1,220   | 52                                       | <.020  | 9.60  | .090   | 1.7   | 11   |
| 07-16-82 | 1200 | 13.0                     | 6.9                            | 1,540                                   | 1,220   | 53                                       | <.020  | 11.0  | . 090  | 2.1   | 13   |
| 08-13-82 | 1245 | 13.0                     | 6.8                            | 1,500                                   | 1,190   | 55                                       | <.020  | 12.0  | .120   | 2.1   | 14   |
| 09-17-82 | 1140 | 13.0                     | 6.7                            | 1,480                                   | 1,230   | 58                                       | <.020  | 11.0  | .060   | 1.9   | 13   |
| 10-22-82 | 1205 | 13.5                     |                                | 1,500                                   | 1,110   | 57                                       | <.020  | 11.0  | <.060  | 1.2   | 12   |
| 11-19-82 | 1200 | 13.5                     | 7.0                            | 1,470                                   | 1,080   | 60                                       | <.020  | 10.0  | <.060  | 1.2   | 11   |
| 12-17-82 |      |                          | 6.9                            | 1,480                                   | 1,130   | 58                                       | <.020  | 9.60  | .060   | 1.0   | 11   |
|          |      | Site                     | 38434610                       | 04433301; w                             | ell SC015066  | 24DBA Cere                               | sa 1 (lat 3  | 8°43'46", 1   | ong 104°43'  | <u>33")</u>   |  |
| 06-24-81 | 1305 | 15.0                     | 7.4                            | 779                                     | 549   | 32                                       | .000   | 8.10  | 100  | .76   | 8.9  |
| 06-24-82 |      | 14.5                     | 7.9                            | 800                                     | 535   | 30                                       | <.020  | 7.80  | <.060  | 1.1   | 8.9  |
|          |      | Site                     | 38434710                       | )4434201; w                             | ell SC015066  | 24DBB Cere                               | sa 3 (lat 3  | 8°43'47", 1   | ong 104°43'  | <u>42")</u>   |  |
| 06-24-81 | 1140 | 14.5                     | 7.1                            | 703                                     | 497   | 31                                       | .000   | 8.00  | .110   | .95   | 9.0  |
| 06-24-82 |      | 14.0                     | 7.5                            | 750                                     | 486   | 28                                       | <.020  | 8.40  | <.060  | 1.6   | 10   |
|          |      | Site                     | 38432710                       | 4432501; w                              | ell SC015066  | 24DDC Enfe                               | ld 3 (lat 3  | 8°43'27", 1   | ong 104°43'  | 25")  |  |
| 06-24-81 | 1355 | 14.0                     | 6.9                            | 804                                     | 570   | 31                                       | .000   | 7.20  | .110   | 1.2   | 8.4  |
| 06-24-82 | 1600 | 14.0                     | 7.2                            | 760                                     | 517   | 27                                       | <.020  | 6.40  | .070   | .90   | 7.3  |
|          |      | Sit                      | e 3843481                      | 04391201;                               | well SC01506  | 5522DBB2 JH                              | W 1 (lat 38  | °43'48", 10   | ng 104°39'1  | <u>2")</u>  |  |
| 06-28-82 | 1300 | 14.0                     | 7.2                            | 1,650                                   | 1,200   | 30                                       | <.020  | 1.70  | .070   | 1.2   | 2.9  |
|          |      | sit                      | e 3843491                      | 04390401;                               | well SC01506  | 522DBA1 JH                               | W 2 (lat 38  | °43'49", lo   | ng 104°39'0  | <u>4")</u>  |  |
| 06-25-82 | 1600 | 13.0                     | 7.5                            | 1,300                                   | 1,120   | 39                                       | <.020  | 2.70  | <.060  | 1.7   | 4.4  |
|          |      | Sit                      | e 3843471                      | 04390901;                               | well SC01506  | 522DBB JHW                               | 3 (lat 38°   | 43'47", lon   | g 104°39'09  | <u>")</u>   |  |
| 06-28-82 | 1330 | 14.0                     | 7.4                            | 1,520                                   | 1,380   | 24                                       | <.020  | 1.40  | <.070  | 1.0   | 2.4  |
|          |      | Sit                      | e 3843391                      | 04390001;                               | well SC01506  | 522DBD JHW                               | 4 (lat 38°   | 43'39", lon   | g 104°39'00  | <u>")</u>   |  |
| 06-25-82 | 1500 | 13.0                     | 7.6                            | 1,300                                   | 900   | 44                                       | <.020  | 2.70  | .080   | 1.7   | 4.4  |
|          |      | Sit                      | e 3843471                      | 04385901;                               | well SC01506  | 522DBA4 JH                               | W 5 (lat 38  | °43'47", lo   | ng 104°38'5  | 9")   |  |
| 06-28-82 | 1415 | 14.0                     | 7.5                            | 1,620                                   | 1,270   | 34                                       | <.020  | 2.50  | .070   | 1.5   | 4.0  |
|          |      |                          |                                | -,                                      | -,  |  |  |   |  |   |  |

Table 11.0-2.--Ground-water quality data--Continued

| Date     | Time     | Temper-<br>ature<br>(°C) | pH<br>(stand-<br>ard<br>units) | Specific<br>conduct-<br>ance<br>(µS/cm) | Dissolved-<br>solids<br>residue<br>at 105°C<br>(mg/L) | Dissolved<br>chloride<br>(mg/L<br>as Cl) | Dissolved<br>nitrite<br>nitrogen<br>(mg/L<br>as N) | Dissolved<br>nitrogen<br>NO <sub>2</sub> +NO <sub>3</sub><br>(mg/L<br>as N) | Dissolved<br>ammonia<br>nitrogen<br>(mg/L<br>as N) | Dissolved nitrogen, ammonia and organic (mg/L as N) | Dis-<br>solved<br>nitrogen<br>(mg/L<br>as N) |
|----------|----------|--------------------------|--------------------------------|---|---|--|--|---|--|---|--|
|          |          |                          | MISCEI                         | LANEOUS WE                              | LLS (general  | lly located                              | north to so  | uth in stud   | y area)  |   |  |
|          |          | Sit                      | e 3849051                      | 04491301;                               | well SC01406  | 6619ACC Man                              | ley (lat 38  | °49'05", lo   | ng 104°49'1  | 3")   |  |
| 07-20-82 | 1445     | 16.0                     | 6.9                            | 1,120                                   | 803   | 39                                       | <.020  | 8.40  | .060   | .80   | 9.2  |
|          |          | Sit                      | e 3848391                      | 04490601;                               | well SC01406  | 6619DCD Hay                              | es (lat 38°  | 48'39", lon   | g 104°49'06  | <u>")</u>   |  |
| 07-07-82 | 1200     | 13.0                     | 6.8                            | 320                                     | 189   | 11                                       | <.020  | .960  | .060   | .50   | 1.5  |
| Site 384 | 840104   | 482201; w                | ell SC014                      | 06620CDC1                               | Colorado Sp   | rings Sewag                              | e Treatment  | Plant well  | (lat 38°48   | '40", long 10                                       | 4°48'22")                                    |
| 07-02-81 | 1445     | 13.0                     | 6.6                            | 1,520                                   | 1,170   | 65                                       | .000   | . 100   | .800   | .99   | 1.1  |
| 07-09-82 | -        | 14.0                     | 6.8                            | 1,200                                   | 861   | 48                                       | .030   | .520  | 1.40   | 1.8   | 2.3  |
|          |          | Site                     | 384746104                      | 453501; we                              | 11 SC0140662  | 7DDC HA &                                | AC 7 (lat 3  | 8°47'46", 1   | ong 104°45'  | 35")  |  |
| 03-11-82 | 1245     | 13.0                     | 7.4                            | 890                                     | 409   | 22                                       | .020   | .410  | 5.20   | 5.9   | 6.3  |
|          |          | Site 38                  | 481410447                      | 3101; well                              | SC01406628B   | BCC Janitel                              | l Road (lat  | 38°48'14",  | long 104°4   | 7'31")  |  |
| 06-25-81 | 1610     | 13.5                     | 6.7                            | 920                                     | 627   | 41                                       | 0.000  | 7.70  | 0.060  | 1.4   | 9.1  |
| 04-13-82 | 1350     | 17.0                     | 6.8                            | 1,080                                   | 775   | 37                                       | <.020  | 6.20  | .070   | .53   | 6.7  |
| 07-06-82 | 1330     | 14.0                     | 6.9                            | 1,000                                   | 614   | 40                                       | .040   | 9.00  | .060   | 2.2   | 11   |
| 10-14-82 | 1520     |                          | 6.5                            | 932                                     | 631   | 34                                       | .090   | 7.30  | .070   | 1.5   | 8.8  |
| 12-20-82 | 1530     | 12.0                     | 6.2                            | 898                                     | 627   | 37                                       | .020   | 5.50  | . 270  | .90   | 6.4  |
|          |          | Site 38                  | 474710447                      | 3701; well                              | SC01406628C   | CC1 Standa                               | rd gas (la   | t 38°47'47"   | , long 104°  | 47'37")   |  |
| 04-14-82 | 1245     | 15.0                     | 6.5                            | 662                                     | 442   | 54                                       | .020   | 6.60  | .090   | .71   | 7.3  |
| 07-09-82 | 1035     | 14.0                     | 6.9                            | 600                                     | 389   | 39                                       | <.020  | 7.80  | .070   | 1.5   | 18   |
| 12-20-82 | 1510     | 13.0                     | 5.8                            | 1,300                                   | 942   | 300                                      | <.020  | 6.50  | .070   | 1.1   | 7.6  |
|          |          | Site 38                  | 474710447                      | 3201; well                              | SC01406628C   | CCC2 Traile                              | r Park (lat  | 38°47'47",  | long 104°4   | 7'32")  |  |
| 04-14-82 | 1340     | 13.0                     | 6.7                            | 641                                     | 411   | 55                                       | <.020  | 5.50  | . 160  | 1.1   | 6.6  |
| 07-09-82 | 1010     | 16.0                     | 7.0                            | 710                                     | 431   | 49                                       | .020   | 7.20  | .150   | 1.6   | 8.8  |
|          |          | Site                     | 384755104                      | 480301; we                              | 11 SC0140662  | 9DCA1 Robe                               | rtson (lat   | 38°47'55",  | long 104°48  | '03")   |  |
| 07-20-82 | 1330     | 14.5                     | 6.8                            | 650                                     | 403   | 38                                       | <.020  | 7.10  | .060   | 1.7   | 8.8  |
|          | <u>s</u> | ite 38473                | 810447380                      | 1; well SC                              | 01406632AAD   | Harrison H                               | igh School   | (lat 38°47'   | 38", long 1  | 04°47'38")  |  |
| 06-25-81 |          | 14.5                     | 6.7                            | 804                                     | 550   | 33                                       | .000   | 8.90  | .080   | 1.2   | 10   |
| 04-14-82 |          | 14.5                     | 6.9                            | 843                                     | 594   | 36                                       | <.020  | 7.50  | .080   | .63   | 8.1  |
| 07-06-82 | 1215     | 15.0                     | 7.1                            | 790                                     | 568   | 34                                       | <.020  | 7.60  | <.060  | 1.7   | 9.3  |
|          |          | Sit                      | e 3847181                      | 04463701;                               | well SC01406  | 633DAA Bar                               | nes (lat 38  | °47'18", lo   | ng 104°46'3  | <u>7")</u>  |  |
| 06-25-81 |          | 15.5                     | 6.9                            | 1,310                                   | 951   | 45                                       | .000   | 14.0  | .060   | 1.6   | 16   |
| 07-01-82 | 0900     | 14.0                     | 7.3                            | 1,100                                   | 985   | 33                                       | <.020  | 13.0  | <.070  | 1.2   | 14   |
|          |          | Site 38                  | 465910 <b>44</b> 6             | 4301; well                              | SC01406633D   | DC Colar C                               | ompound (la  | t 38°46'59"   | , long 104°  | <u>46'43")</u>                                      |  |
| 10-13-82 | 1130     | 15.5                     | 7.3                            | 230                                     | 165   | 3.1                                      | <.020  | 1.10  | <.060  | 1.0   | 2.1  |

Table 11.0-2.--Ground-water quality data--Continued

| Date                 | Time | Temper-<br>ature<br>(°C) | pH<br>(stand-<br>ard<br>units) | Specific<br>conduct-<br>ance<br>(µS/cm) | Dissolved-<br>solids<br>residue<br>at 105°C<br>(mg/L) | Dissolved<br>chloride<br>(mg/L<br>as Cl) | Dissolved<br>nitrite<br>nitrogen<br>(mg/L<br>as N) | Dissolved<br>nitrogen<br>NO <sub>2</sub> +NO <sub>3</sub><br>(mg/L<br>as N) | Dissolved<br>ammonia<br>nitrogen<br>(mg/L<br>as N) | Dissolved nitrogen, ammonia and organic (mg/L as N) | Dis-<br>solved<br>nitroger<br>(mg/L<br>as N) |
|----------------------|------|--------------------------|--------------------------------|---|---|--|--|---|--|---|--|
|                      |      | Site                     | 384746104                      | 452801; we                              | 11 SC0140663  | 34AAA HA &                               | AC 8 (lat 3  | 38°47'46", 1  | ong 104°45'  | 28")  |  |
| 03-11-82             | 1120 |                          | 7.2                            | 535                                     | 345   | 13                                       | <.020  | 2.30  | .070   | .72   | 3.0  |
| 06-18-82             |      | 14.0                     | 6.9                            | 580                                     | 413   | 23                                       | . 020  | 2.70  | . 200  | 1.0   | 3.7  |
| 12-20-82             | 1430 | 13.0                     | 6.3                            | 532                                     | 361   | 40                                       | <.020  | 2.20  | .120   | 1.0   | 3.2  |
|                      |      | Site 38                  | 471710445                      | 5201; well                              | SC01406634I   | OBB1 Cormac                              | k East (lat  | . 38°47'17",  | long 104°4   | 5'52")  |  |
| 03-10-82             | 1700 |                          | 6.9                            | 1,340                                   | 860   | 120                                      | <.020  | 1.00  | .390   | 1.5   | 1.6  |
|                      |      | Site 3                   | 847171044                      | 55301; wel                              | 1 SC01406634  | DBB2 Cormac                              | k West (lat  | . 38°47'17",  | long 104°4   | 5'53")  |  |
| 03-11-82             | 1700 | 14.0                     | 6.9                            | 1,380                                   | 827   | 100                                      | <.020  | .500  | . 390  | 1.4   | 1.9  |
| 07-15-82             |      | 14.0                     | 6.8                            | 1,250                                   | 783   | 86                                       | <.020  | .590  | .410   | 1.4   | 2.0  |
| 10-28-82             | 1735 | 13.0                     | 6.9                            | 1,180                                   | 757   | 82                                       | <.020  | .690  | .480   | 1.5   | 2.2  |
|                      |      | Site                     | 38465610                       | 14460901; w                             | ell SC014066  | 34CDC Corma                              | c <b>k 3 (</b> lat 3                               | 8°45'56", 1   | ong 104°46'  | <u>09)</u>  |  |
| 10-14-82             | 1400 |                          | 6.8                            | 1,150                                   | 844   | 27                                       | <.020  | 7.90  | .060   | 1.2   | 9.1  |
|                      |      | <u>Site 384</u>          | 658104460                      | 0001; well                              | SC01406634CI  | DD1 Cormack                              | Domestic (1  | at 38°46'58   | ", long 104  | °46'00"   |  |
| 03-10-82             | 1400 |                          | 7.4                            | 1,030                                   | 686   | 55                                       | <.020  | 3.90  | .060   | .71   | 4.6  |
| 07-09-82             | –    | 16.0                     | 7.3                            | 1,100                                   | 709   | 52                                       | <.020  | 4.30  | <.060  | 1.1   | 5.4  |
| 10-14-82<br>12-20-82 |      |                          | 6.7<br>6.4                     | 986<br>955                              | 686<br>659  | 43<br>46                                 | <.020<br><.020                                     | 4.60<br>4.60  | <.060<br><.060                                     | 1.2<br>.70  | 5.8<br>5.3                                   |
|                      | -555 | Site                     |                                |   | 11 SC0150660  |  | •  |   |  |   | •      |
| 10-13-82             | 1220 | 13.5                     | 7.0                            | 550                                     | 367   | 29                                       | <0.020   | 15.0  | <0.060   | 1.2   | 16   |
| 10 15 02             | 1220 |                          |                                |   |   |  |  |   |  | 1.2   | 10   |
|                      |      |                          |                                |   | 1; well SCOI  |  |  |   |  |   |  |
| 10-13-82             | 1500 | 13.0                     | 7.2                            | 1,240                                   | 865   | 39                                       | <.020  | 27.0  | .070   | 1.6   | 29   |
|                      |      | Site                     | 384613104                      | 443601; we                              | 11 SC0150660  | 2DAC Burr                                | well (lat 3  | 8°46'13", 1   | ong 104°44'  | 36")  |  |
| 10-13-82             | 1430 | 12.0                     | 7.8                            | 1,420                                   | 1,080   | <b>3</b> 5                               | <.020  | 9.50  | .080   | 1.0   | 11   |
|                      |      | Site                     | 384639104                      | 461401; we                              | 11 SC0150660  | 3BAC1 Mars                               | Gas (lat   | 38°46'39",  | long 104°46  | <u>5'14")</u>                                       |  |
| 06-23-81             | 1450 | 16.5                     | 6.8                            | 884                                     | 659   | 23                                       | .010   | 9.90  | .070   | 1.0   | 11   |
| 07-01-82             | 1030 | 15.0                     | 7.1                            | 940                                     | 668   | 20                                       | <.020  | 13.0  | <.070  | .90   | 14   |
|                      |      | Site                     | 38464310                       | 4463601; w                              | ell SC015066  | 04AAD CSTL                               | CONC (lat°3  | 8'46"43, lo   | ng 104°46'3  | <u>16")</u>   |  |
| 10-14-82             | 1300 |                          | 6.4                            | 708                                     | 477   | 18                                       | <.020  | 5.00  | .060   | 1.1   | 6.1  |
|                      |      | Sit                      | e 3844431                      | 04441801;                               | well SC01506  | 6614ADD Cam                              | den (lat 38  | °44'43", lo   | ong 104°44'1                                       | .8")  |  |
| 06-25-81             |      | 13.5                     | 6.5                            | 775                                     | 520   | 33                                       | .000   | 6.80  | .060   | 1.2   | 8.0  |
| 07-09-82             | 1120 | 14.0                     | 7.0                            | 820                                     | 549   | 34                                       | <.020  | 4.00  | . 070  | 1.3   | 5.3  |
|                      |      | Site 38                  | 450910445                      | 4801; well                              | SC01506610I   | OCD B Ditch                              | well 1 (la   | t 38°45'09"   | , long 104°  | <u>'45'48")</u>                                     |  |
| 06-22-82             | 1400 | 11.0                     | 7.5                            |   | 6,050   | 100                                      | <.020  | 7.20  | <.060  | 1.4   | 8.6  |

Table 11.0-2.--Ground-water quality data--Continued

| Date                 | Time   | Temper-<br>ature<br>(°C) | pH<br>(stand-<br>ard<br>units) | Specific<br>conduct-<br>ance<br>(µS/cm) | Dissolved-<br>solids<br>residue<br>at 105°C<br>(mg/L) | Dissolved<br>chloride<br>(mg/L<br>as Cl) | Dissolved<br>nitrite<br>nitrogen<br>(mg/L<br>as N) | Dissolved<br>nitrogen<br>NO <sub>2</sub> +NO <sub>3</sub><br>(mg/L<br>as N) | Dissolved<br>ammonia<br>nitrogen<br>(mg/L<br>as N) | Dissolved nitrogen, ammonia and organic (mg/L as N) | Dis-<br>solved<br>nitrogen<br>(mg/L<br>as N) |
|----------------------|--------|--------------------------|--------------------------------|---|---|--|--|---|--|---|--|
|                      |        | Site 38                  | 454710445                      | 4801; well                              | SC01506615  | ABA B Ditch                              | well 2 (la   | t 38°45'47"   | , long 104°  | 45'48")   |  |
| 06-22-82             | 1600   | 11.0                     | 7.4                            |   | 25,900  | 240                                      | .040   | 1.00  | 1.10   | 3.3   | 4.3  |
| Sit                  | e 3844 | 091044408                | 01; well                       | SC01506624                              | BBB Securi  | ty Sewage Tr                             | eatment Pla  | nt well (la   | t 38°44'09"  | , long 104°44                                       | ("80"  |
| 06-25-81<br>07-09-82 |        | 14.0<br>14.0             | 6.7<br>7.2                     | 1,260<br>1,380                          | 794<br>789  | 120<br>110                               | .000<br>.190                                       | 5.90<br>4.00  | 4.20<br>2.40                                       | 5.5<br>3.0  | 11<br>7.0                                    |
|                      | Sit    | e 3844481                | 04441401;                      | well SC01                               | 506613BCB2  | Fountain Va                              | lley School  | (lat 38°44  | '48", long   | 104°44'14")   |  |
| 08-19-81<br>07-02-82 |        | 14.0<br>15.0             | 6.9<br>7.1                     | 655<br>760                              | 421<br>495  | 25<br>36                                 | .030<br><.020                                      | 6.40<br>6.10  | .130<br><.060                                      | .93<br>1.5  | 7.3<br>7.6                                   |
|                      | Si     | te 384437                | 104422601                      | ; well SCO                              | 1506518DBA  | Fountain Va                              | lley School  | (lat 38°44  | '37", long   | 104°42'26")   |  |
| 06-25-81<br>07-02-82 |        | 14.0<br>12.5             | 7.1<br>7.3                     | 1,620<br>1,620                          | 1,280<br>1,350  | 52<br>45                                 | .000<br><.020                                      | 4.60<br>3.40  | .060<br>.110                                       | .97<br>1.6  | 5.6<br>5.0                                   |
|                      |        | Site                     | 384308104                      | 431601; we                              | 11 SC0150662  | 25ADA1 Rice                              | Dom (lat 3   | 8°43'08", 1   | ong 104°43'  | 16")  |  |
| 07-09-82             | 1315   | 13.0                     | 7.4                            | 1,520                                   | 1,080   | 61                                       | <.020  | 5.10  | <.060  | 1.0   | 6.1  |
|                      |        | Site                     | 38430810                       | 4431901; w                              | ell SC015066  | 525ADA2 Ric                              | e 2 (lat 38  | °43'08", lo   | ng 104°43'1  | 9")   |  |
| 08-09-82             | 1530   | 14.0                     | 7.0                            | 1,300                                   | 1,090   | 54                                       | <.020  | 6.10  | .110   | .70   | 6.8  |
|                      |        | Site 3                   | 842361044                      | 25401; wel                              | 1 SC01506530  | CCD3 Finkb                               | einer (lat   | 38°42'36",  | long 104°42  | <u>'54")</u>  |  |
| 07-01-82             | 1400   | 14.0                     | 7.5                            | 900                                     | 583   | 41                                       | <.020  | 6.20  | <.070  | 1.1   | 7.3  |
|                      |        | Site                     | 38424010                       | 4424501; w                              | ell SC015065  | 30CDA Fran                               | cois (lat 3  | 8°42'40", 1   | ong 104°42'  | 45")  |  |
| 07-01-82             | 1250   | 17.0                     | 7.3                            | 1,100                                   | 708   | 44                                       | <.020  | 4.0   | <.070  | .90   | 4.9  |
|                      |        | Sit                      | e 3843491                      | 04411501;                               | Black Squi  | rrel pipe li                             | ne (lat 38°  | 43'49", lon   | g 104°41'15  | <u>")</u>   |  |
| 06-25-82             | 1500   | 15.0                     | 7.6                            | 340                                     | 218   | 8.4                                      | <.020  | 4.60  | < . 0,70   | 1.5   | 6.1  |